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THE EFFECT OF TURNOVER RATE ON GROUP TASK TIME

WHEN TASK TIME IS GOVERNED

BY THE LEARNING CURVE

RESEARCH REPORT

Presented in Partial Fulfillment of the Requirements For the Degree Master of Engineering, Industrial Engineering Department of Texas A&M University

Ву

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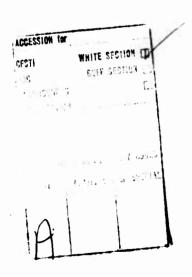
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ABSTRACT

A model is developed to analyze the effect of various percentage turnover per turnover period on group task time when task time is governed by the learning function.

A computer program is developed which generates tables showing the results of the analysis. Nineteen families of curves are presented which depict the contents of the tables.



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CONTENTS

Chapter		Page
I	INTRODUCTION	1
II	CLASSICAL LEARNING CURVE THEORY	7
III	DEVELOPMENT OF A COMPUTER MODEL	17
	1. Development of Point Convolution	17
	2. Definition of terms	18
	3. The Computer Model	21
	4. The Computer Program	25
IV	RESULTS OF THE ANALYSIS	28
٧	CONCLUSIONS AND EXTENSIONS	37
	1. Conclusions	37
	2. Extensions	37
	LIST OF REFERENCES	39
	APPENDICES	40
	Appendix A:	Ā0.1
	1. The Computer Program for Table Generation	A0.2
	2. Flow Chart	A0.6
	3. Tahles	A1.1

	Page
Appendix B:	. во.1
1. The Computer Program for Curve Plotting	. BO.2
2. Figures B1-B19	. B1-B19

FIGURES

Figure		Page
2.1	CLASSICAL LEARNING CURVE FOR EXPERIENCE FACTORS OF .7, .8, AND .9.	12
2.1.a	LOGARITHMIC PLOT OF THE CLASSICAL LEARNING CURVE FOR AN EXPERIENCE FACTOR OF .9.	12
2.2	LEARNING CURVE WHEN t(x) IS THE LABOR HOURS PER PIECE	15
2.3	LEARNING CURVE WHEN t(x) IS THE AVERAGE LABOR HOURS PER PIECE	15
3.1	DETERMINATION OF TURNOVER PERIOD DURING WHICH THE "STEADY STATE" TASK TIMES ARE OBTAINED.	26

LIST OF FIGURES IN APPENDIX B

Figures		Page
B1	PLOT OF T(IX) AND TN(IX) FOR DIFFERENT TURNOVER RATES WITH Q=0.80 IETR=10	B1
B2	PLOT OF CUMULATIVE AVERAGE TASK TIME WITH Q=0.80 IETR=5	В2
В3	PLOT OF CUMULATIVE AVERAGE TASK TIME WITH Q=0.80 IETR=10	В3
B4	PLOT OF CUMULATIVE AVERAGE TASK TIME WITH Q=0.80 IETR=15	В4
B5	PLOT OF CUMULATIVE AVERAGE TASK TIME WITH Q=0.95 IETR=5	B5
В6	PLOT OF CUMULATIVE AVERAGE TASK TIME WITH Q=0.95 IETR=10	В6
В7	PLOT OF CUMULATIVE AVERAGE TASK TIME WITH Q=0.95 IETR=15	В7
в8	PLOT OF AVERAGE TASK TIME PER TIME PERIOD WITH Q=0.80 IETR=5	B8
В9	PIOT OF AVERAGE TASK TIME PER TIME PERIOD WITH Q=0.80 IETR=10	В9
B10	PLOT OF AVERAGE TASK TIME PER TIME PERIOD WITH Q=0.80 IETR=15	B10
B11	PLOT OF AVERAGE TASK TIME PER TIME PERIOD WITH Q=0.95 IETR=5.	B11

TABLES

Table Page

TABLES GENERATED BY THE COMPUTER

MODEL Appendix A

Figures		Page
B12	PLOT OF AVERAGE TASK TIME PER TIME PERIOD WITH Q=0.95 IETR=10	B12
B13	PLOT OF AVERAGE TASK TIME PER TIME PERIOD WITH Q=0.95 IETR=15	B13
B14	PLOT OF RATIO OF AVERAGE TASK TIME PER TIME PERIOD FOR DIFFERENT TURNOVER RATES TO THE AVERAGE TASK TIME PER TIME PERIOD WITH NO TURNOVER WITH Q=0.80 AND IETR=5.	B14
B15	PLOT OF RATIO OF AVERAGE TASK TIME PER TIME PERIOD FOR DIFFERENT TURN- OVER RATES TO THE AVERAGE TASK TIME PER TIME PERIOD WITH NO TURNOVER WITH Q=0.80 AND IETR=.10	B15
B16	PLOT OF RATIO OF AVERAGE TASK TIME PER TIME PERIOD FOR DIFFERENT TURN- OVER RATES TO THE AVERAGE TASK TIME PER TIME PERIOD WITH NO TURNOVER WITH Q=0.80 AND IETR=15	В16
B17	PLOT OF RATIO OF AVERAGE TASK TIME PER TIME PERIOD FOR DIFFERENT TURN- OVER RATES TO THE AVERAGE TASK TIME PER TIME PERIOD WITH NO TURNOVER WITH Q=0.95 and IETR=5	B17
B18	PLOT OF RATIO OF AVERAGE TASK TIME PER TIME PERIOD FOR DIFFERENT TURN- OVER RATES TO THE AVERAGE TASK TIME PER TIME PERIOD WITH NO TURNOVER WITH Q=0.95 AND IETR=10	B18
B19	PLOT OF RATIO OF AVERAGE TASK TIME PER TIME PERIOD FOR DIFFERENT TURN- OVER RATES TO THE AVERAGE TASK TIME PER TIME PERIOD WITH NO TURNOVER WITH 0=0.95 AND JETR=15	B19

CHAPTER I

INTRODUCTION

In 1936, Dr. T. P. Wright introduced the concept of "learning" via a learning function which empirically described the cumulative average labor cost of producing an airplane as the total number of airplanes to be produced was increased. It is generally recognized by laymen that the time required to accomplish a task will diminish after each successive performance until a seemingly stable rate of performance is obtained. manner in which the task time decreases as a function of the number of performances may be predicted with reasonable success by the learning curve. A rather simplistic but intrinsically sound definition of "learning" for the purposes of this paper could be expressed as follows: Learning occurs when on successive performances of a task the time to perform the task is diminished.

The usual application of the learning curve is by manufacturers who must determine a competitive price when bidding on a contract which specifies the number of items which are to be supplied. It may be readily seen that a vendor who bids on the basis of "first unit"

cost would grossly overprice his product. The learning function is also used on successive orders by the buyer to determine a reasonable price to pay the producer after the first costly units have been produced. Certainly, if little time has elapsed between placing a second order and the fulfillment of the previous contracted quantity, the cost for successive units should closely correspond to the cost of the last few units produced. Hence, a considerable savings to the buyer would be possible if he were aware of the "learning function" before negotiating a new contract. A producer might prefer to lose money or break even on the first batch of articles in anticipation of future orders when he would indeed be able to offer a much lower price than his competitors due to previous "learning."

The military commodity commands require maintainability specifications to be written into the request
for proposal and contract for new equipments when
applicable. Basically, these maintainability requirements are written in such a manner as to assure a certain
mean repair time for the equipment or parts of the
equipment. An attempt is usually made to describe the
distribution of repair times by stating a maximum repair
time or the standard deviation of the repair time. The

acceptability of the equipment must be illustrated by demonstrating the equipment repair time. Methods for determining acceptance or rejection based on the maintainability demonstration tests are contained in MIL STD 471. The tests are usually made under controlled conditions, supposedly duplicating those which will actually be encountered under normal maintenance conditions.

One of the fallacies in making this type of demonstration is that no allowance is made for the expected "learning" which will occur as the maintenance crews perform successive repairs on the equipment.

Obviously, some notice of the learning function should be taken when specifying the maintainability requirements; otherwise, the specifications will tend to be overly restrictive and result in unnecessarily increased purchase cost of an equipment. Indiscriminate use of the normal learning function to predict the mean repair time should be avoided since factors such as turnover of maintenance personnel, time between successive performances of the task and design changes or retrofit actions must be considered.

This paper is devoted to an analysis of the effect of various turnover rates on the time required to perform a task by a group when the task time is governed by the

learning function. Some basic assumptions were made to facilitate the analysis and are as follows:

- Turnover will occur only at the end of a turnover period.
- An integer number of task repetitions will be accomplished in each time period.
- 3. The ratio of the crew size to the number of persons leaving the crew is an integer.

Assumption three was included only to facilitate the rapid achievement of a "steady state" average task time per time period.

In Chapter Three a computerized model will be developed to analyze the effect of turnover under the assumptions stated above. The method used to devermine group task time when individual task times are known will be explained. A definition of all terms and a detailed analysis of the model will be presented. A computer program will be used to generate tables which will list values for the following:

- a. Group task time to perform the ith repetition with zero turnover.
- b. Group task time to perform the ith repetition with "P" percent turnover.
- c. Cumulative average group task time to perform the ith repetition with zero turnover.

- d. Cumulative average group task time to perform the ith repetition with "P" percent turnover.
- e. Average group task time per turnover period with zero turnover.
- f. Average group task time per turnover period with "P" percent turnover.
- g. Ratio of group task time with "P" percent turnover to group task time with zero turnover for
 the ith repetition.
- h. Ratio of group task time per turnover period with "P" percent turnover to group task time per turnover period with zero turnover.

Examples of the tables are included in Appendix A. A separate computer program which utilizes the IBM 360 computer and Calcomp Plotter to plot the tabled relationships is included in Appendix B along with nineteen plots.

A summary of the results of the models and recommended extensions of the analysis of this problem will be made in Chapters Four and Five.

A brief history of the development of the classical theory of learning is presented in Chapter Two. The basic "learning function" as originally presented in 1936 and later models will be stated. A brief discussion of the methodology used in applying the learning

function will be discussed.

CHAPTER II

CLASSICAL LEARNING CURVE THEORY

A brief overview of the history of learning theory is presented at this time to give the reader an insight into the development of the classical learning theory. Aristotle first stated the theory of association and his views are presented here as Tichener (5)*paraphrased them.

"Suppose, Aristotle says, that we are trying to recall something that has slipped our mind, what do we ordinarily do? We hunt through a number of things, beginning with something that is like what we want to recall, or contrary to it, or that was next to it in time, or adjacent to it in space."

Thus Aristotle foreshadowed the development of the four laws of association of ideas: similarity, contrast, succession in time and coexistence in space. These laws were later refined to form the basic argument of the "associationists."

The psychologists worked out logical forms to explain association. The concepts of motivation, pleasure and pain were introduced into the theory of learning by British psychologists.

Numbers in parentheses refer to List of References.

Ebbinghaus began to try to quantity the effect of frequency of association on learning during the last quarter of the 19th century. His results were clear cut and showed that such as association existed. Ebbinghaus thus brought learning theory to its contemporary stage.

English (4) summed up the general "orthodox" position of psychologists on learning in the following statement.

"Mental life or behavior has its basis in experience. The environment affects us through our sense organs. The resulting neural impulse somehow leaves "traces" of its passage through the nervous system so that a recurrence of the same neural circuit is thereafter facilitated. Within limits, the more frequently this circuit is traversed, the greater the facilitation and therefore the greater the learning. Learning is thus the getting and keeping intact of a unitary and unchanging response, or of a unitary bit of knowledge or an idea. Improvement is the selection of more suitable responses, or the elimination of parts of a complex response, but the basic fact is the fixation of unchangeable units."

English went on to say that no one advocates the view exactly as stated above; however, this is the essence of the views most psychologists held at the time.

T. P. Wright (7) in his famous article "Factors Affecting the Cost of Airplanes" introduced the classical learning curve as applied to the average cumulative labor cost of airplanes as the quantity of production increased. Wright began his studies of the variation in cost with quantity in 1922 which led to the publication of his article in 1936.

In developing the curve which shows variation of labor cost with production quantity, it became evident that its form was of the type depicted by the formula $F = N^X$. This resolves into an expression for X as follows:

X = Log F Where F = a factor of cost variation
reciprocal to the quantity N. The
reciprocal of F represents a direct
percent variation of cost vs. quantity. A curve
may be plotted which shows directly the relationship between the two variables and when plotted
log-log paper, it becomes a straight line. In
See Figure 2.1 in this paper such a
curve appears; there called the eighty percent
curve which is represented by a value of .322 for
the exponent X in the above formula. This eighty
percent has a definite meaning in that it represents the factor by which the average labor cost
in any quantity shall be multiplied in order to
determine the average labor cost for a quantity
of twice that number of airplanes.

Wright then presents examples of the theory as applied to the cost of an airplane per pound when producing increasing quantities.

Several authors after Wright have presented mathematical models to explain the stimulus-response learning theories developed by neurologists and

psychologists. However, the results of Wright's work modified to concern individual task times will be the primary consideration of this paper. Occasional references will be made to other mathematical models for enlightenment of the reader.

Wright stated some of the problems encountered with succeeding orders of the same plane which increased costs over those predicted by the learning function. Some of the factors mentioned are: design changes introduced between orders, the lapse of time which encourages forgetting, labor turnover between orders, and refurbishment of tools. The purpose of this paper is to quantify the effect of labor turnover on the average task time.

Wright's original equation is modified to the form shown in Equation 2.1 so that "x" represents the cumulative number of units produced, "N" is the slope of the curve and t(1) is the "value" factor for the first unit. The "value" factor might represent cost of the first unit, time required to perform the initial maintenance task, time required to build the first unit or any other "value" for which the learning function can be shown to be valid. Figure 2.1 shows a plot of the normalized learning function with the value of the ordinate being taken as one unit of cost per physical unit while the abscissa represents the cumulative number

of waits produced. It should be noticed that the values of x are necessarily discrete; however, it is common practice to ignore this fact and to treat Equation 2.1 as a continuous function. In actual application the logarithmic form of Equation 2.1 is used and is shown in Equation 2.1.a.

$$t(x) = t(1) x^{N}$$
 (2.1)

$$\log t(x) = \log t(1) + N \log x$$
 (2.1.a)

Equation 2.1.a is shown plotted in Figure 2.1.a. From the plot it is obvious that N must be a negative number. The value of N may be determined as follows:

$$N = \frac{\log (t(2x)) - \log (t(x))}{\log (2x) - \log (x)} = \frac{\log \frac{t(2x)}{t(x)}}{\log \frac{2x}{x}}$$

$$= \frac{\log \frac{t(2x)}{t(x)}}{\log 2} \qquad (2.2)$$

Wright showed that each time the quantity of "airplanes" doubled, the ratio of t(2x) to t(x) was a constant factor. Let us then call this factor the "experience factor - Q". Therefore, Equation 2.2 will appear as

$$N = \frac{\log Q}{\log Q} \qquad (2.2.a)$$

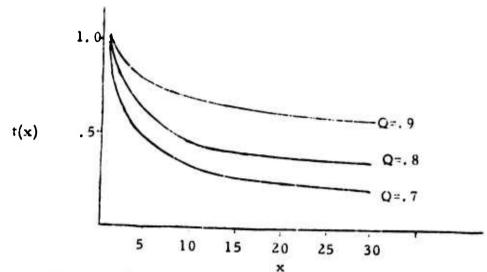


Figure 2.1 Classical learning curve for experience factors of .7, .8, and .9.

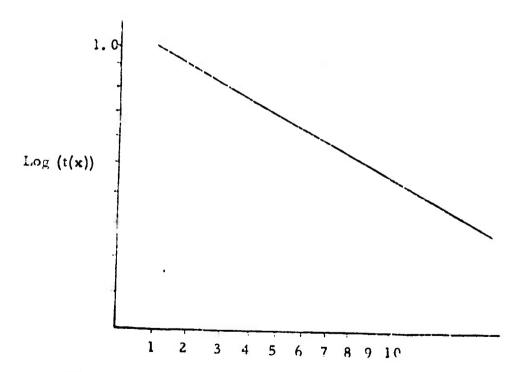


Figure 2.1.a Logarithmic plot of the classical learning curve for an experience factor of .9.

Thus, Equation 2.1 may be written as shown in Equation 2.3.

$$t(x) = t(1) x^{\frac{\log Q}{2}}$$
 (2.3)

Armen Alchian (1) suggested and tested several alternate relationships between direct labor per pound of airframe cumulative production, time of production or rate of production. The results of the comparison of the predictive nature of these relationships to the classical learning curve indicated that the alternates would not generally be better fits. A list of the relationships is presented here.

L = direct labor per pound

T = time

P = production

 ΔP = rate of production per month

a = constant where: a > 0

b = constant where: -1 < b < 0

$$\log L = a_1 + b_1 T$$
 (2.4.a)

$$\log L = a_2 + b_2 T + b_3 (\Delta P)$$
 (2.4.b)

$$\log L = a_3 + b_4 \log T + b_5 \log (\Delta P)$$
 (2.4.c)

$$\log L = a_4 + b_6 T + b_7 \log (\Delta P)$$
 (2.4.d)

$$log L = a_5 + b_8 T + b_9 log (P)$$
 (2.4.e)

$$\log L = a_6 + b_{10} \log P + b_{11} \log (\Delta P)$$
 (2.4.f)

When past history of the parameters concerning the production of an item or the maintenance labor time per task or any other variable for which a model is desired is available, one may resort to regression analysis.

Draper and Smith (3) present methods by which a regression analysis and test of hypothesis may be accomplished. This is a very powerful tool when properly used.

Dr. Wright used the learning curve as applied to the cumulative average hours per unit. Conway and Schultz (2) have considered the relationships between the curve based on the hours per piece and the curve as Dr. Wright originally proposed. Figure 2.2 shows the relationship when t(x) in Equation 2.3 is considered to be the hours per piece. Figure 2.3 depicts the relationship when t(x) in Equation 2.3 is considered to be the cumulative average hours per piece. Conway and Schultz then state that proponents of neither model have been able to establish the superiority of one model over the other either by logic or empirical evidence. Hence, it is largely a matter of choice as to which model is more computationly convenient as to which is used.

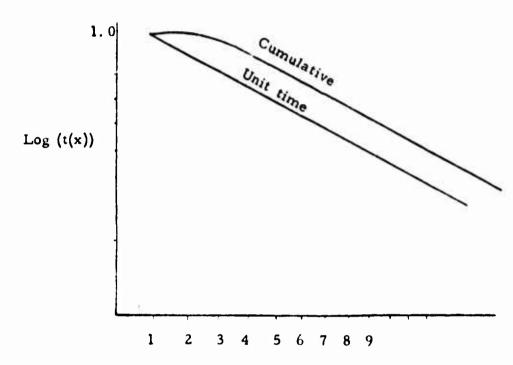


Figure 2.2 Learning curve when t(x) is the labor hours per piece.

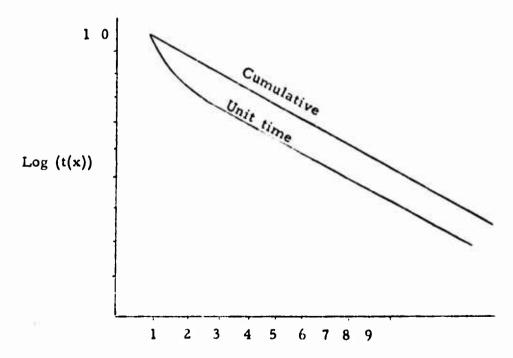


Figure 2.3 Learning curve when t(x) is the average labor hours per piece.

Wilson (6) has shown that the time required to perform a given maintenance task decreases as the number of times the task has been repeated increases and, logically, the average time also decreases. This fact is important and is used as a basis for the model to be developed in this paper. The curves presented for task time per task and cumulative average task time per task follow the same general form as those shown in Figure 2.2.

The computer model utilized to generate the tables shown in appendix A which describe the effect of turnover rate on group task time will be developed in the following chapter. Appendix B contains plots of the results of the computer model.

CHAPTER III

DEVELOPMENT OF A COMPUTER MODEL

1. Development of Point Convolution

"Point convolution" is a phrase which was coined by the author to describe the method of combining individual task times to form a composite group task time (convolution of task times) for a given repetition (point) of the repair task. A similar problem is encountered when one wishes to determine the expected time to complete a given task when each member of the work group has a different "work rate." For example: if workman A and workman B could complete a given task in 2 and 4 hours respectively when working alone, how long would it take workman A and workman B when working together to complete the task? The solution simply involves finding the reciprocal of the sum of the work rates of workman A and workman B.

 $T_A = \text{Time required for workman A to perform the task}$

 $T_B = Time required for workman B to perform the task$

 $R_A = \frac{1}{T_A} = Work rate for workman A$

 $R_{\rm B} = \frac{1}{T_{\rm R}} = \text{Work rate for workman B}$

 R_{T} = Combined work rate of workman A and B

$$R_T = R_A + R_B$$

 T_T = Time required for workman A and B to perform one task together

$$T_{T} = \frac{1}{R_{T}}$$

The concept may be extended to include any reasonable number of workmen.

$$R_{T} = R_{A} + R_{B} + R_{C} + ... + R_{N}$$

$$T_{T} = \frac{1}{R_{T}}$$
(3.1)

Now that a method for convolving task times for a given absolute repetition has been developed, the terms to be used in the computer model will be defined.

2. Definition of Terms

The important terms which are used in the computer model are listed below in alphabetical order:

- ATDAN Ratio of average task time per time period
 with "PERCNT" percent turnover to average
 task time per time period with zero turnover.
- ATTPN Average task time per time period with zero turnover.
- ATTTP Average task time per time period with "PERCNT" percent turnover.
 - AVGT Cumulative average task time per time period with "PERCNT" percent turnover.

- AVGTN Cumulative average task time per time period with zero turnover.
 - ETR Expected number of repair tasks per crew in one time period.
 - F The learning factor "N" as described in Equation 2.2
- FAILR The failure rate of the item being repaired.
- IETR* Integer value of ETR.
- IRAT Number of turnover periods before the
 "steady state" condition is reached.
 - M Number of men leaving a crew at the end of a turnover period.
 - MM Number of men comprising a crew at any given time.
- NCRUS Number of crews in the work force who repair the item under consideration.
- NSYS The number of systems or items in the population from which failures are drawn.
- PERCNT Equals 100 times M divided by MM and is the present turnover in one turnover period.
 - Q The experience factor as described in Equation 2.2.a.
- Note: All names starting with I-N represent integer numbers.

- R The "work rate" for one member of the work crew.
- T Task time for the entire crew to complete one task repetition with turnover.
- TI Time required for the crew to perform the first task.
- TIMP The length of time comprising one time period (turnover period).
- TDTN The ratio of the time required to perform a task with "PERCNT" turnover to the time required to perform a task with zero turnover.
 - TN The time required to perform a task when the turnover per time period is zero.
- XCRUS Floating point representation of NCRUS.
 - XETR Floating point expected number of failures
 per time period.
 - XIR Integer value of MM divided by M.
 - ${\tt XM}$ Floating point representation of M.
 - XMM Floating point representation of MM.
- XNSYS Floating point representation of NSYS.
 - XR Floating point representation of R.

Indexing symbols and symbols for other temporary variables used in the computer program are not listed.

3. The Computer Model

The first objective in defining the model is to consider which parameters have a commonality between different situations so as to reduce the number of computations necessary to describe a range of different situations. Two factors can be readily determined from the classical learning function. Logically, separate tables will need to be generated for each value of the experience factor "Q" since this factor determines the slope of the curve. The tables may be normalized by setting the time required to perform the initial task, TI, equal to one. This is done so the time required to perform a given repetition may be determined from the tables simply by multiplying the tabled value by the actual time required to perform the initial task. The basis for specifying other parameters which exhibit commonality will be developed in the following paragraphs.

Just for the moment, consider the failures of the equipment or the item under consideration to follow the Poisson distribution. The failure rate of the exponential distribution is constant; hence, the number of items failing in an increment of time is directly proportional to the size of the time increment and the number of items in the population. The number of these

failures which a given crew would be required to repair is inversely proportional to the number of repair crews. The foregoing relationships are mathematically stated in Equation 3.2.

$$ETR = \frac{(NSYS)(FAILR)(TIMP)}{(NCRUS)}$$
 (3.2)

For the purposes of this paper, it shall be required that ETR be an integer value. Consideration of a noninteger value of ETR would require the development of a probabilistic model which would indubitably be much more difficult to evaluate and would also tend to conceal the essence of the results with its complexity. Hence, all members of a crew will be considered to complete any task which they begin; i.e., no substitutions and no absences will be allowed. It would seem that all cases with the same number of repetitions of the repair task during a given time period might exhibit some commonality. Note that the preceeding statement does not require the time period between turnovers, the failure rate, the number of items in the population or the number of crews to take on any particular value; but rather, allows each to take on a large range of values.

It seems reasonable to group situations according to the percent turnover at the end of each turnover period. The reason for doing this will be made clearer

as the model is developed.

Let $T^*(IX)$ represent the time required for one person in the crew to accomplish the entire IX^{th} repair assuming this to be possible. For $1 \le IX \le IETR$:

$$R(IX) = \frac{MM}{T^*(IX)}$$
 (3.3)

After the first turnover period, only MM-M of the original crew remain and M unexperienced repairmen are added to the crew. The time required for one repairman from the original group to perform the IXth repetition is T*(IX); however, this will be the first task repetition for each of the "M" new repairmen. The time required for a new repairman to perform the task will correspond to T*(IX-IETR). Therefore, for IETR <IX ≤ 2(IETR):

$$R(IX) = \frac{(MM-M)}{T^*(IX)} + \frac{M}{T^*(IX-IETR)} \qquad (3.4)$$

And similarly it may be shown that for 2(IETR) < IX≤ 3(IETR):

$$R(IX) = \frac{(NM-2M)}{T^*(IX)} + \frac{M}{T^*(IX-IETR)} + \frac{M}{T^*(IX-2(IETR))}$$

and
$$T(IX) = \frac{1}{R(IX)}$$
 (3.5)

When MM is an exact multiple of M, it may be shown that for

$$\left[\frac{MM}{M} - 1\right]$$
 IETR < IX $\leq \frac{MM}{M}$ (IETR):

$$R(IX) = \sum_{N=0}^{\frac{MM}{M}} -1 \frac{M}{T^*(IX-(N)IETR)}, \quad (3.6)$$

and for
$$\frac{MM}{M}$$
(IETR) < IX $\leq \left[\frac{MM}{M} + 1\right]$ IETR:

$$R(IX) = \sum_{N=0}^{\frac{MM}{M}} -1 \frac{M}{T^*(IX-(N)IETR)}$$
 (3.7)

and for every interval thereafter.

Therefore, our tables need only extend to repetition number $\frac{MM}{M}$ (IETR) since thereafter:

$$T^{*}\left[\frac{MM}{M} \quad (IETR)\right] + 1 = T^{*}\left[\left(\frac{MM}{M} - 1\right) \quad (IETR) + 1\right], \quad (3.8)$$

$$T^{*}\left[\left(\frac{MM+1}{M}\right) \quad (IETR) + 1\right] = T^{*}\left[\left(\frac{MM}{M}\right) \quad (IETR) + 1\right]$$

$$= T^{*}\left[\left(\frac{MM}{M} - 1\right) \quad (IETR) + 1\right].$$

When MM is not an exact multiple of M, it can be shown that it is necessary to perform calculations for T(IX) only for IX less than or equal to the integer value of MM divided by M plus one times IETR, i. e.: $IX \leq (IETR) \left\lceil 1 + INTEGER \left(\frac{MM}{M} \right) \right\rceil.$

Figure 3.1 illustrates the relationships presented above. Values in the body of the table represent the number of men from a group added during the time period indicated on the left of the table still remaining in the work group during the time period indicated at the top of the table.

Performing calculations for this many repetitions could be quite laborious if either $(\frac{MM}{M})$ or IETR is large. Fortunately the digital computer can rapidly perform the necessary calculations once a suitable program has been written.

4. The Computer Program

The computer program written to perform this analysis and a flow chart for the program are included in Appendix A along with some samples of the output which was generated. The reason for including a discussion of the computer program is simply to indicate how the necessary indexing was performed.

The following important indices are used in the computer program:

- IX The repetition number.
- IT The time period number.
- TRAT = The number of time periods required for repetition of task times within successive time

	-8,	M=2			
PA	1	2	3	4	5
1	8	6	4	2	
2		2	2	2	2
3			2	2	2
				2	2
					2
	,			4	

Steady State Obtained

MM=8, M=3						
PA P	1	2	3	4	5	
1	8	5	2			
2		3	3	2		
3			3	3	2	
3 3						
3						
Stea	Steady State Obtained					

Note: The first entry in each row corresponds to the number added at the beginning of that turnover period.

A number in the body of the table represents the number of men in the task force as a function of the period in which they were added (PAP) and the present period (P) for the MM and M shown.

Figure 3.1. Determination of turnover period during which the "steady state" task times are obtained.

periods to occur.

Equations 3.4 and 3.5 show how the portion of task time contributed by the original work force decreases until it makes no contribution in time period IRAT and thereafter. A special function "A" was devised to correspond to the work rate of the original work group.

"A" is given by:

$$A(IX) = \frac{1}{MM} \left[(MM - (IT)M)/(IX) EXP(F) \right]. \tag{3.9}$$

The portion of the work rate contributed by the men added after the first period is represented by "B" where:

$$B(IX) = \frac{1}{MM} \sum_{N=1}^{IT} M/[(IX-(IT)(ETR)) EXP(F)] (3.10)$$

Hence, the total work rate for any repetition before IRAT time periods is represented by:

$$R(IX) = \frac{1}{MM} \left[(MM-IT(M))/(IX)EXP(F) + \sum_{N=1}^{IT} (M/(IX-IT(ETR))EXP(F)) \right]$$
(3.11)

where
$$T(IX) = \frac{1}{R(IX)}$$
.

For time period number IRAT, the work rate is expressed by:

$$R(IX) = \frac{1}{MM} \sum_{N=1}^{IRAT-1} M/(IX - IT(ETR)) EXP(F)$$
(3.12)

For every time period thereafter, the task time for the particular repetition is found by the relationship:

$$T(IX) = T(IX - IETR). (3.13)$$

CHAPTER IV

RESULTS OF THE ANALYSIS

The input parameters required to generate a data set are the crew size, number of men in a turnover group, number of systems in the population, failure rate of the systems, length of time between turnovers, number of crews among which the failures are allocated, initial task time and the learning factor for the crew. In a case where only a limited number of repairs could be made during a turnover period, the parameters required to determine the number of repairs during a turnover period could be omitted. The parameters which could be omitted are the failure rate, the turnover period, number of crews and the number of systems in the population. The same parameters could be omitted in any situation where the number of task repetitions in a turnover period are known and equal for each turnover period.

Tables were generated for a crew size of 100 men with turnovers of 5, 10, 20, 25, 50 and 100 men per turnover period, a crew size of 50 men with turnovers of 1, 2, 5, 10, 25 and 50 men per turnover period, and a crew size of 10 men with turnovers of 1, 2, 5 and 10 men per turnover period for Q's of .80, .85, .90 and .95 with IETR's of 5, 10 and 15 repetitions during a turnover period. Examples of the above mentioned tables are included in Appendix A.

In every case where turnover occurred, the task time and average task time increased. Figure B1 (Appendix B) is a plot of the task time with various turnover percentages, a Q of .80 and 5 repetitions per turnover period. Notice that the task time during the first turnover period follows the normal learning curve regardless of the percent turnover. After the first turnover period, a discontinuous increase in the task time occurs at the beginning of each successive turnover period. The waveform for each percentage turnover has an exponentially decaying component until IRAT turnover periods have occurred. The task time then becomes a steady state waveform with a period of IETR repetitions. The type of plot shown in Figure B1 would be of use in determining the task time for any given repetition.

Perhaps a more useful bit of information would be

the determination of the cumulative average task time for various percent turnovers. Figures B2 through B4 depict the cumulative average task time for a given number of repetitions for a Q of .80 and IETR's of 5, 10 and 15. Observe that the curve corresponding to the zero percent turnover or normal learning function is the same regardless of the value of IETR as long as the experience factor is the same. For an IETR of 5 and a 20 percent turnover, the cumulative average task time after 200 repetitions is increased by 79 percent over that for the normal learning function. When IETR is changed to 10 and 15, the percent increase of the cumulative average task time is 48 and 34 percent respectively. When Q is increased to .95, the percent increase due to turnover for IETR's of 5, 10 and 15 is 16, 11 and 8 percent respectively. Figures B5 and B7 are plots of the cumulative average task time for a Q of .95 and IETR's of 5. 10 and 15. One may conclude from the above analysis that for a given Q as the number of repetitions in a given turnover period is increased, the cumulative average task time for a non zero percent turnover will be decreased. One may also conclude that the effect of turnover on task times governed by the learning function decreases as Q is increased.

Figure B1 depicts a very interesting relationship

when one is interested in obtaining a microscopic view of the task time; however, it may be desirable to determine the average task time during any given time period. Figure B8 through B13 are plots of the average task time per time period for Q's of .80 and .95 and IETR's of 5, 10 and 15 for various percent turnovers. The curves are discrete functions; however, they are depicted as being continuous. Values should only be used for an integer number for the period number. After IRAT turnover periods, the average task time per turnover period is constant. Observation of the plots immediately reveals that the average task time during any turnover period after the first increases as the percent turnover is increased.

Plots of the ratio of average task time per time period for different turnover rates to the average task time per time period with zero turnover are shown in Figures B14-B19 for various percent turnovers, Q's and IETR's. Analysis of the plots reveals the following information:

- The ratio increases for a given Q, period number and percent turnover as IETR is increased.
- 2. The ratio is decreased by increasing Q for the same IETR, period number and percent turnover.

3. Increasing both Q and IETR for the same period number and turnover rate causes the ratio to decrease.

The figures in Appendix B are a good source to obtain approximate values of cumulative average task time for use in rough or first estimates. However, if contractual requirements are to be determined, tables such as those shown in Appendix A should be consulted.

Tables are included in Appendix A for 10, 20 and 50 percent turnover per turnover period for Q equal to 0.8, IETR equal to 5.0, and MM's of 10, 50 and 100. Also included is a table for 10, 20 and 50 percent turnover per turnover period for Q equal to 0.8, IETR equal to 10.0, and an MM of 100. A table for 10, 20 and 50 percent turnover per turnover period for Q equal to 0.95, IETR equal to 5.0, and an MM of 100 is also included. Before attempting to use the tables it would be wise to read the first page in Appendix A where the numbering system is explained.

In order to illustrate that the parameters Q, IETR and PERCNT are the only parameters necessary to determine a unique normalized table, tables A1, A2, and A3 may be compared point by point to tables A4, A5 and A6 respectively. Comparing tables A1, A2, A3 or A4, A5, A6 to tables A7, A8 and A9, respectively, leads one to

inductively conclude that a unique table is indeed generated for each set of values of Q, IETR and PERCNT. The foregoing may readily be seen from the mathematical model presented in Section 3 of this chapter. If any of the above tables are compared to tables A13, A14 and A15 where Q is equal to 0.95, it is found that the tabled entries are not identical.

The conclusions stated in the paragraph above are very important in that they allow the use of a table generated for a crew size of 10 with a turnover of 1 per turnover period to be used when the actual situation under consideration involves a crew size of 330 with a turnover of 33 per period (Q and IETR for each case are the same). This fact of course allows generalized tables to be generated and catalogued rather than having to generate a table for each set of parameters as they are encountered.

An example of the use of the tables will now be discussed. The following problem is presented:

The XYZ company operates a nationwide trucking firm for short distance hauling of heavy industrial products. Maintenance centers are located in strategic points about the nation, and are owned and operated by company ABC. Each maintenance crew is composed of ten men each with an experience factor of 0.8. The turnover rate is exactly two men every five major overhauls due to the

difficulty of the work. There will be approximately 100 major overhauls performed by each crew during one year. The ABC company wishes to determine what price to charge for the labor manhours so that it may make a good estimate of total costs before bidding on the contract. The labor cost for the first repetition was demonstrated to be \$1000.

Solution 1: A direct application of the normal learning curve yields the following results (See Table A2).

The cumulative average task time after performing the 100^{th} repetition is found by locating AVGTN(100).

AVGTN(100) = 0.32650.

Hence, the total labor cost for overhauling 100 trucks is estimated as follows:

TLC = 100(1000)(0.32650) = \$32,650.

The cost of overhead is 20% of raw labor.

OVHD = 0.20(32,650) = \$6,530.

The cost of parts is fixed and is \$500 per truck.

PARTS = 100(500) = \$50,000.

Hence the total cost of overhauling 100 trucks is:

TOTAL COST = TLC + OVHD + PARTS = \$89,130.

Solution 2: The effect of turnover is to be taken into account in this solution. (See Table A2).

The cumulative average task time after performing

the 100th repetition when turnover is twenty percent per turnover period is found by locating AVGT(100) in the tables.

AVGT(100) = 0.48130.

TLC = 100(1000)(0.48130) = \$48,130.

OVHD = 0.20(48, 130) = \$9,626.

PARTS = 100(500) = \$50,000.

TOTAL COST = \$107,756.

Analysis of solutions 1 and 2: The difference in the estimated labor costs alone amounts to \$15,480. This amounts to a 47.4 percent increase in labor costs. Total costs are increased by \$18,576. If company ABC had decided to charge fifteen percent over the total cost as the profit margin and had used the normal learning curve as the basis for calculating labor costs, they would have lost money on the contract.

The other columns in the tables could be used to schedule jobs in the shop, to determine the distribution of labor costs over the contract period, and to rapidly determine the average task time during a turnover period.

C'HAPTER V

CONCLUSIONS AND EXTENSIONS

1. Conclusions

This analysis readily discloses the fact that considerable attention should be given to turnover rate, number of repetitions per turnover period and experience factor of the maintenance crews which are to perform maintenance on a given equipment or item before specifying the maintainability parameters. Indiscriminate use of the classical learning function could lead to gross underestimation of future task times when turnover is present.

This paper has presented the basis for a handbook of curves and tables based on three parameters:

- 1. Q experience factor,
- 2. IETR repetitions per turnover period, and
- PERCNT percent turnover per turnover period.

2. Extensions

The model just presented assumes that each man in the group has the same experience factor. A model could readily be developed which predicts the effect of turnover when each man in the group has a different experience factor; however, calculations would have to be for each specific case since there are many possible combinations of parameters.

No consideration of the interaction between workers was considered in the foregoing model. After the initial turnover period, experienced men are available to give advice to the new workers thus possibly increasing the rate at which learning would occur. A model could be developed in which the work rate for the new men is proportionately increased for the first few repetitions.

An even more interesting model would be one in which not all members of the work group participated in the performance of each task. It seems that such an analysis would become quite difficult when turnover is also a factor to be considered.

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APPENDICES

APPENDIX A

This appendix contains the computer program used to generate tables showing the effects of turnover on group task time when task time is governed by the learning curve, a flow chart of the computer program and tables generated by the program.

The page numbers include the table numbers in this appendix. Page "A2.4" indicates that the page is in Appendix A, Table 2, and page 4 of Table 2. There are eight pages in each table in Appendix A.

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GO TO 153
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TI 1.00000 5.00000 5.00000 1.00000 1 0.74755 1 10.00000 1.00000 1.00000 1 0.74755 2 12.50000 0.80000 0.90000 2 0.53146 3 14.24291 0.70210 0.83403 3 0.46451 4 15.62500 0.4000 0.78553 4 0.42891 5 16.78873 0.59564 0.74755 5 0.40694 6 17.02227 0.58743 0.72056 6 0.37254 7 18.08849 0.55284 0.69686 7 0.38295 8 19.00240 0.52625 0.67553 8 0.37673 9 14.81993 0.50454 0.65653 9 0.371364 10 20.56618 0.44624 0.43950 10 0.37136 11 20.09221 0.49771 0.62461 11 0.37136 12 20.92458 0.47791 0.61422 13 21.54577 0.46198 0.50251 14 22.30052 0.44842 0.59150 15 22.90209 0.43655 0.58117 16 22.03416 0.45384 0.57321 17 22.77304 0.43912 0.56533 18 23.41122 0.42715 0.55765 19 23.99173 0.41681 0.55724 20 24.53133 0.40740 0.52657 24.65618 0.59150 15 22.90209 0.43655 0.58117 12 23.37436 0.42762 0.53752 22 24.05578 0.46194 0.52525 0.55765 19 23.99173 0.41681 0.55722 22 24.05578 0.40759 0.46551 0.52557 24 25.2006 0.38615 0.53557 22 22 24.05578 0.40714 0.551185 22 25.55740 0.40780 0.45751 0.52557 24 25.2006 0.38905 0.51587 24 25.2006 0.38905 0.51587 24 25.2006 0.38905 0.51587 25 25.55740 0.39128 0.50355 0.40019 0.49225 0.255554 0.37657 0.49812 0.59552 0.49941 0.2555724 0.39026 0.48906 0.51587 0.49913 0.40020 0.48906 0.55187 0.49913 0.40020 0.48906 0.55187 0.49913 0.40020 0.48906 0.48906 0.55187 0.49913 0.40020 0.48906 0.4890	MM 10	M NSYS 1 10000	FAILR 0.50000E-03	T[MP 10.0000	CREWS 10	Q 0.80000
1 10.00000 1.00000 1 0.74755 2 12.50000 0.80000 0.90000 2 0.53146 3 14.24291 0.70210 0.83403 3 0.46451 4 15.02500 0.04000 0.78553 4 0.42891 5 16.78873 0.95644 0.74755 5 0.40694 6 17.02327 0.58743 0.72066 6 0.39254 7 18.08849 0.55254 0.69686 7 0.36295 8 19.00240 0.52625 0.67553 8 0.37673 9 19.31993 0.50454 0.65653 9 0.37673 9 19.31993 0.50454 0.65653 9 0.37304 10 20.56619 0.49624 0.503653 9 0.37304 11 20.09221 0.49771 0.62661 11 0.37136 12 20.92458 0.47791 0.61422 13 21.54577 0.46193 0.50251 14 22.30052 0.44842 0.59150 15 22.90709 0.443655 0.58117 16 22.03416 0.45384 0.57321 17 22.77304 0.43912 0.56533 18 23.4112 0.42715 0.55765 19 23.99173 0.41681 0.55024 20 24.57132 0.40764 0.55311 . 21 23.37436 0.42715 0.55765 22 24.05578 0.41553 0.53207 23 24.560.9 0.40551 0.52657 24 25.20076 0.39681 0.57321 25 25.70360 0.39681 0.57116 26 24.31266 0.4114 0.51185 27 24.98750 0.40620 0.50371 28 25.55740 0.39681 0.50355 29 26.07468 0.38351 0.49941 30 26.55564 0.37657 0.49523 31 24.560.9 0.40620 0.50375 32 25.63724 0.39006 0.48906 33 26.19258 0.38179 0.44561 34 26.5664 0.37459 0.49521 35 27.16383 0.36114 0.47677 37 26.07530 0.36150 0.47677 37 26.07530 0.36150 0.47677 37 26.07530 0.36150 0.47675 38 26.62221 0.37563 0.47175 39 27.1173 0.36876 0.46645 41 25.70590 0.38610 0.46645 42 22.2118 0.37653 0.45627 43 26.48406 0.37167 0.46645 44 22.3164 0.37657 0.46567 45 27.83118 0.36529 0.45827 47 26.46488 0.37657 0.46524 48 27.00505 0.38620 0.46645 49 27.49438 0.36571 0.45657 40 27.49438 0.36571 0.45657 41 25.49438 0.36571 0.45657 42 27.49487 0.39667 0.46656 43 27.49488 0.37667 0.456294 44 27.49438 0.36371 0.45657	1.					
47 26.46448 0.37786 0.45294 48 27.00505 0.37030 0.45122 49 27.49438 0.36371 0.44943 50 27.94867 0.35780 0.44760	1. 11. 12.3456789012345678901234567890123444445 11. 11. 12.345678901234567890123444445	TI 10.00000 12.50000 12.50000 14.24291 15.62500 16.78873 17.02323 18.08649 19.81993 20.56618 20.92458 21.64577 22.30052 22.90709 22.90709 22.90709 22.90709 22.90709 22.90709 22.90709 22.90709 22.90709 22.90709 22.90709 22.90709 22.90709 22.90709 22.90709 22.90709 22.90709 22.90709 22.90709 23.41122 23.99173 24.55133 23.37436 24.65049 25.20006 27.70360 24.32266 24.98750 26.67530 26.67530 26.67530 26.67530 26.34164 27.37518 27.83118	ETR IETR 5.00000 T(IX) 1.00000 0.80000 0.80000 0.59564 0.59564 0.59564 0.52625 0.50454 0.48624 0.49771 0.46198 0.44842 0.43655 0.44842 0.42715 0.46198 0.42715 0.41681 0.42782 0.42715 0.41681 0.42782 0.42715 0.41681 0.42782 0.42715 0.41681 0.40551 0.38905 0.41114 0.40020 0.38179 0.37459 0.36814 0.39316 0.387563 0.36876 0.36876 0.36876 0.36876 0.36529 0.35931	AVGT(IX) 1.00000 0.90000 0.83403 0.74755 0.74755 0.69686 0.67553 0.65653 0.65653 0.65653 0.65653 0.55765 0.557321 0.56533 0.55765 0.55765 0.51587 0.51587 0.51587 0.51587 0.51587 0.51587 0.51587 0.51587 0.51587 0.51587 0.51587 0.51587 0.51587 0.51587 0.51587 0.51587 0.48581 0.48581 0.48581 0.48581 0.47927 0.46456 0.46456 0.46456 0.46456 0.46827 0.45827 0.45827 0.45827	J A 1 2 3 4 5 6 7 8 9 10	ATTTP(J) 0.74755 0.53146 0.46451 0.42891 0.40694 0.39254 0.38295 0.37673 0.37136
51 25.83052 0.38714 0.44641 52 26.46448 0.37786 0.44509	47 48 49 50	26.46448 27.00505 27.49438 27.94867 25.83052	0.37786 0.37030 0.36371 0.35780 0.38714	0.45294 0.45122 0.44943 0.44760 0.44641		

53	27.00505	0.37030	0.44368
54	27.19438	0.30771	0.44220
55	27.94867	0.35780	0.44067
	25.83052		
56		0.38714	0.43971
57	26. 46448	0.37786	0.43863
58	27.00505	0.37030	0.43745
59	27.49433	0.36371	0.43620
50	21.94867	0.35780	0.43489
61	25.83052	0.38714	0.43411
6?	26.40448	0.37786	C.43320
63	27.00505	0.37033	0.43220
54	27.49438	0.36371	0.43113
65	27.94867	C.35780	0.43000
60	25.83052	0.38714	0.42935
67	26.46448	0.37786	0.42859
68	27.00505	0.37030	0.42773
69	27.49438	0.36371	0.42680
7 C	27.94967	0.35780	0.42581
71	25.83052	0.38714	0.42527
72	26.46448	0.37786	0.42461
73	27.00505	0.37030	
			0.42387
74	27.49438	0.36371	0.42305
75	27.94867	0.35780	0.42218
76	25.33052	0.38714	0.42172
77	26.46448	0.37786	0.42115
78	27.00505	0.37030	C.42050
79	27.49438	0.36371	0.41978
80	27.94867	0.35780	0.41901
81	25.83052	0.38714	C.41861
82	26.46448	0.37786	0.41812
8 3	27.00505	0.37030	0.41754
94	27.49438	0.36371	0.41690
85	27.94867	0.35780	0.41620
36	25.53052	0.38714	0.41587
97	26.46443	0.37786	0.41543
88	27.00505	0.37030	0.41492
89	27.49438	0.36371	0.41434
	27.94867	0.35780	
90			0.41371
91	25.83052	0.38714	0.41342
92	26.46448	0.37786	0.41303
93	27.00505	0.37030	0.41257
94	27.49438	0.36371	0.41205
95			
	27.94867	0.35780	0.41148
96	25.83052	0.38714	0.41123
97	26.46448	0.37786	0.41089
98	27.00505	0.37030	G. 41047
99	27.49438	0.36371	
			0.41000
100	27.94867	0.35780	0.40948
101	25. 8305 <i>2</i>	0.38714	0.40926
102	26.46448	0.37786	0.40895
103	27.00505	0.37030	0.40857
104	27.49438	0.36371	0.40814
105	27.94867	0.35780	0.40766
106	25.83052	0.38714	0.40747
107	26.46448	0.37786	0.40719
108	27.00505	0.37030	
			0.40685
109	27.49438	0.36371	0.40645
110	27.94867	0.35780	0.40601
111	25.83052	0.38714	0.40584
112	26.46448	0.37786	0.40559
113	27.00505	0.37030	
443	2100000	0.31030	0.40528

114	27.49438	0.36371	0.40491
115	21 1	0.35780	-
110	25.83052		0.40450
		C.38714	0.40435
117	25.46448	0.37786	0.40413
118	27.00505	0.37030	0.40384
119	27.49438		
		0.36371	0.40350
120	27.94867	0.35780	0.40312
121	25.83052	0.38714	0.40299
122	26.46448	0.37786	
123	27.00505		0.40279
		0.37030	0.40252
124	27.49438	0.36371	0.40221
125	27.94867	0.35780	0.40185
126	25.83052	C.38714	
127			0.40174
	26.46448	0.37786	0.40155
128	27.00505	0.37030	0.40130
129	27.49438	0.36371	0.40101
130	27.94867		
131		0.35780	0.40068
	25.83052	0.38714	0.40058
132	26.46448	0.37786	0.40040
133	27.00505	0.37030	C.40018
134	27.49438		
135		0.36371	0.39991
	27.94867	0.35780	0.39959
136	25.83052	0.38714	0.39950
137	26.46448	0.37786	0.39934
138	27.00505	0.37030	
139			0.39913
	27.49438	0.36371	C.39888
140	27.94867	0.35780	0.39859
141	25.83052	0.38714	0.39850
142	26.46449	0.37786	C.39836
143	27.00505	0.37030	
144			C.39816
	27.49438	0.36371	0.39792
145	27.94867	0.35780	0.39765
146	25.93052	0.38714	0.39757
147	26.46443	0.37786	0.39744
149	27.90505		
149		0.37030	0.39726
	27.49438	0.36371	0.39703
150	27.94867	0.35780	0.39677
151	25.83052	0.38714	0.39671
152	26.46448	0.37786	
153	27.00505		0.39658
		0.37030	0.39641
154	27.49438	0.36371	0.39620
155	27.94867	0.35780	0.39595
156	25.83052	0.38714	0.39589
157	26.46448		
158		0.37786	0.39578
	27.00505	0.37030	0.39562
159	27.49438	0.36371	0.39542
160	27.94867	0.35780	0.39518
161	25.93052	0.38714	
162			0.39513
	26.46448	0.37786	0.39503
163	27.00505	0.37030	0.39487
164	27.49438	0.36371	0.39468
165	27.94867	0.35780	
166			0.39446
	25.83052	0.38714	0.39442
167	26.46448	0.37786	0.39432
168	27.00505	0.37030	0.39417
169	27.49438	0.36371	0.39399
.70	27.54867		
		0.35780	0.39378
.71	25.83052	0.38714	0.39374
.72	26.46448	0.37786	0.39365
.73	27.00505	C.37030	0.39351
74	27.49438	0.36371	
•	L 1 # 7 7 7 3 0	0.30311	0.39334

175	27.94867	0.35780	0.39314
176	29.03082	0.38714	0.39311
177	26.46443	0.37786	0.39302
178	27.00505	0.37030	0.39289
179	27.49438	0.36371	0.39273
130	27.94867	0.35780	0.39253
181	25.83052	0.38714	0.39250
182	26.46448	0.37786	0.39242
183	27.00505	0.37030	0.39230
184	27.49438	0.36371	0.39215
135	27.94867	0.35780	0.39196
186	25.83052	0.38714	0.39194
187	26.46448	0.37786	0.39186
188	27.00505	0.37030	0.39175
189	27.49438	0.36371	0.39160
190	27.94867	0.35780	0.39142
191	25.83052	0.38714	0.39140
192	26.46448	0.37786	0.39133
193	27.00505	0.37030	0.39122
194	27.49438	0.36371	0.39108
195	27.94867	0.35780	0.39091
196	25.83052	0.38714	0.39089
197	26.46448	0.37786	0.39082
198	27.00505	0.37030	0.39072
199	27.49438	0.36371	0.39058
200	27.94867	0.35780	0.39042

53	0.27855	1.32937	0.39552
54	0.21653	1.31300	0.39432
55	0.27525	1.29990	0.39117
56	0.27366	1.41408	0.38907
57	0.27210	1.38866	0.38702
58	0.27059	1.36852	0.38501
59	0.26910	1.35158	
50	0.26765		0.38305
		1.33583	0.38113
61	0.26623	1.45417	0.37924
62	0.26484	1.42678	0.37740
63	0.26349	1.40544	0.37559
64	0.20214	1.38744	0.37382
65	0.26084	1.37172	0.37208
65	0.25956	1.49152	0.37037
67	0.25831	1.46285	0.36870
68	0.25708	1.44042	0.36706
69	0.25587	1.42145	0.36545
70	0.25469	1.40484	0.36386
71	0.25353	1.52700	0.36231
72	0.25239	1.49714	
73			0.36078
	0.25127	1.47371	0.35928
74	0.25017	1.45383	0.35781
75	0.24910	1.43639	0.35536
76	0.24804	1.56082	0.35493
77	C.24699	1.52586	0.35353
78	0.24597	1.50547	0.35215
79	0.24496	1.48476	0.35080
80	0.24397	1.46655	0.34946
81	0.24300	1.59317	0.34815
82	0.24204	1.56116	0.34685
83	0.24110	1.53589	0.34558
84	0.24017	1.51438	
85	0.23926		0.34432
		1.49545	0.34309
86	0.23836	1.62419	0.34187
87	0.23747	1.59119	0.34067
98	0.23660	1.56509	C.33949
39	0.23574	1.54283	0.33832
90	0.23490	1.52322	0.33717
91	0.23406	1.65401	0.33604
92	0.23324	1.62007	0.33492
93	0.23243	1.59318	0.33382
94	0.23163	1.57022	0.33273
95	0.23084	1.54997	0.33166
96	0.23007	1.68273	0.33060
97	0.22930	1.64791	0.32956
98	0.22854	1.62027	
99	0.22780		0.32853
100		1.59664	0.32751
	0.22706	1.57578	0.32650
101	0.22634	1.71246	0.32551
102	0.22552	1.67479	0.32453
103	0.22441	1.64643	0.32356
104	0.22421	1.62217	0.32261
105	0.22352	1.60072	0.32167
105	0.22284	1.73728	0.32073
107	0.22217	1.70080	0.31981
108	0.22151	1.67175	0.31890
159	0.22085	1.64697	0.31800
110	0.22020	1.62488	0.31711
111	0.21956	1.76325	
112	0.21693		0.31623
		1.72598	0.31537
113	0.21830	1.69628	0.31451

		. 3000	
114	0.21768	1.67083	0.31366
115	C. 2170:	1.64830	0.31282
116	0.21547	1.78844	0.31199
	0.21587	1.75042	0.31116
117			
118	0.21520	1.72009	0.31035
119	0.21470	1.69407	0.30955
120	0.21412	1.67103	0.30875
121	0.21355	1.81290	0.30797
122	0.21294	1.77417	0.30719
123	0.21242	1.74323	0.30642
124	0.21157	1.71667	0.30565
125	0.21132	1.69314	0.30490
125	0.21078	1.83669	0.30415
127	0.21025	1.79726	0.30341
128	0.20972	1.76573	0.30268
129	0.20919	1.73866	0.30196
		-	
130	0.20867	1.71465	0.30124
131	0.20816	1.85984	0.30053
132	0.20765	1.81974	0.29982
133	0.20714	1.78765	0.29913
134	0.20665	1.76007	0.29844
135	0.20615	1.73561	0.29775
136	0.20565	1.88240	0.29708
137	0.20519	1.84165	0.29641
138	0.20470	1.80901	0.29574
139	0.20422	1.78095	0.29508
140	0.20375	1.75605	0.29443
141	0.20329	1.90441	0.29378
142	0.20232	1.86302	0.29314
143	0.20237	1.82986	0.29251
144	0.20191	1.80133	0.29188
145	0.20145	1.77600	0.29126
146	0.20102	1.92589	0.29064
		1.88389	
147	0.20058		0.29002
148	0.20014	1.85022	0.28942
149	C.19971	1.92123	0.23881
150	0.19928	1.79549	0.28322
151	0.19885	1.94589	0.28763
152	0.19843	1.90429	0.28704
153	0.19801	1.87012	0.28646
154	0.19759	1.84069	0.28588
155	0.19719	1.81455	0.28531
156	0.19678	1.96741	0.29474
157	0.19 37	1.92423	0.28418
158	C.19597	1.88958	0.28362
159	0.19557	1.85972	0.28307
160	0.19518	1.83319	0.28252
161	0.19479	1.58749	0.28197
162	0.19440	1.94376	0.28143
153	0.19401	1.90862	0.28089
	0.19363	1.87835	0.28036
154			
165	0.19325	1.85144	0.27983
156	0.19288	2.00716	0.27931
157	0.19251	1.96287	0.27879
168	0.19214	1.92728	0.27827
		1.89660	0.27776
169	0.19177		
170	0.19141	1.86932	0.27725
171	0.19105	2.02643	0.27675
172	0.19069	1.98160	0.27625
173	0.19033	1.94556	0.27575
		1.91448	0.27526
174	0.18998	10 71 740	0121720

175	C.18963	1.48694	0.27477
170	0.18928	2.04532	0.27428
177	0.18894	1.99996	0.27380
178	0.18859	1.96349	0.27332
179	0.18825	1.93202	0.27285
180	0.18792	1.90403	0.27238
191	0.19759	2.06384	0.27191
182	0.18725	2.C1798	0.27144
133	0.18692	1.98108	0.27098
184	0.18659	1.94923	0.27052
185	0.18627	1.92090	0.27007
186	0.18594	2.08203	0.26961
187	C.18562	2.03566	0.26917
138	0.18530	1.99834	0.26872
189	0.18499	1.96613	0.26828
190	0.18467	1.93746	0.26784
191	0.19436	2.09988	0.26740
192	0.18405	2.05303	0.26696
193	0.18374	2.C1530	0.26653
194	0.18344	1.98273	0.26611
195	0.19314	1.95373	0.26568
196	0.18283	2.11743	0.26526
197	0.18254	2.07009	0.26484
198	0.18224	2.03196	0.26442
199	0.18194	1.99904	0.26401
200	0.18165	1.96972	0.26359

мм 10	M NSYS 2 10000	FAIL 0.500CCE-0		CREWS 10	Q 0.80000
1	TI •00000	ETR IF	TR 5		
1X 1 2 3 4 5 6 7 8 9 10 11 12 13 14	R(IX 10.0000 12.5000 14.2429 15.5250 16.7887 16.2429 17.4675 19.3538 20.1464 18.5446 19.5946 20.4561 21.2142	T(IX) 0 1.00000 0 .80000 1 0.70210 0 0.64000 3 0.59564 0 0.61565 4 0.57249 7 0.54131 4 0.51669 7 0.49636 2 0.53924 0 0.51034 0 0.48885 0 0.47138	AVGT(IX) 1.00000 C.90000 0.83403 0.78553 0.74755 0.72557 0.70370 0.68340 C.66488 0.64803 0.53814 0.62749 0.61682 0.60643	1 2 3 4 5	TTTP(J) 0.74755 0.54850 0.49328 0.46955 0.46046 0.46046
15 16 17 18 19 20 21 22 23 24 25 26 27	21.9021 19.6543 20.6508 21.4649 22.8302 20.1010 21.0817 21.8813 22.5837 23.2210 20.1010 21.0817	1	0.59644 0.59096 0.58469 0.57139 0.56472 0.56152 0.55756 0.55318 0.54387 0.54208 0.53957		•
28 29 30 31 32 33 34 35 36 37 38	21.9813 22.5837 23.2210 20.1010 21.0817 21.8813 22.5837 23.2210 20.1010 21.0817 21.8813 22.5837	0.44280 0.43064 0.49749 0.47434 0.45701 0.44280 0.43064 0.49749 0.47434 0.45701	0.53663 0.53339 0.52997 0.52892 0.52721 0.52508 0.5266 0.52066 0.52003 0.51941 0.51819 0.51658 0.51469		
40 412 43 445 467 49 51 51	23.22104 20.10106 21.08176 21.08176 22.58376 23.22104 20.10104 21.08176 23.22104 20.10104 21.08176	0.49749 0.47434 0.45701 0.45701 0.43064 0.49749 0.47434 0.45701 0.44280 0.43064 0.49749	0.51259 0.51222 0.51132 0.51005 0.50852 0.50679 0.50659 0.50590 0.50489 0.50362 0.50216 0.50207 0.50153		

53	21.88135	0.45701	0
54	22.58 15	0.44280	0.50069
55	23.22134	0.43064	0.49962
56	20.10104	0.49749	0.49837
57	21.06179		0.49835
58	21.86135	0.47434	0.49793
59	22.58376	0.45701	0.49722
90	22 1210	0.44280	0.49630
51	23.22104	0.43064	0.49521
62	20.10104	0.49749	0.49524
63	21.08179	0.47434	0.49491
54	21.88135	0.45701	0.49431
	22.58376	0.44280	0.49350
65	23.22104	0.43064	0.49253
66	20.10104	0.49749	0.49261
67	21.38179	0.47434	0.49234
68	21.88135	0.45701	0.49182
69	22.58376	0.44280	0.49111
70	23.22104	0.43064	
71	20.10104	0.49749	0.49024
7 2	21.08179	0.47434	0.49034
73	21.88135	0.45701	C. 49012
74	22.58376		0.48967
75	23.22104	0.44280	0.48903
76	20.10104	0.43064	0.48826
77	21.00104	0.49749	0.48838
78	21.08179	0.47434	0.48819
79	21.88135	0.45701	0.48779
	22.58376	0.44280	0.48723
80	23.22104	0.43064	0.48652
51	20.10104	0.49749	0.48665
82	21.38179	0.47434	0.48650
83	21.38135	0.45701	0.48615
84	22.58376	0.44280	0.48563
85	23.22104	0.43064	0.48498
86	20.10104	0.49749	
37	21.08179	0.47434	0.48513
88	21.38135	0.45701	0.48501
89	22.58376	0.44280	0.48469
90	23.22104		0.48422
91	20.10164	0.43064	0.48362
92	21.08179	0.49749	0.48377
93	21.88135	0.47434	0.48367
94	22.58376	0.45701	0.48338
95		0.44280	0.48295
96	23.22104	0.43064	0.48240
97	20.10104	0.49749	0.48256
98	21.08179	0.47434	C.48247
99	21.88135	0.45701	0.48221
	22.58376	0.44280	0.48182
100	23.22104	0.43064	0.48130
101	20.10104	0.49749	0.48146
102	21.08179	0.47434	0.48139
103	21.88135	0.45701	0.48116
104	22.58376	0.44280	
105	23.22104	0.43064	0.48079
106	20.10104	0.49749	0.48031
107	21.06179	0.47434	0.48047
108	21.38135	0.45701	C. 48042
109	22.58376		0.48020
110	23.22104	0.44280	0.47986
111		0.43064	0.47941
112	20.10104	0.49749	0.47957
113	21.08179	0.47434	0.47952
	21.86135	0.45701	0.47932

114	22.58376	0.44280	0.47900
			-
115	. , = - ` '4	0.43064	0.47358
116	20.10104	0.44749	0.47375
117	21.08179	0.47434	0.47871
115	21.30135	0.45701	0.47853
110	22.58376	0.44280	0.47822
1.30		0.43064	
120	23.22104		C.47783
121	20.10104	0.49149	0.47799
122	21.08179	0.47434	0.47796
123	21.82135	0.45701	0.47779
124	22.58376	0.44280	0.47751
125	23.22104	0.43064	0.47713
			_
125	20.10104	0.49749	0.47729
127	21.18179	0.47434	0.47727
128	21.88135	0.45701	0.47711
1 20	22.58376	0 66290	
129	62.36310	0.44280	0.47685
130	23.22104	0.43064	0.47649
_			-
131	20.10104	0.49749	0.47665
132	21.08179	0.47434	0.47663
133	21.86135	0.45701	0.47649
134	22.58376	0.44280	0.47623
135	23.22104	0.43064	0.47590
136	20.10104	0.49749	0.41606
137	21.08179	0.47434	C. 47604
138	21.88135	0.457Cl	0.47591
139	22.58376	0.44280	0.47567
140	23.22104	0.43064	0.47535
141	20.10104	0.49749	0.47550
142	21.08179	0.47434	0.47549
143	21.86135	0.45701	0.47536
144	22.56376	0.44280	0.47514
145	23.22134	0.43064	0.47483
147			
146	20.10104	0.49749	0.47499
-			
147	21.08179	0.47434	0.47498
148	21.88135	0.45701	0.47486
149	22.58376	0.44280	C. 47465
150	23.22104	0.43064	0.47435
151	20.10104	0.49749	0.47451
152	21.08179	0.47434	0.47450
		-	
153	21.88135	0.45701	0.47439
154	22.58376	0.44280	0.47418
155	23.22104	0.43064	0.47390
156	20.10104	0.49749	0.47406
157	21.08179	0.47434	0.47406
158	21.80135	0.45701	0.47395
159	22.59375	0.44280	0.47375
160	23.22104	0.43064	0.47348
161	20.10104	0.49749	0.47363
162	21.08179	0.47434	0.47364
163	21.89135	0.45701	0.47353
	22.58376	0.44260	0.47335
154			
165	23.22104	0.43064	0.47309
		0.49749	0.47324
166	20.10134		
167	21.08179	0.47434	0.47324
168	21.88135	0.45701	0.47315
159	22.58376	0.44280	0.47297
170	23.22104	0.43064	0.47272
171	20.10104	0.49749	0.47286
172	21.06179	0.47434	0.47287
173	21.88135	0.45701	C.47278
174	22.58376	0.44280	0.47261

175	23.22104	0.43064	7.47237
17b	20.10194	0.49749	C.47251
177	21.18179	0.47434	0.47252
178	21.88135	0.45701	0.47243
179	22.58376	0.44280	0.47227
180	23.22104	0.43764	0.47204
181	20.10104	0.49749	0.47218
182	21.08179	0.47434	0.47219
183	21.98135	0.45701	0.47210
1 34	22.58376	0.44280	0.47195
185	23.22104	0.43064	0.47172
186	20.10104	0.49749	0.47186
187	21.03179	0.47434	0.47187
188	21.88135	0.45701	0.47179
189	22.58376	0.44280	0.47164
190	23.22104	0.43064	0.47143
191	20.10104	0.49749	0.47156
192	21.09179	0.47434	0.47158
193	21.98135	0.45701	0.47150
194	22.58376	0.44280	0.47135
195	23.22104	0.43064	0.47114
196	20.10104	0.49749	0.47128
197	21.08179	0.47434	0.47129
196	21.88135	0.45701	0.47122
199	22.58376	0.44280	0.47108
200	23.22104	C. 43764	0.47088

v vj	v. NS	Y S	FAILR	TIMP	CREWS	Q
10	2 100	0.500	005-03	10.0000	10	0.80000
	TI	ETR	IETR			
1	1.00000	5.00000	5			
1.	TA. / T v 1	TOTALLIVA	ANCTHILLY	ATTON		TDANIZIA
IX 1	1.00000	TDTN(1x) 1.00000	1.00000	0.74		1.00000
Ž	0.80000	1.00000	0.90000	0.51		1.06397
3	0.70210	1.00000	0.83403	0.439		1.12356
4	0.64000	1.00000	0.78553	0.394		1.18910
5	0.59564	1.00000	0.74755	0.36		1.26245
6	0.56168	1.09609	0.71657	0.34	226	1.34534
7	0.53449	1.07110	0.69056			
8	0.51200	1.05725	0.66824			
9	0.49295	1.04817	0.64876			
10	0.47651	1.04167	0.63154			
11	0.46211 0.44935	1.16690 1.13575	0.60224			
13	0.43792	1.11631	0.59960			
14	0.42759	1.10241	0.57802			
15	0.41820	1.09177	0.56737			
16	0.40960	1.24217	0.55751			
17	0.40158	1.20553	0.54934			
18	0.39436	1.18135	0.53979			
19	0.38756	1.16330	0.53178			
20	0.38121	1.14902	0.52425			
21	0.37527	1.32569	0.51715			
22	0.36969	1.28309	0.51045			
23	0.36444	1.25402	0.50410			
24	0.35943	1.23178	0.49808			
25 26	0.35478	1.21382 1.42004	0.49234 0.48688			
27	0.34610	1.37053	0.48167			
28	0.34207	1.33600	0.47668			
29	0.33823	1.30915	0.47191			
30	0.33456	1.28720	0.46733			
31	0.33105	1.50277	0.46293		•	
32	0.32768	1.44758	0.45871			
دَ 3	0.32445	1.40857	0.45464			
34	0.32135	1.27794	0.45072			
35	0.31836	1.35268	0.44694			
36	0.31549	1.57688	0.44328 0.43976			
37 38	0.31272	1.51684 1.47402	0.43634			
39	0.30746	1.44016	0.43304			
40	0.30497	1.41210	0.42984			
41	0.30255	1.64430	0.42673			
42	0.30021	1.58002	0.42372			
43	0.29795	1.53386	0.42079			
44	0.29575	1.49719	0.41795			
45	0.29362	1.46667	0.41519			
46	0.29155	1.70536	0.41250			
47	0.28954	1.63828	0.40988			
45	0.22758	1.58915	0.40734			
44	0.28568	1.54998	0.40485			
50 51	0.28383 0.28202	1.51727 1.76399	0.40243 0.40007			
52	0.28027	1.69247	0.39777			
-						

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54
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                                    U. 38907
    57
           0.27210
                       1.74324
                                    0.38702
    58
           C.27058
                       1.68997
                                    0.38501
    59
           0.25910
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                                    0.38305
    60
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                                    0.38113
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    62
           0.26484
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                                   0.37740
    63
           0.26348
                       1.73454
                                   0.37559
    54
           C. 26214
                       1.68913
                                   0.37382
    55
           0.26084
                       1.65099
                                   0.37208
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           0.25956
                       1.91665
                                   0.37037
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           0.25831
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                                   0.36870
    68
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    69
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   70
           C.25469
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                                   0.36386
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                      1.96224
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                                   0.35928
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                                   0.35781
   75
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                                   0.35536
   76
          0.24804
                      2.00571
                                   0.35493
   77
          0.24699
                      1.92047
                                   0.35353
   78
          0.24597
                      1.85799
                                  0.35215
   79
          0.24496
                      1.80760
                                  0.35090
   80
          0.24397
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   91
          0.24300
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          0.24204
   82
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   83
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                                  0.34558
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          3.23926
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   98
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         0.23490
                     1.83334
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  71
         0.23406
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  92
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  93
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  94
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 101
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102
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103
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104
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                    1.97439
                                 0.32261
105
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                    1.92662
                                 0.32167
100
        0.22294
                    2.23246
                                 0.32073
107
        0.22217
                    2.13505
                                 0.31981
108
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                    2.06320
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109
        0.22035
                    2.00497
                                 0.31800
110
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                                0.31711
111
        0.21956
                    2.26583
                                0.31623
112
        3.21893
                    2.16667
                                0.31537
113
        C. 21830
                    2.09348
                                C.31451
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114	0.21763	2.03413	0.31366
115	0.217.7	1.98388	0.31282
116	0.21:17	2.29820	0.31199
117	0.21537	2.19735	0.31116
118	0.21525	2.12287	0.31035
119	0.21470	2.96243	0.30955
120	0.21412	2.01124	0.30875
121	0.21355	2.32964	0.30797
122	0.21293	2. 22715	6.30719
123	0.21242	2.15142	0.30642
124	0.21137	2.08994	0.30565
125	0.21132	2.03785	0.30490
125	0.21078	2.36020	0.30415
127	0.21025	2.25614	0.30341
128	0.20972	2.17919	0.30341
129	0.20919	2.11671	0.30196
130	0.20867	2.06374	0.30124
131	0.20016	2.0374	0.30053
132	0.20765	2.28436	0.30053
133	0.20714		
134	0.20714	2.20624	0.29913
135	0.20615	2.14278	0.29844
136	0.20566	2.08897	0.29775
		2.41395	0.29708
137	0.20518	2.31187	0.29641
138 139	0.20470	2.23261	0.29574
140	0.20422	2.16820	0.29508
	0.20375	2.11357	0.29443.
141	0.20329	2.44723	0.29378
142	0.20282	2.33870	0.29314
143	0.20237	2.25834	0.29251
144 145	0.20191	2.19301	0.29188
140	0.20146	2.13758 2.47484	0.29126
147	0.20102	2.36490	0.29064
148	0.20058 0.20014		0.29002
149		2.28346	0.28942
150	0.19971 0.19928	2.21724 2.16104	0.28331
			0.28822
151	0.19385	2.50181	0.28763
152	0.19843	2.39050	0.28704
153 154	0.19801	2.30502	0.28646
	0.19759	2.24093	0.28588
155 156	0.19715 0.19678	2.13397	0.28531
157	0.19637	2.52819	0.28474
156	0.19597	2.41554 2.33204	0.28418 0.28362
159	0.19557	2.25410	
160	0.19513	2.20641	0.29307 0.29252
161	0.10479	2.55400	0.23197
162	0.19445	2.44004	
163	0.19401	2.35554	0.28143 0.28089
164	0.19353	2.28678	0.28036
165	0.19325	2.22837	0.27983
166	0.19288		0.27931
167	0.19251	2.57927 2.46404	0.27879
168	0.19214	2.37957	0.27827
159	C.19177	2.30899	0.27776
170	0.19141	2.24990	0.27725
171	0.19105	2.60403	0.27675
172	0.19069	2.48755	0.27625
173	0.19033	2.40113	0.27575
174	0.18998	2.33077	0.27526
	0 1 10 330	2000011	0.21260

175	0.18463	2.27099	0.27477
176	0.13924	2.02030	0.27428
177	0.18894	2.51060	0.27380
178	0.18859	2.42325	0.27332
179	0.18825	2.35212	0.27285
180	0.18792	2.29158	0.27239
181	0.13758	2.65211	0.27191
132	C.18725	2.53322	0.27144
183	0.18692	2.44496	0.27098
184	0.18659	2.37308	0.27052
135	0.18627	2.31198	0.27007
136	0.18594	2.67548	0.26961
187	C.18562	2.55542	0.26917
188	0.18530	2.46627	0.26872
189	0.18499	2.39365	0.26828
190	0.18467	2.33192	0.26784
191	0.18436	2.69842	0.26740
192	0.18405	2.57722	0.26696
193	0.18374	2.48720	0.26653
194	0.18344	2.41386	0.26611
195	0.18314	2.35150	0.26568
196	0.18283	2.72096	0.26526
197	0.18254	2.59864	0.26484
198	0.18224	2.50776	0.26442
199	0.18194	2.43371	0.26401
200	0.18165	2.37074	0.26359

MM M NSYS FAILR TIMP CREWS 5 10 10000 C.50000E-03 10.0000 10 0.80000 TI ET? TETR 1.00000 5.00000 5 Iλ R(IX) T(IX)AVGT(IX) J ATTTP(J) 1 10.00000 1.00000 1.00000 1 0.74755 2 12.50000 0.80000 0.90000 2 0.60774 3 14.24291 0.60774 0.70210 0.83403 3 4 15.62500 0.64000 C.78553 5 16.78973 0.59564 0.74755 6 13.90182 0.71933 0.74284 7 15.60472 0.64083 0.72827 9 0.59217 16.88707 0.71126 9 0.55693 17.95552 0.69411 10 18.88731 0.52946 0.67765 11 13.90182 0.71933 0.68144 12 15.60472 0.64083 0.67805 13 16.88707 0.59217 0.67145 14 17.95552 0.55693 0.66327 15 18.88731 0.52946 0.65434 13.90182 16 0.71933 0.55841 17 15.60472 0.64083 0.65737 18 16.89707 0.59217 0.65375 19 17.95552 0.55693 0.64865 20 18.38731 0.52946 0.64269 21 13.90192 0.71933 0.64634 22 15.60472 0.64083 0.64609 23 16.09707 0.59217 0.64375 17.95552 0.55693 24 0.64013 25 18.68731 0.52946 0.63570 25 13.90182 0.71933 0.63892 27 15.60472 0.64083 0.63899 28 16.88707 0.59217 0.63732 29 17.95552 0.55693 0.63455 30 18.88731 0.52946 0.63104 13.90182 31 0.71933 0.63389 32 15.60472 0.64083 0.53411 33 16.88707 0.59217 0.63294 34 17.95552 0.55693 0.63060 35 18.88731 0.52946 0.62771 36 13.90192 0.71933 C.63026 37 15.66472 0.64083 0.63054 38 16.88707 0.59217 0.62953 17.95552 0.55693 39 0.62767 40 18.38731 0.52946 0.62522 41 13.90182 0.71933 0.62751 42 15.60472 0.64083 0.62783 43 16.88707 0.59217 C. 62700 17.95552 0.62541 44 0.55693 45 18.88731 0.52945 0.62328 46 13.90162 0.71933 0.62536 47 15.60472 0.64093 0.62569 48 16.88707 0.59217 0.62499 49 17.95552 0.55093 0.62360 50 18.88731 0.52946 0.62172 51 13.90182 0.71933 0.62364 52 15.60472 0.64083 0.62397

53	16.88707	0.59217	0.62337
54	11.15552	0.55693	0.62214
55	18.88731	0.52946	C. 62045
56	13.57182	0.71933	0.62222
57	15.6047?	0.64083	0.62254
58	15.38707	0.59217	0.62202
59	17.95552	0.55693	0.62092
60	18.88731	0.52946	0.61939
61	13.90182	0.71933	0.62103
62	15.60472	0.64083	0.62135
63	16.88707	0.59217	0.62089
54	17.95552	0.55693	0.61989
65	18.98731		
		0.52946	0.61849
66	13.90182	0.71933	0.62002
67	15.60472	0.64083	C.62033
68	16.88707	0.59217	0.61992
69	17.95552	0.55693	0.61901
7 Ĺ	18.88731	0.52946	0.61773
71	13.90182	0.71933	0.61916
72	15.60472	0.64083	0.61946
73	16.88707	0.59217	0.61908
74			
	17.95552	0.55693	0.61824
75	18.88731	0.52946	0.61706
76	13.90182	0.71933	0.61841
77	15.60472	0.64083	0.61870
78	16.88707	0.59217	0.61836
79	17.95552	0.55093	C.61758
80	18.88731	0.52946	0.61648
81	13.90182	0.71933	0.61775
82	15.60472	0.64083	0.61803
83	16.88707	0.59217	0.61772
84	17.95552	0.55693	0.61699
85	15.88731	0.52946	0.61596
bć	13.90182	0.71933	0.61717
37	15.60472	0.64083	0.61744
88	16.68707	C.59217	0.61715
89	17.45552	0.55693	0.61647
90	18.88731	0.52946	
			0.61551
91	13.90182	0.71933	0.61665
92	15.60472	0.64083	0.61691
93	16.88707	0.59217	0.61664
94	17.95552	0.55693	0.61501
95	18.88731	0.52946	0.61510
96	13.40182	0.71933	0.61618
97	15.60472	0.64083	0.61644
98	16.88707	0.59217	0.61619
90	17.95552	0.55693	0.61559
100	18.88731	0.52946	0.61473
101	13.90182	0.71933	0.51577
102	15.50472	0.64083	0.61601
103	16.88707	0.59217	0.61578
104	17.95552	0.55693	0.61521
105	18.58731	0.52946	0.61440
	13.90182	0.71933	0.61539
106			
107	15.60472	0.64083	0.61563
108	16.88707	0.59217	0.61541
109	17.95552	0.55693	0.61487
110	18.38731	0.52946	C.61409
111	13.90182	0.71933	0.61504
112	15.60472	0.64083	0.61527
113	16.88707	0.59217	0.61507

114	17.95552	0.55693	0.61456
115		0.52946	0.6145
116 117	13.90132	0.71933 0.64083	0.61473
118	16.88707 17.95552	0.59217	0.61476
120	18.88731	0.55893	0.61427
121	13.90182	0.52946	0.61357
122	15.60472	0.71933	0.61444 0.61466
124	16.88707 17.95552	0.59217	0.61447
126	18.88731	0.52946	0.61333 0.61417
127	15.60472	0.64083	0.61438
128	16.88707	0.59217	0.61421
129	17.95552	0.55693	0.61377
130	18.88731	0.52946	0.61312
131	13.90182 15.60472	0.71933 0.64083	0.61393
133	16.88707	0.59217	0.61397
134	17.95552	0.556 9 3	
1,35 1,36	18.38731 13.90182	0.52946	0.61292
137	15.50472	0.64083	0.61390
138	16.88707		0.61374
139	17.95552 18.68731	0.55693 0.52945	0.61333
141	13.90182	0.71933	0.61349
142	15.60472		0.61368
143	16.88707 17.95552	0.59217	0.61353
145	18.88731	0.52946	C.61256
145	13.90182	0.71933	C.61329
147	15.5047?	0.64083	C.61348
148	15.88707	0.59217	O.61334
149 150	17.95552 18.83731	0.55693	0.61296
151 152	13.90182	0.71933	0.61240
153	16.88707	0.64033	0.61329
154	17.95552		C.61315
155	18.38731	0.55693	0.61279
156	13.90182	0.52946	0.61225
157	15.60472	0.71933	0.61294
155	16.88707	0.64083	
159	17.95552	0.59217	0.61298
150	19.38731	0.55693	0.61263
161 162	13.90182	0.52946	0.61211
153	15.60472	0.64083	0.61295
164	16.88707	0.59217	0.61282
165	17.95552	0.55693	0.61248
166	18.38731		0.51198
157	13.90182	0.71933	0.61262
158	15.60472		0.61279
169	16.88707	0.59217	0.61267
170	17.95552	0.55693	0.61234
171	18.98731	0.52946	0.61185
	13.90182	0.71933	0.61248
172	15.60472 16.38707	0.64083	0.61264 0.61253
174	17.95552	0.55693	0.61221

4110)

		*	
175 176	18.49721	0.52946	0.61173
177	13 1 32	0.71933	0.61235
175	15.50472	0.54083	0.61251
179	16.80707	0.59217	0.61239
	17.95452	0.55693	0.61208
180	18.99731	0.52946	0.61162
191	13.90182	0.71933	0.61222
182	15.60472	0.64083	0.61238
183	15.88707	0.59217	0.61226
184	17.95552	0.55593	0.61196
185	18.88731	0.52946	0.61152
136	13.40182	0.71933	0.61210
187	15.50472	0.64083	0.61225
189	16.38707	0.59217	0.61214
189	17.95552	0.55693	0.61185
190	18.88751	0.52946	0.61142
191	13.90182	0.71933	0.6119R
192	15.60472	0.64083	0.51213
193	16.38707	0.59217	0.61203
194	17.95552	0.55693	
195	18.88731	0.52946	0.61175
196	13.90182	C.71933	0.61132
197	15.00472	0.64083	0.61188
198	15.88707	0.59217	0.51202
199	17.95552		0.61192
200	16.88731	0.55693	0.61165
	1010101	0.52946	0.61123

мм 10	5 5	10000		FAILR OOF-03	TIMP 10.0000	CREWS 10	0.8000
	1.00000		FTR 5.00000	1E1R 5			
	11.000 TNO 0.00 TNO 0	100010043900110003107044375200300310704437520030031070443752003107043107043107043107044310704431070443107044310704431070443107443107044431070444310704443107044431070444310704443107044431070444310704444444444	FTR	151R	ATTPN: 0.74: 0.51: C.43	(J) 1 755 553	0.80000 ATDAN(J) 1.00000 1.17888 1.38428
43 44 45 46	0.2	9575 9362	1.98749 1.88311 1.80321 2.46727	0.42079 0.41795 0.41519 0.41250			
47 48 4,	0 • 2 · 0 • 2 · 0 • 2 ·	8954 6758 8558 8333	2.21229 2.05913 1.94950 1.86542	0.40988 0.40734 0.40485 0.40243			
51 52			2.55060 2.28651	0.40007			

	0.37.		
53	9. 27244	2.12588	0.39552
74	0.27	61144	0.39332
55	0.27525	1.92354	0.39117
56	0.27366	2.62487	0.39907
57	0.27210	2.35510	0.38702
58	0.27058	2.18848	0.38501
59	0.26910	2.06961	0.38305
50	0.26765	1.57818	0.38113
		-	
51	0.26623	2.70194	0.37924
52	0.26484	2.41972	0.37740
53			0.37559
	0.26348	2.24752	
54	0.26214	2.12452	0.37382
55	0.20034	2.02982	0.37208
66	0.25956	2.77134	0.37037
67	0.25831	2.48090	0.36870
68	0.25708	2.30346	0.36706
69	0.25537	2.17560	0.36545
70	0.25459	2.C7883	0.36386
71	0.25353	2.83727	0.36231
			-
72	0.25239	2.53905	0.36078
73	0.25127	2.35668	0.35928
74	0.25017	2.27613	0.35781
75	0.24910	2.12552	0.35630
76	0.24804	2.90011	0.35493
77	0.24699	2.59453	0.35353
78	0.24577	2.40749	0.35215
79	0.24495	2.27353	0.35080
30	0.24347	2.17014	0.34946
31	0.24300	2.96021	0.34815
82	0.24204	2.64761	0.34685
93	0.24110	2.45613	0.34558
54	C.24017	2.31890	0.34432
35	0.23926	2.21291	0.34309
80	0.23836	3.01785	0.34187
37	0.23747	2.69854	0.34067
8 3	0.23660	2.50282	0.33949
39	0.23574	2.36246	0.33832
90	0.23490	2.25400	0.33717
91	0.23406	3.07325	0.33604
32	0.23324	2.74753	0.33492
93	0.23243	2.54774	
			0.33392
74			0.33382
	0.23163	2.40440	0.33382 0.33273
95		2.40440	0.33273
95	0.23084	2.40440 2.29358	0.33273 0.33166
96		2.40440	0.33273
96	0.23084 0.23007	2.40440 2.29358 3.12663	0.33273 0.33166 0.33060
96 97	0.23084 0.23007 0.22930	2.40440 2.29358 3.12663 2.79474	0.33273 0.33166 0.33060 0.32956
96	0.23084 0.23007	2.40440 2.29358 3.12663 2.79474 2.59106	0.33273 0.33166 0.33060
96 97 98	0.23084 0.23007 0.22930 0.22854	2.40440 2.29358 3.12663 2.79474 2.59106	0.33273 0.33166 0.33060 0.32956 0.32853
96 97 98 99	0.23084 0.23007 0.22930 0.22854 0.22740	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485	0.33273 0.32166 0.33060 0.32956 0.32853 0.32751
96 97 98	0.23084 0.23007 0.22930 0.22854	2.40440 2.29358 3.12663 2.79474 2.59106	0.33273 0.33166 0.33060 0.32956 0.32853
96 97 98 99	0.23084 0.23007 0.22930 0.22854 0.22780 0.22706	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650
96 97 98 99 00	0.23084 0.23007 0.22930 0.22854 0.22740 0.22706 0.22634	2.40440 2.29358 3.12663 2.79474 2.59196 2.44485 2.33177 3.17815	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551
96 97 98 99	0.23084 0.23007 0.22930 0.22854 0.22780 0.22706	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650
96 97 98 99 00 01	0.23084 0.23007 0.22930 0.22740 0.22706 0.22634 0.22662	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551 0.32453
96 97 98 99 00 01 02	0.23084 0.23007 0.22930 0.22854 0.22740 0.22706 0.22634 0.22634 0.22634	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033 2.63290	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551 0.32453 0.32356
96 97 98 99 00 01 02	0.23084 0.23007 0.22930 0.22740 0.22706 0.22634 0.22662	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551 0.32453
96 97 98 99 00 01 02	0.23084 0.23007 0.22930 0.22790 0.22796 0.22634 0.22634 0.226491 0.22421	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033 2.63290 2.48394	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551 0.32453 0.32356 0.32261
96 97 98 99 00 01 02 03 05	0.23084 0.23007 0.22930 0.22854 0.22790 0.22706 0.22634 0.22634 0.22421 0.22421	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033 2.63290 2.48394 2.36868	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551 0.32453 0.32356 0.32261 0.32167
96 97 98 99 00 01 02 03 04 05 06	0.23084 0.23007 0.22930 0.22790 0.22796 0.22634 0.22634 0.22491 0.22421 0.22352 0.2284	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033 2.63290 2.48394 2.36868 3.22798	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551 0.32453 0.32356 0.32261 0.32167 0.32073
96 97 98 99 00 01 02 03 04 05 06	0.23084 0.23007 0.22930 0.22790 0.22796 0.22634 0.22634 0.22491 0.22421 0.22352 0.2284	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033 2.63290 2.48394 2.36868 3.22798	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551 0.32453 0.32356 0.32261 0.32167 0.32073
96 97 98 99 001 003 004 007	0.23084 0.23007 0.22930 0.22740 0.22796 0.22796 0.22634 0.22634 0.22421 0.22421 0.22352 0.22284 0.22217	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033 2.63290 2.48394 2.36868 3.22798 2.88443	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551 0.32453 0.32356 0.32261 0.32167 0.32073 0.31991
96 97 98 99 001 003 007 007	0.23084 0.23007 0.22930 0.22790 0.22796 0.22634 0.22634 0.22634 0.22421 0.22421 0.22352 0.22284 0.22217	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033 2.63290 2.48394 2.36868 3.22798 2.88443 2.67339	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551 0.32453 0.32356 0.32261 0.32167 0.32073 0.31991 0.31890
96 97 98 99 001 003 007 007	0.23084 0.23007 0.22930 0.22790 0.22796 0.22634 0.22634 0.22634 0.22421 0.22421 0.22352 0.22284 0.22217	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033 2.63290 2.48394 2.36868 3.22798 2.88443 2.67339	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551 0.32453 0.32356 0.32261 0.32167 0.32073 0.31991
967 98 99 001 003 007 007 007 009	0.23084 0.23007 0.22930 0.22790 0.22796 0.22634 0.22634 0.2262 0.22421 0.22352 0.22284 0.22217 0.22151 0.22085	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033 2.63290 2.48394 2.36868 3.22798 2.88443 2.67339 2.52178	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551 0.32453 0.32356 0.32361 0.32167 0.32167 0.32167 0.32167 0.32167 0.32167 0.32167 0.32167
967 98 90 90 90 90 90 90 90 90 90 90 90 90 90	0.23084 0.23007 0.22930 0.22790 0.22796 0.22634 0.22634 0.226491 0.22421 0.22352 0.22284 0.22217 0.22151 0.22020	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033 2.63290 2.48394 2.36868 3.22798 2.88443 2.67339 2.52178 2.40442	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551 0.32453 0.32356 0.32261 0.32167 0.32167 0.31991 0.31890 0.31800 0.31711
967 98 90 90 90 90 90 90 90 90 90 90 90 90 90	0.23084 0.23007 0.22930 0.22790 0.22796 0.22634 0.22634 0.2262 0.22421 0.22352 0.22284 0.22217 0.22151 0.22085	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033 2.63290 2.48394 2.36868 3.22798 2.88443 2.67339 2.52178	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551 0.32453 0.32356 0.32361 0.32167 0.32167 0.32167 0.32167 0.32167 0.32167 0.32167 0.32167
967 98 99 90 90 90 90 90 90 90 90 90 90 90 90	0.23084 0.23007 0.22930 0.22954 0.22790 0.22706 0.22634 0.22634 0.22421 0.22421 0.22352 0.22284 0.22217 0.22151 0.22020 0.21956	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033 2.63290 2.48394 2.36868 3.22798 2.88443 2.67339 2.52178 2.40442 3.27623	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551 0.32453 0.32356 0.32356 0.32167 0.32073 0.31890 0.31890 0.31711 0.31623
967 997 990 900 900 900 900 900 900 900 90	0.23084 0.23007 0.22930 0.22954 0.22790 0.22706 0.22634 0.22634 0.22421 0.22421 0.22352 0.22284 0.22217 0.22151 0.22085 0.22020 0.21956 0.21893	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033 2.63290 2.48394 2.63290 2.48394 2.52798 2.88443 2.67339 2.52178 2.40442 3.27623 2.92715	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551 0.32453 0.32356 0.32356 0.32261 0.32167 0.32073 0.31991 0.31890 0.31711 0.31623 0.31537
967 98 99 90 90 90 90 90 90 90 90 90 90 90 90	0.23084 0.23007 0.22930 0.22954 0.22790 0.22706 0.22634 0.22634 0.22421 0.22421 0.22352 0.22284 0.22217 0.22151 0.22020 0.21956	2.40440 2.29358 3.12663 2.79474 2.59106 2.44485 2.33177 3.17815 2.84033 2.63290 2.48394 2.36868 3.22798 2.88443 2.67339 2.52178 2.40442 3.27623	0.33273 0.33166 0.33060 0.32956 0.32853 0.32751 0.32650 0.32551 0.32453 0.32356 0.32356 0.32167 0.32073 0.31890 0.31890 0.31711 0.31623

114	0. 71 1t.	2.55445	0.31366
115	0.2.	43000	0.31282
110	0.2164	5. 32 (13	0.31199
117	0.21547	2,56959	
			0.31116
118	C.21528	2.75070	0.31035
119	C.21470	2.50465	0.30955
120	0.21412	2.47213	0.30375
121	0.21355	1. 36 RA9	0.30797
1.22	0.21298	3. CCA86	0.30719
123	0.21242	2.78709	0.30642
124	0.21147	2.62865	0.30565
125	0.21132	2.50544	
126			0.30490
	0.21078	3.41268	0.30415
127	0.21025	3.04802	0.30341
128	0.20972	2.82368	0.30268
129	0.20919	0.66232	0.30196
130	0.20867	2.53727	0.30124
131	0.20816	3.45571	0.30053
132	0.20755	3.C8614	0.25982
133	0.20714	2.85373	0.29913
134	0.20555	2.69511	0.29844
135	0.20615	2.56829	0.29775
130	0.20565	3.49763	0.29708
137	0.20518	3.10110	0.29641
138	0.20477	2. 492 19	0.29574
139	0.20.22	2.72708	0.29508
140	0.203/5	2.50253	0.29443
141	0.20329	3.53852	0.29378
1+2	0.20232	3.15955	
			0.29314
143	0.20237	2.92623	0.29751
144	0.2019.	1.75429	0.29188
145	0.20145	2.62806	0.29125
146	0.20102	3.57844	0.25064
147	0.20058	3.19495	0.29002
148	0.20014	2.95879	0.28942
149	0.19971	2.78876	0.23881
150	0.10028	2.65689	0.28822
151	0.19535	3.61744	C.28743
152	0.19843	3.22954	0.28/04
153	0.19801	2.99061	0.29646
154	0.19759	2.01355	
155	0.19718	2.68509	0.28588
156	0.19678		0.28531
157		3.65558	0.28474
	0.19657	3.26336	0.28418
158	0.19597	3.02173	0.28362
159	0.19557	2.84769	0.28307
100	0.19514	2.71268	0.29252
161	0.19479	3.69290	0.23197
162	0.19440	3.29647	0.25143
153	0.19401	3.05219	0.28089
154	0.19363	2.47622	0.28036
165	C.19325	2.73968	0.27983
155	0.19288	3.72943	0.27931
157	0.19251	3.32889	0.27879
158	0.19214	3.08202	0.27827
159	0.19177	2.90416	
170			0.27776
	0.19141	2.76614	0.27725
171	0.19105	3.76574	0.27675
172	0.19069	3.36065	0.27625
173	0.19033	3.11125	0.27575
174	0.18998	2.93155	0.27526

175	0.18941	2.79207	0.27477
176		1.40033	0.27428
177	0. 10: 40	1.39179	0.27380
178	C.18851	3.13992	0.27332
179	0.19825	2.95841	0.27285
180	0.18792	2.81751	0.27238
181	0.18758	3.83476	0.27191
132	0.18725	3.42235	0.27144
184	0.18692	3.16805	0.27098
154	0.18659	2.98477	0.27052
185	0.18627	2.84247	0.27007
156	0.18594	3.86855	0.26961
187	0.18562	3.45234	0.26917
138	0.18530	3.19566	0.26372
189	0.18499	3.01064	0.26828
190	0.18457	2.86698	
191			0.26784
	0.18436	3.90173	0.26740
192	0.13405	3.46179	0.26696
193	C.18374	3.22278	0.26653
194	0.18344	3. C3605	0.26611
195	0.18314	2.89105	0.26568
196	0.18283	3. 93432	0.26526
197	0.15254	3.51073	0.26484
198	0.18224	3.24942	0.26442
199	0.18194	3.06102	0.26401
200	0.18165	2.91471	0.26359

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TI ETA IETR 1.00000 5.00000 5

1.	90 JUG	5.00000	5		
•	0 - 1 11 1	* 4 * * * *			
IX	8 (14)		AVGT(IX)	J	ATTTP(J)
1	50.00000		1.00000	1	0.74755
2	62.50000		0.90000	2	0.53146
3	71.21454		0.83403	3	0.46451
4	79.12493		0.78553	4	C.42891
5	93.44308		0.74755	5	0.40694
Č:	87.11615	0.53743	0.72086	6	0.39254
7	90.44246	0.55284	0.69686	7	0.38295
9	95.01204	0.52625	0.67553	8	0.37673
Q	40.00013	0.50454	0.65653	9	0.37304
1 C	102.43099	0.45023	0.63950	10	0.37136
1.1	100.46106	0.49771	0.62661	11	0.37136
12	104.52299	0.4779]	0.61422		
1.3	103.02888	0.46198	0.60251		
14	111. 0270	0.44842	0.59150		
15	114.33551	0.41655	0.58117		
16	110.17094		0.57321		
17	113.86526				
18	117.05624	2.42715	0.55765		
19	119.95856		0.55024		
20	122.65014	0.40764	0.54311		
21	116.87181		0.53762		
22	120.32890		0.53207		
23	123.30246		0.52656		
24	125.00484		0.52116		
25	128.51804		0.51587		
26	121.61336		0.51185		
27	124.93755		0.50771		
28	127.78708		0.50355		
29	130.37338	0.38351	0.49941		
30	132.77773	0.37557	0.49532		
31	124.93922	0.40019	0.49225		
32	124.1 0623	0.39006	0.48906		
33	130.46232	9.36179	0.48581		
34	133.48021	0.37459	0.48253		
3.5	135.91918		0.47927		
36	127.1/381				
37	130.37650				
38	133.11102				
39	135.58821				
40	137.5HH75		0.46145		
41	128.52902		0.46456		
42	131.70834				
43	134.42041				
4.4	136.87604		0.45827		
45	139.15596		0.45607		
46	124.15271		0.45457		
47	132.32249		0.45294		
4 P	135.02533		0.45122		
49	137.47211		0.44943		
5 C	139.74345		0.44760		
51	129.15271				
52	132.32248	0.37786	0.44509		

53	135. 12 - 3	0.17030	0.44368
	· Is		
Э н		7 71	0.44720
55	1 3 2 4 4 4 4 5	0. 25/90	0.44067
56	129.15271	0.20114	0.43971
57	132.32248	0.37786	0.43863
58	135.02534	0.37030	0.43745
54	137.47211	0.36371	0.43620
60	1:9.74345	0.35780	0.43489
61	129.15271	0.38714	0.43411
62	132.32248	0.37786	0.43320
53	135.02533	0.37030	0.43220
64	137.47211	0.36371	0.43113
65	137.74345	0.35780	0.43000
6.5			
66	129.15271	0.38714	0.42935
67	132.37248	0.27786	0.42859
68	135.02533	0.37030	0.42773
59	137.47211	0.36371	0.42680
70	139.74345	0.35780	0.42581
71	129.15271	0.38714	0.42527
72	132.32242	0.37786	0.42461
73	135.02533	7.37037	0.42387
74	137.47211	0.36371	0.42305
75	139.74345	0.35780	0.42218
76	129.15271	0.38714	0.42172
77	132.32248	0.27786	0.42115
78	135.02533	0.37030	C.42050
79	137.47211		0.41978
		C.36371	
80	139.74345	0.35780	0.41901
31	129.15271	6.38714	C. 41961
82	132.32245	0.37786	2.41812
33	135.02533	0.37030	0.41754
84	137.47211	0.36371	0.41690
35	139.74345	0.35780	0.41620
86	129.15271	0.38714	0.41587
37	132.32248	C.37785	0.41543
.58	135.02533	0.37030	0.41492
89	137.47211	0.36371	0.41434
90	139.74345	0.35780	0.41371
91	129.15271	0.38714	0.41342
92	132.32248	0.37786	0.41303
93	135.02533	0.37030	0.41257
94	137.47211	0.36371	0.41205
95	139.74345	C. 35780	0.41148
96	129.15271	0.38714	0.41123
97	132.32248	0.37786	0.41089
98	135.02533	0.37030	C.41047
			C.41000
33	137.47211	0.36371	
100	139.74345	0.35780	0.40948
101	129.15271	0.39714	0.40926
102	132.32248	0.37780	0.40895
103	135.02533	0.37030	0.40857
			0.40814
104	137.47211	0.36371	
105	139.74345	0.35780	0.40766
106	129.15271	0.39714	0.40747
107	132.32248	0.37786	0.40719
138	135.02533	0.37030	0.40685
	137.47211	0.36371	0.40645
109			
110	139.74745	0.35780	0.40601
111	129.15271	0.38714	0.40584
			0.40559
112	132.32248	0.37786	
113	135.02533	C.37030	0.40528

114	137.	0.36371	0.40491
115	W .	• 180	0.4645
116	1.7	C. 3114	0.40435
117	137.5.748	0.37750	0.40413
118	145.0,5,3	. 37030	0.40384
110	13/04/211	1.311	0.40350
130	139.743.5	0.25780	0.40312
121	129.15.71	0.28714	0.40299
122	132.32768	0. 27786	0.40279
123	135.02.32	0.37030	0.40252
124	137.4/211	0.363/1	0.40221
125	139.74945	0.35730	0.40185
:26	129.15071	0.38714	C. 40174
127	1 2.32248	0.37766	0.40155
128		0. 37039	
	135.02533		0.40130
129	137.47211	6.35371	0.40101
130	139.74245	0.35780	0.40068
131	129.15271	33/14	0.40058
137	192.32248	0.37756	0.40040
133	136.02533	7.37630	C.40018
1 34	137.47211	6.311	r. 39991
135	139.74345	0.34/30	0,39950
136	1, 9, , 5271	(7) 4	2.30050
137	132.323.5	0.37786	0.39934
138	135.32533	0.37027	0.399 13
130	137.47211	(. 20371	0.39988
1 - C	139.74345	0.1700	0.39859
141	129.15271	0.1.714	0.39450
142	132.32244	7 ? 71.6	C.39836
1+3	135.02573	0.37(10)	C. 39916
144	137.47211	0.35511	1.39792
145	139.74345	5.35730	0.39765
146	121.15271	0.38/14	0.39757
		5. 17786	
147	132.32245		0.39744
143	136.02637	· · · 7030	0.39726
149	137.47231	0.36371	0.39703
_			
150	130, 76.345	0.35780	0.39677
151	126.14271	1.38714	0.39571
		0.37786	0.39658
152	132. 12244		
. 50	135.02574	U. 47030	0.39641
154	137.4 / / 11	0.36371	0.39620
155	129.74345	0.35780	0.39595
156	129.15271	0.34714	0.39589
157	137.12245	0.37786	0.39578
158	134.02533	(. 47030	0.39562
159	137.47211	9. 44 3 71	0.39542
150	134,74244	0.35740	0.39518
151	129.15.271	0.54714	0.39513
152	122.3724	0.31136	0.39503
163	1:5.02533	0.37030	0.39487
154	137.47211	(.36371	0.35468
165	1:5.14:45	1. 46 180	C. 39440
166	120.15.71) . 1 . 714	0.39442
167	132.32249	0.57786	6.39432
154	135.025-3	(7r∋0	0.39417
1 5 0	137.47211	1.26771	0.34399
176	144,74345	0.35780	0.39378
171	129.15271	0.33714	0.39374
172	132.32248	6.37786	0.39365
173	135.02533	0.27030	0.39351
174	137.47211	0.36371	0.39334

175	137. 43.	0.34780	0.39314
175	1	. 11/14	6.35211
177	132.327	0.37786	0.39302
178	124.324.33	0.37030	0.39289
179	137.47211	0.36371	0.39273
130	139.74345	(. 35780	0.39253
131	129.15271	C.38714	0.39250
192	132.32248	0.37786	0.39242
153	135.02533	0.37030	0.39230
184	137.47211	0.36371	0.39215
185	139.74345	0.35780	0.39196
135	129.15271	0.38714	0.39194
157	132,32248	0.37796	0.39186
199	135.02533	0.37030	0.39175
159	137.47211	0.36371	0.39160
190	139.74345	0.35780	0.39142
191	129.15271	0.38714	0.39140
192	132.32248	0.21786	0.39133
193	135.02533	0.37030	0.39122
194	137.47211	0.56371	0.39108
195	139.74345	0.35780	C.39091
196	129.15271	0.38714	0.39089
197	132-32748	0.37780	C.39082
198	135.02533	0.37030	c.39072
199	137.47211	0.36371	0.39058
200	139.74345	0.35780	0.39042

1 1.00000 1.00000 1.00000 0.74755 1.00 2 0.80000 1.00000 0.90000 0.51553 1.03 3 0.70210 1.00000 0.83403 0.43903 1.05 4 0.64000 1.00000 0.78553 0.39488 1.06 5 0.59564 1.00000 0.74755 0.36473 1.11 6 0.56168 1.04584 0.71657 0.34226 1.14 7 0.53448 1.03433 0.69056 0.32458 1.17 8 0.51200 1.02753 0.66824 0.31014 1.21 9 0.49295 1.02552 0.54876 0.29802 1.25 10 0.47651 1.02041 0.63154 0.28764 1.29	Q 0.80000
1 1.00000 1.00000 1.00000 0.74755 1.00 2 0.50000 1.00000 0.90000 0.51553 1.03 3 0.70210 1.00000 0.63403 0.43903 1.05 4 0.64000 1.00000 0.78553 0.39488 1.08 5 0.59564 1.00000 0.74755 0.36473 1.11 6 0.56168 1.04594 0.71657 0.34226 1.14 7 0.53449 1.03433 0.69056 0.32458 1.17 8 0.51200 1.02783 0.66824 0.31014 1.21 9 0.49295 1.02352 0.54976 0.29802 1.25 10 0.47651 1.02041 0.63154 0.28764 1.29 11 0.46211 1.07702 0.51613 0.27859 1.33 12 0.44935 1.06356 0.50224 13 0.43792 1.05496 0.59950 14 0.42759 1.04871 0.55761 17 0.40168 1.09319 0.54834 18 0.39436 1.0635 0.56737 16 0.40950 1.10371 0.55761 17 0.40168 1.09319 0.54834 18 0.39436 1.05313 0.53979 19 0.38756 1.07549 0.53178 20 0.38121 1.06934 0.52425 21 0.37527 1.14004 0.51715 22 0.36969 1.12399 0.51045 23 0.36444 1.11270 0.56410 24 0.35948 1.10385 0.49808 25 0.35478 1.09658 0.49234 26 0.35933 1.17357 0.46688 27 0.34507 1.14383 0.47668 29 0.33823 1.13288 0.47191 30 0.33456 1.12597 0.46733 31 0.33456 1.12597 0.46733 31 0.33456 1.12597 0.46733 31 0.33456 1.12597 0.46733	
33	
41 0.30155 1.28579 0.42673 42 0.30021 1.26452 0.42372 43 0.29795 1.24843 0.42679 44 0.29575 1.23514 0.41795 45 0.29302 1.22372 0.41519 46 0.29155 1.32787 0.41250 47 0.28954 1.30506 0.40988 48 0.28758 1.28764 0.40734 49 0.28556 1.27314 0.40485 50 0.28363 1.26062 0.40007	

	V		
53	0.3785	1.32.27	0.39552
÷ •			
		11	0.39332
55	0.275.	1.00000	0.39117
56	0.27305		
		1-41403	0.38907
57	0.27216	1. 74863	0.38702
5.8	0.27043		
		1.36357	0.38501
54	0.26911	1.35158	0.38305
50	0.25705		
		1.23693	0.38113
01	0.26623	1.45417	0.37924
52	0.25484	1.42678	
			0.37740
o 3	C.25348	1.40544	0.37559
64	0.25214	1.33744	
			0.37392
65	0.26034	1.37172	0.37208
60	0.25956	1.49152	0.37037
57	0.25831	1.46 285	C•36870
68	C.25708	1.44042	0.36706
59	∂.2558 7	1.42145	0.36545
70	0.25459	1.40484	0.36386
71			
	0.25353	1.52700	0.36231
72	0.25239	1.49714	0.36078
73	0.25127	1.47370	0.35928
74	0.25017	1.45383	C.35781
75			
	0.24910	1.435 9	0.35636
76	0.24304	1.56052	0.35493
77	0.246,99		
		1.52936	0.55353
78	0.24597	1.50547	0.35215
79	0.24495		
		1.43475	0.35080
30	0.24397	1.46655	0.34946
31	3.24300		
		1.59317	0.34815
82	0.24204	1.50110	0.34685
33	0.24110		
		1.53599	0.34558
84	0.24017	1.51438	0.34432
35	0.23925		
		1.49545	0.34309
56	0.23830	1.62418	0.34187
37	0.23747	1.59119	
			0.34067
86	0.23660	1.56508	0.33949
39	0.23574	1.54283	
			0.33832
90	0.23490	1.52322	0.33717
91	0.23406	1.65401	
			0.33604
92	0.23324	1.52007	C.33492
93	0.23243	1.59318	0.33382
94	0.23163	1.57022	0.33273
95	0.23084	1.54997	0.33166
96			
	0.23007	1.69273	0.33060
97	0.22933	1.64791	0.32956
98	0.22854	1.62027	
			0.32853
99	0.22737	1.59654	0.32751
.00	0.22700	1.575/8	
			0.32650
.01	0.22534	1.71046	0.32551
0.2	0.22562	1.67479	
			0.32453
. 33	3.22491	1.54643	0.32356
.04	0.22421	1.62216	0.32261
05	0.22352	1.60072	0.32167
36	0.22284	1.73/28	0.32073
27	0.23217	1.70079	0.31981
0.8	C. 22151	1.67175	0.31490
59	0.22035		
		1.64687	0.31800
10	0.22023	1.62487	0.31711
11	0.21956	1.76325	
			0.31623
12	0.21493	1.72598	0.31537
13	0.21830	1.69626	
•	(• C * O) A	4 0 70 2 0	0.31451

114	2.217	1.67082	0 31366
			0.31366
115	2.7.7.	64039	0.31282
116	0.21541	1.79443	0.31199
117	0.21507	1.75042	0.31116
118	0.21528	1.72009	0.31035
119	0.21470	1.69407	
			0.30455
120	0.21412	1.67103	0.30875
121	0.21355	1.81290	0.30797
122	0.21299	1.77416	0.30719
123	0.21242	1.74323	0.30642
124	0.21187		
		1.71667	0.30565
125	0.21132	1.69314	0.30490
126	0.21078	1.83668	0.30415
127	0.21025	1.79725	0.30341
128	0.20972	1.76573	0.30268
129	0.20919	1.73865	0.30196
130	0.20867	1.71465	0.30124
131	0.20816	1.85984	0.30053
137	0.20765	1.81974	0.29982
133	0.20714	1.78765	0.29913
134	0.20665	1.76007	0.29944
135	0.20615	1.73551	0.29775
136	0.20565	1.89246	0.29709
137	0.20518	1.84165	0.29641
130	0.20470	1.80901	0.29574
139	0.20422	1.78095	0.29518
140	0.20375	1.75605	0.29443
141	0.20329	1.90441	0.29378
142	0.20282	1.86302	0.29314
143	0.20237	1.82986	0.29251
144	0.20191	1.80133	0.29188
145	0.20146	1.77600	0.29126
146	0.20102	1.52589	0.29064
147			
	0.20053	1.88389	0.29002
148	0.20014	1.85022	0.28942
1+9	0.19971	1.82123	0.28881
150	0.19923	1.79549	0.28822
151	0.19885	1.94688	0.28763
152	0.19843	1.90429	0.28704
153	0.19861	1.87011	0.28646
154	0.19759	1.84069	0.28588
155	0.19718	1.81454	0.28531
156	0.19678	1.95741	0.28474
157	0.19637	1.92423	0.28418
158	0.19597	1.88957	0.28362
159	0.19557	1.85972	0.28307
150	0.19518	1.83319	0.28252
161	0.19479	1.98749	0.28197
162	0.19440	1.94375	0.28143
163	C.19401	1.90862	0.24089
154	0.19363	1.87934	C.28036
165	0.19325	1.85143	0.27983
166	0.19283	2.CC716	0.27931
157	0.19251	1.96287	0.27879
168	0.19214	1.92728	0.27827
169	0.19177	1.89659	C.27776
170	0.19141	1.86931	0.27725
171	0.19105	2.02642	0.27675
172	0.19059	1.93160	0.27625
173	0.19033	1.94556	0.27575
174			
114	0.18998	1.91448	0.27526

175	9. 130b	1.83684	0.27477
176	0.1.1.	1.045:1	0.27428
177	0.19844	1.99996	0.27380
178	0.16859	1.96349	0.27332
179	0.18835	1.93202	0.27285
180	0.18792	1.90403	0.27239
181	0.18758	2.00384	0.27191
182	0.18725	2.01798	0.27144
183	0.18692	1.98107	0.27098
184	0.14659	1.94923	0.27052
135	0.18627	1.92090	0.27007
lee	0.18594	2.08203	C.26961
187	0.13562	2.03566	0.26917
188	0.18530	1.99534	0.26872
189	0.18499	1.96613	0.26828
190	0.18467	1.93746	0.26784
191	0.18436	2.09988	0.26740
192	0.18405	2.05303	0.26696
193	0.15374	2.01530	0.26553
194	0.19344	1.98273	0.26611
195	0.18314	1.95373	0.26568
196	0.18283	2.11742	0.26526
197	0.18254	2.07009	0.26484
198	0.18224	2.03196	C.26442
199	0.18194	1.99903	0.26401
200	0.18165	1.96972	0.26359

MM 50	M VSVS 10 10000	FAIL 0.5000CE-0		CREWS 10	0.80000
1	TI 00 000c .1	ETR 1E	TR 5		
	ŢŢ	ETR 1E 5.00000 1 (1X) 1.00000 0.80000 0.80000 0.80000 0.70210 0.64000 0.59564 0.61565 0.51249 7.0.541669 9.0.531088 7.0.49636 7.0.49636 7.0.49638 7.0.49638 7.0.49638 7.0.49638 1.0.49749 0.49749	TR	J Å	0.8C000 ATTTP(J) 0.74755 0.54850 0.49328 0.46955 0.46046 0.46046
45 46 47 48 49 50	116.1052 100.5052 105.4090 109.4067 112.9188 116.1052	2 0.49749 0 0.47434 8 0.45701 1 0.44280	0.50679 0.50659 0.50590 0.50489 0.50362 0.50216		
51 52	100.5052	0.49749	0.50210 0.50207 0.50153		

-			
53	1 0 9. คือไล	0.45701	0.50069
54	1	8.4230	0.49962
55	110.10.20	0.43064	0.49837
56	100.50522	0.49749	
			0.49935
57	105.40900	0.47434	0.49793
56	109.40578	0.45701	
			0.49722
50	112.91331	0.44289	0.49630
6 C	116.10526	0.43064	0.49521
61	100.50522	0.49749	0.49524
52	105.40900	0.47434	0.49491
63	109.40678		
		0.45701	0.49431
64	112.91881	0.44280	0.49350
55	116.10526	0.43064	0.49253
65	100.50522	0.49745	0.49261
57	105.40900	0.47434	0.49234
68	109.40578		
		0.45701	0.49182
59	112.91881	0.44280	0.49111
70	116.10526	0.43064	0.49024
71	100.50523	0.49749	0.49034
72	105.40900	0.47434	6.49012
73	109.40578	0.45701	0.48967
74	112.91891	C. 44280	0.48903
75			
	116.10526	0.43064	0.48826
76	100.50522	0.49749	0.48838
77	105.40900	0.47434	
			9.48819
78	109.40679	0.45701	0.48779
79	112.91831	0.44280	0.48723
3.0	116.10526	0.43064	0.48652
31	100.50522	0.49749	0.48665
82	105.40900		
		0.47434	0.48650
83	109.40678	0.45701	0.43615
34	112.91981	0.44280	
			0.48563
85	116.10525	0.43064	0.48498
96	100.50522	0.49749	0.48513
87	105.40900	0.47434	0.48501
38	109.40678	0.45701	0.48469
89	112.91881		
		0.44280	0.48422
9C	116.10526	0.43064	0.48362
91	100.5052?	0.49749	0.48377
92	105.40900	0.47434	0.48367
93	109.40678	0.45701	0.48338
94	112.91831	0.44280	0.48295
95	116.10526	0.43064	0.4824C
96	100.50522	0.40749	0.48256
97	105.40900	0.47434	0.48247
98	109.40678	0.45701	0.48221
90		_	
	112.91881	0.44280	0.48182
100	116.10526	0.43064	0.48130
101	100.50522	0.49749	
			C.49146
102	105.40900	0.47434	0.48139
103	109.40678	0.45701	0.48116
174	112.91831	0.44280	0.48079
105	116.10526	0.43064	0.48031
106	100.50522		
		0.49749	0.48047
107	105.40900	0.47434	C. 48042
100	109.40579	0.45701	0.48020
109	112.91881	0.44280	C.47986
110	116.10526	0.43064	0.47941
111	100.50522		
		0.49749	0.47957
112	105.40900	0.47434	0.47952
113	109.40578	0.45701	0.47932
	,,,,,,,,		35 TT /36

114	112,01981	0.44280	0.47900
115			
		0.43064	0.47358
116	100,50,22	0.49749	0.47875
117	105.40900	0.47434	0.47871
118	109.40679	0.45701	0.47853
119	112.91881	0.44280	0.47822
120	116.10526	0.43064	0.47783
121	100.50522	0.49749	0.47799
122	105.40900		
		0.47434	0.47796
123	109.40678	0.45701	0.47779
124	112.91881	0.44280	0.47751
125	116.10526	0.43064	C.47713
126	100.50522	0.49749	0.47729
127	105.40900	0.47434	0.47727
128	109.40678	0.45701	0.47711
129	112.91881	0.44280	0.47685
130			
	116.10526	0.43064	0.47649
131	100.50522	0.49749	0.47665
1.32	105.40900	0.47434	0.47663
133	109.40678	0.45701	0.47649
134	112.91881	0.44280	0.47623
135	116.10526	0.43064	0.47590
136	100.50522	0.49749	0.47606
137	105.40900	0.47434	0.47604
138	109.40678	0.45701	0.47591
139	112.91881	0.44280	0.47567
140	116.10526	0.43064	0.47535
141	100.50522	0.49749	0.47550
142	105.40900	0.47434	0.47549
143	109,40578	0.45701	0.47536
144	112.91881	0.44280	0.47514
145	116.10526	0.43064	0.47483
146	100.50522	0.49749	0.47499
147	105.40906	0.47434	0.47498
148	109.40678	0.45701	0.47486
149	112.91881	0.44280	0.47465
150	116.10526	0.43064	C.47435
151	100.50522	0.49749	0.47451
152	105.40900	0.47434	0.47450
153	109.40678	0.45701	0.47439
154	112.91881	0.44280	0.47418
155	116.10526	0.43064	0.47390
156	100.50522	0.49749	C.47406
157	105.40900	0.47434	0.47406
156	109.40678	0.45701	0.47395
159	112.91881	0.44280	0.47375
100	116.10520	0.43064	0.47348
161	100.50522	0.49749	0.47363
162	105.40900	0.47434	0.47364
	109.40678	0.45701	0.47353
163			_
154	112.91881	0.44280	0.47335
165	116.10526	0.43064	C. 47309
166	100.50522	0.49749	0.47324
167	105.40900	0.47434	0.47324
168	109.40578	0.45701	0.47315
169	112.91881	0.44280	0.47297
170	116.10526	0.43064	0.47272
171	100.50522	0.49749	0.47286
172	105.40900	0.47434	0.47287
173	109.40678	0.45701	0.47278
174	112.91881	0.44280	0.47261

175	114 10000		
	116.16126	0.43064	0.47237
176	11110 . 11 15, 2	0.49749	0.47251
177	105.40900	0.47434	0.47252
178	109.40578	0.45701	0.47243
179	112.91881	0.44280	0.47227
180	116.10526	0.43064	0.47204
181	100.50522	0.49749	
182	105.40900	0.47434	0.47218
183	109.40678	0.45701	0.47219
184	112.91881		0.47210
135	116.10526	0.44280	0.47195
186	100.50522	0.43064	0.47172
167		0.49749	0.47186
188	105.40900	0.47434	0.47187
189	109.40678	0.45701	0.47179
	112.91881	0.44280	0.47164
190	116.10526	0.43064	0.47143
191	100.50522	0.49749	0.47156
192	105.40900	0.47434	0.47158
193	109.40678	0.45701	0.47150
194	112.91881	0.44280	0.47135
195	116.10526	0.43064	
196	100.50522	0.49749	0.47114
197	105.40900	0.47434	0.47128
198	109.40678		0.47129
199	112.91881	0.45701	0.47122
200	116.10526	0.44280	0.47108
	110.10259	0.43064	0-47088

MM 50	M ASY 10 1000		FA165 005-03	TIMP CREWS 10.0000 10	
	71 1.00000	FTR 5.00000	IFTR 5		
112345678901234567890123456789012345678901234567890123456789012345678901234567890	1.00000 IN (1 ()) 1.00000 0.80000 0.70210 0.64000 0.50564 0.50564 0.50564 0.50564 0.50564 0.50564 0.50564 0.50564 0.50564 0.50564 0.50564 0.50564 0.640765 0.40765 0.40766 0.40766 0.30766 0.30766 0.30766 0.35644 0.35646 0.35647 0.35646 0.357527 0.35646	5.00000 TOTN(x) 1.000000 1.000000 1.000000 1.0000000 1.00000000	AVGTN (1000 0.90000 0.93464 0.93464 0.93464 0.93464 0.74565 0.74565 0.64466 0.64466 0.65466 0.65466 0.65466 0.65466 0.65466 0.65466 0.65466 0.65466 0.65466 0.45666 0.45666 0.45666 0.45666 0.45666 0.45666 0.45666 0.466666 0.466666 0.46666 0.46666 0.46666 0.46666 0.46666 0.46666 0.4666	ATTPN(J) 0.74755 0.51553 0.43203 0.39488 0.36473 0.7426	ATDAN(J) 1.00000 1.06397 1.12356 1.18910 1.25245 1.34534
51 52	0.28202 0.28027	1.76399	0.40263 1.40007 0.35777		

53	0.27455	1.64066	0.39552
54	0.010	50923	0.39332
55	0.27525	56455	0.39117
50	0.27366	1.81791	0.38907
	0.27210	1.74324	
57			0.38702
58	0.27058	1.68897	0.38501
59	0.26910	1.64547	0.38305
60	0.26705	1.60899	0.38113
01	0.26623	1.85465	0.37924
62	0.26484	1.79107	0.37740
53	0.26348	1.73454	0.37559
34	0.26214	1.68913	0.37382
65	0.25084	1.65099	0.37208
66	0.25956	1.91665	0.37037
57	0.25831	1.83636	0.36870
68	0.25705	1.77771	0.36706
64	0.25537	1.73054	0.36545
70	0.25469	1.69086	0.36386
71	0.25353	1.96224	0.36231
72	0.25239	1.87940	0.36078
73	0.25127	1.31378	0.35928
74	0.25017	1.70995	0.35781
75	0.24910	1.72883	0.35636
76	0.24804	2.00571	0.35493
77	0.24699	1.92046	0.35353
78	0.24597	1.05799	0.35215
79	0.24496	1.80750	0.35080
80	0.24397	1.76513	0.34946
81	0.24300	2.04727	0.34815
82	0.24204	1.95976	0.34685
93	0.24110	1.89553	0.34558
34	0.24017	1.84367	0.34432
35	0.23926	1.79991	0.34309
86	0.23836	2.CB713	0.34187
87	C.23747	1.99746	0.34067
88	0.23660	1.93156	0.33949
39	0.23574	1.87831	0.33832
9C	0.23490	1.83334	0.33717
91	0.23405	2.12545	0.33604
92	0.23324	2.C3372	0.33492
93	0.23243	1.96623	0.33382
94	0.23163	1.91165	0.33273
95	0.23094	1.86553	0.33166
96	0.23007	2.16237	0.33060
97	0.22930	2.06366	0.32956
98	0.22854	1.99966	0.32853
99	0.22780	1.94381	0.32751
00	0.22706	1.89659	0.32650
131	0.22634	2.19800	0.32551
102	0.22562	2.10241	0.32453
. 33	0.22491	2.03196	0.32356
04	0.22421	1.97489	0.32261
05	0.22352	1.92662	0.32167
. 36	0.22284	2.23246	0.32073
27	0.22217	2.13505	0.31981
, 9R	0.22151	2.06320	0.31990
.09	0.22035	2.00497	0.31800
10	0.22020	1.95554	0.31711
11	0.21956	2.26503	0.31623
.12	0.21893	2.16657	0.31537
12	0 21 830	2 0034R	0 31451

0.217- 0.21587 0.21587 0.21587 0.21587 0.21587 0.21479 0.21487 0.21242 0.21387 0.21387 0.21387 0.21387 0.21973 0.21973 0.21973 0.20919 0.20919 0.20615 0.20518 0.20518 0.20518 0.20518 0.20518 0.20519	2.0343 1.98320 2.19320 2.19320 2.19321 2.193243 2.193243 2.193243 2.193243 2.193243 2.19320	0.31366 0.31282 0.31199 0.31116 0.31035 0.30757 0.30777 0.30779 0.30565 0.3
0.19440 0.19401 0.19363 0.19325	2.44004 2.35554 2.28678 2.22837	0.28143 0.28089 0.28036 0.27983
	0.21587 0.21587 0.21587 0.21587 0.21587 0.21586 0.21587 0.21587 0.21587 0.21587 0.21587 0.21587 0.21587 0.21587 0.21587 0.21587 0.21587 0.21587 0.21587 0.21587 0.21587 0.21587 0.21587 0.21587 0.20514 0.20514 0.20515 0.20516 0.20516 0.20516 0.20516 0.20517 0.20517 0.20517 0.20518 0.2	1.98348 0.21587 2.197320 0.21587 2.19735 0.21587 2.12287 0.21470 2.06243 0.21471 2.06243 0.21412 2.01124 0.21328 2.15142 0.21342 2.03785 0.21329 2.36020 0.21029 2.36020 0.21029 2.36020 0.21029 2.36020 0.21029 2.36020 0.21029 2.36020 0.21029 2.36020 0.21029 2.36020 0.21029 2.36020 0.21029 2.36020 0.20472 2.17919 0.20473 2.38996 0.20465 2.26436 0.20476 2.38996 0.20477 2.32624 0.20478 2.33897 0.20479 2.323261 0.20470 2.33897 0.20472 2.16320 0.20472 2.16320 0.20472 2.133870 0.20473 2.25834 0.20470 <

175	0.18953	2.27099	0.27477
176	0.1892	2.62330	0.27428.
177	0.18994	2.51060	
178	0.18859	2.42325	0.27380
179	0.18825		0.27332
180		2.35212	0.27285
131	0.18792	2.29168	0.27238
	0.19758	2.65211	0.27191
132	0.18725	2.53322	0.27144
183	0.18692	2.44496	0.27098
154	0.18659	2.37308	0.27052
185	0.18627	2.31198	0.27007
186	0.18594	2.67548	0.26961
187	0.18562	2.55542	0.26917
183	0.18530	2.46627	0.26872
139	0.18499	2.39365	0.26828
190	0.18467	2.33191	0.26784
191	0.18436	2.69842	0.26740
192	0.18405	2.57722	0.26696
193	0.18374	2.48720	
194	0.18344	2.41385	C.26653
195	0.18314		0.26611
196	0.18283	2.35150	0.26568
197		2.72096	0.26526
198	0.18254	2.59863	0.26484
	0.18224	2.50776	0.26442
199	0.18194	2.43371	0.26401
200	C.18165	2.37074	0.26359
			/

MM 50	M NSYS 25 10000	FAI 0.50000E-	LR TIMP 03 10.0000	CREWS 10	Q 0.80000
1	• 00000	FTF 1 5.00000	ETR 5		
1 1X123456789011234567890123456789012345678901234567890123456789		5.0000C T(IX) 1.00000 0.80000 0.80000 0.70210 0.64000 0.59564 0.71933 0.64083 0.555653 0.52946 0.71933 0.64083	AVGT(IX) 1.00000 0.90000 0.83403 0.78553 0.74755 0.74284 0.72827 0.71126 0.69411 0.67765 0.68143 0.67365 0.65434 0.65375 0.65434 0.65375 0.64469 0.64639 0.63570 0.63892 0.63899 0.63732	2	TTTP(J) 0.74755 0.60774 0.60774
50 51 52	94.43661 69.50909 78.02361	0.52946 0.71933 0.64083	0.62360 0.62172 0.62364 0.62397		

53	24.43535	0.59217	0.62337
54	99.11.2	0.55693	0.62214
55	94.43661	0.52946	C.62045
56	69.50909	0.71933	0.62222
57 58	78.02361 84.43539	0.64083	0.62254
59	89.77762	0.59217 0.55693	0.62202
60	94.43651	0.52946	0.62092 0.61939
61	69.50909	0.71933	0.62103
62	78.02361	0.64083	0.62135
63	84.43539	0.59217	0.62089
64	89.77762	0.55693	0.61989
65	94.43561	0.52946	0.61849
66	69.50909	0.71933	0.62002
67	78.02361	0.64083	0.62033
68 69	84.43539	0.59217	0.61992
70	89.77762 94.43661	0.55693 0.52946	0.61901
71	69.50909	0.71933	0.61773
72	78.02361	0.64083	0.61946
73	84.43539	0.59217	0.61908
74	89.77762	0.55693	0.61824
75	94.43661	0.52946	0.61706
76	69.50909	0.71933	0.61841
77	78.02361	0.64083	0.61870
78 76	84.43539	0.59217	0.61836
79	89.77762	0.55693	0.61758
80 81	94.43661	0.52946	0.61648
82	69.50909 78.02361	0.71933	0.61775
83	84.43539	0.64083 0.59217	0.61803 0.61772
94	89.77762	0.55693	0.61699
85	94.43661	0.52946	C.61596
86	69.50909	0.71933	0.61717
37	78.02361	0.64083	0.61744
88	84.43539	C.59217	0.61715
89	89.77762	0.55693	0.61647
9 0	94.43661	0.52946	0.61551
91 92	69.50909	0.71933	0.61665
93	78.02361 84.43539	0.64083 0.59217	0.61691
94	39.77762	0.55693	0.61664 0.61601
95	94.43661	0.52946	0.61510
96	69.50909	0.71933	0.61618
97	78.02361	0.64083	0.61644
98	84.43539	0.59217	0.61619
99	89.77762	0.55693	0.61559
100	94.43661	0.52946	0.61473
101	69.50909	0.71933	0.61577
102 103	78.02361	0.64083	0.61601
104	84.43539 89.77762	0.59217 0.55693	0.61578
125	94.43661	0.52946	0.61521 0.61440
106	69.50909	0.71933	0.61539
107	78.02361	0.64083	0.61563
108	84.43535	0.59217	0.61541
109	89.77762	0.55693	0.61487
110	94.43661	0.52946	0.61409
111	69.50909	0.71933	0.61504
112	78.02361	0.64083	0.61527
113	84.43539	0.59217	0.61507

114	99,777.2	0.55693	0.61456
115	14	0.52946	0.51382
116	69.30919	0.71933	0.61473
117	18.02361	0.64083	
* * '	10.05.01	0.04.03	0.61495
113	84.43535	0.59217	0.61476
119	89.77762	0.55693	0.61427
120	94.43661	0.52946	0.61357
121	69.50909	0.71933	0.61444
122	78.02361	2 / / 0 0 3	0 11111
		0.64083	0.61466
123	84.43539	0.59217	0.61447
124	89.77762	0.55693	0.61401
125	94.43661	0.52946	0.61333
126	69.50909		
120	6.4.26.40.3	0.71933	0.61417
127	78.02361	0.64083	0.61438
			1/ • 01430
128	94.43539	0.59217	0.61421
129	89.77762	0.55693	0.61377
130	94.43651	0.52946	0.61312
131	69.50909	C.71933	0 41303
131	0 9 . 3 (190 9		0.61393
132	78,02361	0.64083	0.61413
133	84.43559	0.59217	0.61397
134	89.77762	0.55693	0.61354
	0/ : 2//1		
135	94.43661	0.52946	0.61292
136	69.50909	0.71933	0.61370
		0.017.200	0.01310
137	7S.02361	0.64083	0.61390
_			
138	84.43539	0.59217	0.61374
139	89.77762	0.55693	0.61333
140	94.43561	n Focks	
TAC	94.42001	0.52946	0.61273
141	69.50909	0.71933	0.61349
142	78.02361	0.64083	0.61368
143	84.43539	0.59217	0.61353
1 / /	00 777. 1		
144	89.77762	0.55693	0.61314
145	94.43661	0.52946	0.61256
			0.01230
146	69.50909	0.71933	0.61329
147	78.02361	0.64083	0.61348
148	84.43539	0.59217	0.61334
149	89.77762		0 (1204
47	04.11107	0.55693	0.61296
150	94.43501	0.52946	0.61240
151	69.50909	0.71933	0.61311
152	78.02361	0.64083	0.61329
153	84.43539	0 50317	
100		0.59217	0.61315
154	39.77762	0.55693	0.61279
155	94.43661	0.52945	C.61225
156	69.50909	0.71933	0.51294
157	78.02361	0.64083	0.61311
101			0.01311
158	84.43539	0.59217	0.61298
159	89.77762	0.55693	0.61263
160	94.43661	0.52946	0.61211
161	69.50909	0.71933	0.61277
101	07.0000	V. 11733	0.01211
162	78.02361	0.64083	0.61295
163	84.43535	0.59217	0.61282
164	89.77752	0.55693	0.61248
	94.43661	0.52946	
165			0.61198
166	69.50909	0.71933	0.61262
167	7 8.02361	0.64083	0.61279
168	84.43539	0.59217	0.61267
169	8 9.777 62	0.55693	0.61234
170	94.43661	0.52946	0.61185
171	69.50909	0.71933	0.61248
172	78.0236 1	0.64083	0.61264
173	84.43539	0.59217	0.61253
174	89.77762	0.55693	0.61221
• 1 7	07611102	0 1 7 7 0 9 3	0.01221

175	04 . 3661	0.52946	0.61173
175	4,1	0.71933	0.61235
177	78.02001	0.64083	0.61251
178	84.43539	0.59217	0.61239
179	89.77762	0.55693	0.61208
160	94.43601	0.52946	0.61162
131	69.50909	0.71933	0.61222
182	78.02361	C.64083	0.61238
193	84.43535	0.59217	0.61226
184	89.77762	0.55693	0.61196
185	94.43661	0.52946	0.61152
185	69.50909	0.71933	0.61210
187	78.02361	0.64083	0.61225
188	84.43539	0.59217	0.61214
189	89.77762	0.55693	0.61185
190	94.43661	0.52946	0.61142
191	59.50909	0.71933	0.61198
192	78.02361	0.64083	0.61213
193	84.43539	0.59217	0.61203
194	89.7776?	C. 55693	0.61175
195	94.43661	0.52946	0.61132
196	69.50909	0.71933	0.61188
197	78.02361	0.64083	0.61202
198	84.43539	0.59217	0.61192
199	89.77762	0.55693	0.61165
200	94.43661	0.52946	0.61123

3.6

53	0.27500	2.12598	0.39552
54	11 . 2 .	1.01144	0.39332
55	0.27525	1.92:54	0.39117
56	0.27300	2.62857	0.38907
57	0.27210		
		2.35510	0.38.05
58	C. 27058	2.18848	0.38501
59	0.26910	2.06961	0.38305
60	0.26765	1.97818	C.39113
61	0.26623	2.70194	0.37924
52	0.26494	2.41 172	0.37740
63	0.26348	2.24152	0.37559
64	0.20214	1.12452	0.37382
65	0.26084		
		2.02982	0.37268
55	C. 25955	2.77134	0.37037
67	0.25831	2.49090	0.36870
68	0.25708	2.30346	0.36706
20	0.25537	2.17660	0.36545
70	0.25459	2.07882	0.36386
71	0.25353	2.83727	0.36231
72	0.25239	2.53905	
73	0.25127		C.36078
		2.35668	0.35928
74	0.25017	2.27618	0.35781
75	0.24910	2.12551	0.5634
76	0.24504	2.90011	0.35493
77	0.24699	2.59453	0.35353
78	0.24597	2.40748	0.35215
79	0.24495	2.27353	0.35080
80	0.24397	2.17014	
81			0.34946
	0.24300	2.96021	0.34815
82	0.24204	2.64761	0.34685
83	0.24110	2.45512	0.34558
84	C.24017	2.31890	0.34432
85	0.23926	2.21291	0.34309
86	0.23936	3.01785	0.34187
57	0.23747	2.69854	0.34067
98	0.23660	2.50281	0.33949
39	0.23574	2.36246	
			0.33932
90	0.23490	2.25400	0.33717
91	0.23406	3.07326	0.33604
92	0.23324	2.74753	0.33492
93	0.23243	2.54774	0.33382
94	0.23163	2.40440	0.33273
95	0.23084	2.29358	0.33166
96	0.23007	3.12663	0.33060
97	0.22930	2.79474	0.32956
98	0.22854		
		2.59106	0.32853
99	0.22750	2.44485	0.32751
100	0.22706	2.33177	0.32550
101	0.22634	3.17816	0.32551
102	0.22562	2.84C33	0.32453
.03	0.22491	2.63290	0.32356
.34	0.22421	2.48394	0.32261
.35	C. 22352	2.36868	0.32167
36	0.22254	3.22798	0.32187
27			
	0.22217	2.88443	0.31981
30	0.22151	2.67338	0.31890
09	0.22095	2.52178	0.31800
10	0.22020	2.40442	0.31711
11	0.21956	3.27623	0.31623
12	0.21893	2.92715	0.31537
13	0.21830	2.71262	0.31451
			4478

114	0.21763	2.55345 3.43979	0.31366 0.31288
116 117	0.21697	3. 32304 2. 96959	0.31199
118	0.21529	2.75069	0.31116 0.31035
119	0.21470 3.21412	2.59405 2.47273	0.30955
121	0.21355	3.36849	0.30875 0.30797
122 123	0.21242	3.00840	0.30719
124	0.21187	2.78759 2.62865	0.30642 0.30565
125	0.21132	2.50544	0.30490
126 127	0.21078 0.21025	3.41269 3.04802	0.30415
128	0.20972	2.92368	0.30263
129 130	0.20919	2,66232 2,53 7 2 7	0.30195
131	0.20816	3.45571	0.30124 0.30053
132 133	0.20765 0.20714	3.08614 2.85873	0.29982
134	0.20665	2.69511	0.29913 0.29844
135 136	0.20615 0.20566	2.55829	0.29775
137	0.20518	3.49763 3.12330	0.29703 0.29641
138 139	0.20473	2.89244	0.29574
140	0.20422 0.20375	2•72703 2•59853	0.29508 0.29443
141 142	0.20329	3.53852	0.29378
143	0.20232 0.20237	3.15955 2.92623	0.29314
144	0.20191	2.75829	0.29188
145 146	0.20146	2.62805 3.57844	0.29126
147	0.20059	3.19495	0.29002
148 149	C.20014 0.19971	2.55879 2.78876	0.28942
150	0.19928	2.65689	0.28881
151 152	0.19885 0.19843	3.61744 3.22954	0.28763
153	0.19801	2.99060	0.28704
154 155	0.19759 0.19718	2.81855	0.28588
156	0.19678	2.68509 3.65549	0.28531
157 158	0.19637	3.26330	0.28418
159	0.19597 0.19557	3.02172 2.84769	0.28362 0.28307
160	0.19518	2.71267	0.28252
161 162	0.19440	3.69290 3.29647	0.28197 0.28143
163	C.19401	3.05218	0.23089
164 165	0.19363 0.19325	2.87622 2.73968	0.28036 0.27983
166	0.19295	3.72944	0.27931
167 168	0.19251	3.32889 3.08202	0.27879
169	0.19177	2.90416	0.27827 0.27776
170 171	0.19141 0.19105	2.76614	0.27725
172	0.19109	3.76524 3.36065	0.27675 0.27625
73	0.19033	3.11125	0.27575
	0.18998	2.93155	0.27526

175	0.18967	2.79207	0.27477
176	0.19.12	3.80033	0.27428
177	0.18344	3.39179	0.27380
178	0.18859	3.13992	0.27332
179	0.18825	2.95841	0.27285
180	0.18792	2.81751	0.27238
181	0.18758	3.83476	0.27191
132	0.18725	3.42235	0.27144
193	0.18692	3.16805	0.27098
184	0.18659	2.98477	0.27052
185	0.18627	2.84247	0.27007
186	0.18594	3.96855	0.26961
187	0.18562	3.45234	0.26917
188	0.18530	3.19566	0.26872
189	0.18499	3.01064	0.26828
190	C.18467	2.86598	0.26784
191	0.18436	3.90173	0.26740
192	0.18405	3.48179	0.26696
193	0.18374	3.22278	0.26653
194	0.18344	3.03605	0.26611
195	0.18314	2.89105	0.26568
196	0.18283	3.93432	0.26526
197	0.18254	3.51073	0.26484
198	0.18224	3.24942	0.26442
199	0.18194	3.06102	0.26401
200	0.18165	2.91471	0.26359

MM 100	M 10	N5YS 10000	0.5000	FAILR OE-03		10.	TIMP COCO	CREWS	
		1	ETR 5.00000	I E TR					
	1.0000	70 R (IX)		IX)	AVG1	T(1)	()	ن.	ATTTP(J)
IX 1		100.00000	1.00	000	1.0	0000	00	1 2	0.74755 0.53146
2 3		125.00000			0.1	9000 8340	3	3	0.46451
4		156.24998	0.64			7859 7479		4 5	0.42891 0.40694
5 6		167.88737 170.23 2 73				720		6	0.39254
7		180.88492	0.55	284		696		7	0.38295 0.37673
8		190.02409				675! 656!		8 9	0.37304
10		205.56199			0.	639	50	10	0.37136
11		200.9221	0.49			626		11	0.37136
12		209.24579				614) 602			
14		223.0054	0.44	842	0.	591	50		
15		229.0710				581 573			
16 17		220.34190	_			565			
18		234.1125	0.42	2715		557			
19		239.9173				550 543			
20 21		233.7435				537			
22		240.6578	4 0.41			532			
23		246.6049 252.0097				526 521			
24 25		257.0358	·		0.	515	87		
26		243.2267		1114	0.	511 507	85 71		
27 28		249.8751 255.5741		0020 9128	0.	503	55		
29		260.7465	8 0.38	351		499			
30		265.5554		7657 0019		495			
31 32		249.8785 256.3 7 23	-	9006		489			
33		261.9257	8 0.3	8179		485			
34		266.9604 271.6381		7459 6814		482			
35 36		254.3476	4 0.3	9316	0.	476	87		
37	•	260.7529		8350		474			
38 39		266.2219 271.1762	_	7563 6876		469			
40		275.7773	4 0.3	6261		466			
41		257.0581	-	8902 7963		464			
42		263.4165 268.8408		7197	0.	460)43		
44		273.7519	5 0.3	6529		458			
45		278.3117 258.3054		5931 8714		456 454			
46		264.6450	2 0.3	7786	0.	. 457	294		
48	3	270.0509	4 0.3	7030		45			
49 50		274.9440 279.4868		6371 5780		44			
ەر ق		258.3054	2 0.3	8714	0.	. 44	541		
52		264.6450	2 0.3	7786	0.	. 44	509		

53	270.050.4	0 27026	0 // 36 0
		0.37030	0.44368
54	274.	0.00371	0.44220
55	270.43682	0.35780	0.44067
56	253.30542	0.38714	0.43971
57	264.64502	0.37786	0.43863
58	270.05054	0.37030	0.43745
59	274.94409	0.36371	0.43620
60	279.48682	0.35780	0.43489
61	258.30542	0.38714	0.43411
62	264.64502	0.37786	0.43320
63	270.05054	0.37030	0.43220
64	274.94409	0.36371	0.43113
65	279.48682	0.35780	0.43000
66	258.30542	0.38714	0.42935
67	264.64502	0.37786	0.42859
68	270.05054	0.37030	0.42773
59	274.94409	0.36371	0.42680
70	279.48682	0.35780	0.42581
71	258.30542	0.38714	0.42527
72	264.64502	0.37786	0.42461
73			
	270.05054	0.37030	0.42387
74	274.94409	0.36371	0.42305
75	279.48682	0.35780	0.42218
76	258.30542	0.38714	0.42172
77	264.64502	0.37786	0.42115
78	270.05054	0.37030	C. 42050
79	274.94409	0.36371	0.41978
80	279.48632	0.35780	0.41901
81	258.30542	0.38714	C.41861
82	264.64502	0.37786	0.41812
83	270.05054	0.37030	0.41754
84	274.94409	0.36371	0.41690
	279.48682		
85		0.35740	0.41620
36	258.30542	0.38714	0.41587
87	264.64502	0.37786	0.41543
98	270.05054	0.37030	0.41492
89	274.94409	0.36371	0.41434
	<u> </u>		
90	279.49682	0.35780	0.41371
91	258.30542	0.38714	0.41342
92	264.64502	0.37786	0.41303
93	270.05054	0.37030	0.41257
94	274.94409	0.36371	0.41205
95	279. 48682	0.35780	0.41148
96	258.30542	0.38714	0.41123
97	264.64502	0.37786	0.41089
98	270.05054	0.37030	C. 41047
99	274.94409	0.36371	0.41000
100	279.48682	0.35780	0.40948
101	258.30542	0.38714	0.40926
		0.37786	0.40895
102	264.54502		
103	270.05054	0.37030	0.40857
104	274.94409	0.36371	0.40814
105	279.48682	0.35780	0.40766
106	258.30542	0.38714	0.40747
107	264.64502	0.37786	0.40719
108	270.05054	0.37030	0.40685
109	274.94409	0.36371	0.40645
110	279.48682	0.35780	0.40601
111	258.30542	0.38714	0.40584
112	264.64502	0.37786	0.40559
113	270.05054	0.37030	0.40528

114	274,96409	0.36371	0.40491
115	20	0.75780	0.40450
116	258.30,42	0.38714	0.40435
117	264,5450?	0.37786	0.40413
118	270.05054	0.37030	0.40384
110	274.94409	0.36371	0.40350
120	279.48682	0.35780	0.40312
121	258.30542	0.38714	0.40299
122	204.64502	0.37786	0.40279
123	270.05054	0.37030	0.40252
124	274.94409	0.36371	0.40221
125	279.48682	0.35780	0.40185
126	258.30542	0.38714	0.40174
127	264.64502	0.37786	0.40155
128	270.05054	0.37030	0.40130
129	274.94403	0.36371	0.40101
130	279.48682	0.35780	0.40068
131	258.30542	0.38714	0.40058
132	264.64502	0.37786	0.40040
133	270.05054	0.37030	C.40018
134	274.94409	0.36371	0.39991
135	279.48682	0.35780	0.39959
136	258.30542	0.38714	0.39950
137	264.64502	0.37786	0.39930
136			0.39913
139	270.05054	0.37030	
140	274.94409	0.36371	0.39988
141	279.48682	0.35780	0.39859
142	258.30542	0.38714	0.39850
143	254.64502	0.37786	0.39836
144	270.05054	0.37030	0.39816
144	274.94409	0.36371	0.39792
146	279.48692	0.35780	0.39765
147	258.30542	0.38714	0.39757
146	264.64502	0.37786	0.39744
146	270.05054	0.37030	0.39726
150	274.94409	0.36371	0.39703
	279.48682	0.35780	0.39677
151	258.30542	0.38714	0.39671
152	264.64502	0.37786	0.39658
153	270.05054	0.37030	0.39641
154 155	274.94409	0.36371	0.39620
	279.49682	0.35780	0.39595
156	258.30542	0.38714	0.39589
157	264.04502	0.37786	0.39578
158	270.05054	0.37030	0.39562
159	274.94409	0.36371	0.39542
160	279.48682	0.35780	0.39518
161	258.30542	0.39714	0.39513
162	264.64502	0.37786	0.39503
163	270.05054	0.37030	0.39487
164	274.94409	0.36371	0.39468
165	279.48682	0.35780	0.39446
166	258.30542	0.38714	0.39442
167	264.64502	0.37786	0.39432
169	270.05054	0.37030	0.39417
169	274.94409	0.36371	0.39399
170	279.48682	0.35780	0.39378
171	258.30542	0.38714	0.39374
172	264.64502	0.37786	0.39365
173	270.05054	0.37030	0.39351
174	274.94409	0.36371	0.39334

1 76			
175	279.48692	0.35780	0.39314
176	138 J. 150	0.38714	0.39311
177	204.04502	0.37786	0.39302
178	270.05054	0.37030	0.39289
179	274.94409	0.36371	0.39273
180	279.48682	0.35780	0.39253
181	258.30542	0.38714	0.39250
182	264.64502	0.37786	0.39242
183	270.05054	0.37030	0.39230
134	274.94409	0.36371	0.39215
185	279.48682	0.35780	0.39196
186	258.30542	0.38714	0.39194
187	264.64502	0.37786	0.39194
198	270.05054	0.37030	0.39175
189	274.94409	0.36371	0.39175
190	279.48682	0.35780	
191	258.30542	0.38714	0.39142
192	264.64502	0.37786	0.39140
193	270.05054	0.37030	0.39133
194	274.94409	0.36371	0.39122
195	279.48682	0.35780	0.39108
196	258.30542	0.38714	0.39091
197	264.54502		0.39089
198	270.05054	0.37786	0.39082
199	274.94409	0.37030	C. 39072
200	279.48682	0.36371	C.39058
	L17040002	0.35780	0.39042

MM 100		Y S .0000	0.5000	FAILR POE-03	TIMP 10.0000	CREWS 10	
	TI 1.00000	5.	ETR OCOCO	IETR 5			
X1234567890123456789012345678901234567890123456789012345678901234567890123456789	TN(1 1.000 0.300 0.300 0.5561 0.5561 0.5561 0.5561 0.576 0.476 0.447 0.447 0.447 0.449 0.4491 0.4691 0.3369 0.3564 0.3564 0.3564 0.3564 0.3564 0.3564 0.3564 0.3564 0.3564 0.3564 0.3564 0.3564 0.3564 0.3564 0.3564 0.3564 0.3564 0.3564 0.3564 0.3664 0	1.00 1.00	0000000 0000000 000000 000000 000000 0000	AVGTN(IX) 1.00000 0.90000 0.83403 0.78553 0.747557 0.65656 0.66324 0.64876 0.63154 0.64876 0.63154 0.657802 0.557751 0.557751 0.557751 0.557751 0.51045 0.49808	ATTPN(0.747 0.515 0.439 0.364 0.324 0.324 0.327 0.278	755 353 303 388 373 226 358 314 302 64	ATDAN(J) 1.00000 1.03090 1.05803 1.08618 1.11573 1.14690 1.17985 1.21474 1.25175 1.29109 1.33298
50 51 52	0.2839 0.2820 0.2802	3 1.26 2 1.37	062 272	0.40243 0.40007 0.39777		A 7	1, 5

53	0.2785	1.32937	0.39552
2.1	1,	31359	0.39332
55	0.27525	1.29990	0.39117
56	0.27366	1.41468	0.38907
57	0.27210	1.38868	0.38702
56	0.27058	1.36352	0.38501
59	0.26910	1.35158	0.38305
60	0.26765	1.33583	0.39113
61	0.26623	1.45417	0.37924
62	0.25484	1.42678	0.37740
63	0.26348	1.40544	0.37559
54	0.26214	1.38744	0.37382
65	0.26084	1.37172	0.37208
65 67	0.25956 0.25831	1.49152 1.46285	0.37037 0.36870
68	0.25708	1.44042	0.36706
69	0.25587	1.42145	0.36545
70	0.25469	1.40484	0.36386
71	0.25353	1.52700	0.36231
72	0.25239	1.49714	0.36078
73	0.25127	1.47371	0.35928
74	0.25017	1.45383	0.35781
75	0.24910	1.43639	0.35636
76	0.24804	1.56082	0.35493
77	0.24699	1.52985	0.35353
78	0.24597	1.50547	0.35215
79	0.24476	1.48475	0.35080
30	0.24397	1.46655	0.34946
81	0.24300	1.59317	0.34815
82 83	0.24204 0.24110	1.56116 1.53589	0.34685 0.34558
84	0.24017	1.51438	0.34432
35	0.23926	1.49545	0.34309
86	0.23836	1.62418	0.34187
87	0.23747	1.59119	0.34067
88	0.23660	1.56509	0.33949
39	0.23574	1.54283	0.33832
90	0.23490	1.52322	0.33717
91	0.23406	1.65401	0.33504
92	0.23324	1.62007	0.33492
93	0.23243	1.59318	0.33382
94	0.23163	1.57022	0.33273
95 96	0.23054 0.23007	1.54997 1.68273	0.33166 0.33060
97	0.22930	1.64791	0.32956
98	0.22854	1.62027	0.32853
99	0.22780	1.59664	0.32751
100	0.22706	1.57578	0.32650
101	0.22634	1.71046	0.32551
102	C. 22562	1.67479	0.32453
103	0.22491	1.64643	0.32356
104	0.22421	1.62216	0.32261
105	0.22352	1.60072	0.32167
106	0.22284	1.73728	0.32073
107	0.22217	1.70079	0.31981
103 109	C.22151 O.22085	1.67175 1.64687	0.31890 0.31800
110	0.22020	1.62488	0.31711
111	0.21956	1.76325	0.31623
112	0.21893	1.72598	0.31537
113	0.21830	1.69628	0.31451

114	0.217/	1.67082	0.31366
111-		1.04530	0.31282
116	0.21647	1.78843	0.31199
117			
	0.21587	1.75042	0.31116
118	0.21528	1.72009	0.31035
119	C.21470	1.69407	0.30955
120	0.21412	1.67103	0.30875
121	C.21355	1.81290	0.30797
122	0.21298	1.77416	0.30719
123	0.21242	1.74323	0.30642
124	0.21187	1.71667	0.30565
125	0.21132	1.69314	0.30490
120	0.21073	1.83668	0.30415
127	0.21025	1.79725	0.30341
128	0.20972	1.76573	0.30268
129	0.20919	1.73865	0.30196
130	0.20867	1.71465	0.30124
131	0.20816	1.85984	0.30053
132	0.20765	1.81974	0.29982
133	0.20714	1.78765	0.29913
134	0.20665	1.76067	0.29844
135	0.20615	1.73561	0.29775
136	0.20556	1.88240	0.29708
137	0.20518	1.84165	0.29541
138	0.20470	1.80901	0.29574
139	0.20422	1.78095	0.29508
140	0.20375	1.75605	0.29443
141	0.20329	1.90441	0.29443
142	0.20232	1.86302	0.29314
143	0.20237	1.82986	0.29314
144	0.20191	1.80133	0.29188
145	0.20146	1.77500	
146	0.20102	1.92589	0.29126 0.29064
147	0.20058		
		1.88389	0.29002
148 149	0.20014	1.85022	0.28942
150	0.19971	1.82123	0.28881
	0.19928	1.79549	0.28622
151	0.19885	1.94688	0.28763
152	0.19843	1.90429	0.28704
153	0.19801	1.87011	0.29646
154	0.19759	1.84069	0.28588
155	0.19713	1.81454	0.23531
156	0.19678	1.96741	0.29474
157	0.19637	1.92423	0.28418
158	0.19597	1.88958	0.28362
159	0.19557	1.85972	0.28307
150	0.19518	1.83319	0.28252
161	0.19479	1.58749	0.28197
162	0.19440	1.94375	0.28143
163	0.19401	1.90862	0.28089
154	0.19363	1.87835	0.28036
165	0.19325	1.85143	0.27983
166	0.19238	2.00716	0.27931
167	0.19251	1.96287	0.27879
168	0.19214	1.92728	0.27827
169	0.19177	1.8966C	0.27776
170	0.19141	1.86932	0.27725
171	0.19105	2.02642	0.27675
172	0.19059	1.9816C	0.27625
173	0.19033	1.94556	0.27575
174	0.18995	1.91448	0.27526

175	0.18963	1.88684	0.27477
176	C.18%	2.04531	0.27428
177	0.18894	1.99996	0.27380
178	0.18359	1.96349	
179	0.18825	1.93202	0.27332
180	0.18792	1.90403	0.27285
131	0.18758	2.06384	0.27238
132	0.18725		0.27191
183	0.18692	2 • C1 798	0.27144
184	0.18659	1.98108	0.27098
185	0.18627	1.94923	0.27052
186		1.92090	0.27007
187	0.18594	2.08203	0.26961
158	0.18562	2.03566	0.26917
	0.18530	1.59834	0.26872
189	0.18499	1.96613	0.26828
190	0.18467	1.93746	0.26784
191	0.18436	2.C9988	0.26740
192	0.18405	2.C5303	0.26696
193	0.18374	2.C1530	0.26653
194	0.18344	1.98273	0.26611
195	0.18314	1.95373	0.26568
196	0.18283	2.11742	0.26526
197	0.18254	2.07009	
198	0.18224	2.03196	0.26484
199	0.18194	1.99903	0.26442
200	0.18165	1.96972	0.26401
		40 70 712	0.26359

MM 100	м 20	NSYS 10000	0.5000	FATLR	TIMP 10.0000	CREWS 10	Q 00008.0
	1.0000	00	FTR 5.00000	LETR 5			
X12345678901234567890123456789012345678901 11121111122222222333333333444444444551		R(IX) 100.00000 125.00000 125.00000 142.42908 156.24998 167.48737 162.42911 174.67549 184.73578 193.53839 201.404618 195.94616 204.514288 219.02161 196.54320 206.50888 214.549486 221.8063	1.00 0.00 0.50 0.50 0.50 0.50 0.50 0.50	10000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 10000 1000000	AVGT(IX) 1.0000 0.90000 0.83403 0.78553 0.772557 0.684883 0.64883 0.6648814 0.6638149 0.516843 0.5584859 0.578892 0.52866 0.53897 0.52892 0.52866 0.51222	J 1 2 3 4 5 6	ATTTP(J) 0.74755 0.54850 0.49328 0.46955 0.46046 0.46046
52		210.81801	0.47		0.50153		

53	214, 1 53	0.45701	0.50069
54	22>000	0.44230	0.49962
55	232.21057	0.43064	0.49837
56	201.01048	0.49749	0.49835
57	210.81801	0.47434	0.49793
58	218.81363	0.45701	0.49722
59	225.83766	0.44280	0.49630
60	232.21057	0.43064	0.49521
61	201.01048	0.49749	0.49524
62	210.81801	0.47434	C.49491
63	218.81363	0.45701	C.49431
64	225.33766	0.44280	0.49350
65	232.21057	0.43064	0.49253
66	201.01048	0.49749	0.49261
67	210.81801	0.47434	0.49234
68	218.81363	0.45701	0.49182
59 7 0	225.83766	C • 44280	0.49111
70 71	232.21057	0.43064	0.49024
71	201.01048	0.49749	0.49034
72	210.81801	0.47434	C. 49012
73	219.81363	0.45701	0.48967
74 75	225.83766	0.44280	0.48903
	232.21057	0.43064	0.48826
76 77	201.01048	0.49749	0.48838
	210.91901	0.47434	0.48819
78 79	218.81363	0.45701	0.48779
80	225.83766 232.21057	0.44280	0.48723
81		0.43064	0.48652
32	201.01048	0.49749	0.48665
33	210.81801 218.81363	C•47434 O•45701	0.48650 0.48615
94	225.83766	0.44280	0.48563
85	232.21057	0.43064	0.48498
86	201.01048	0.49749	0.48513
57	210.81801	0.47434	0.48501
58	218.81363	0.45701	0.48469
39	225.83766	0.44280	0.48422
90	232.21057	0.43064	0.48362
91	201.01048	0.49749	0.48377
92	210.81801	0.47434	0.48367
93	218.81363	0.45701	0.48336
94	225.83766	0.44280	0.48295
95	232.21057	0.43064	0.48240
96	201.01048	0.49749	0.48256
97	210.81801	0.47434	0.48247
98	218.81363	0.45701	0.48221
99	225.83766	0.44280	0.48182
100	232.21057	0.43064	0.48130
101	201.01048	0.49749	0.48146
102	210.81801	0.47434	0.48139
103	218.81363	0.45701	0.48116
104	225.93766	0.44280	0.48079
105	232.21057	0.43064	0.48031
106	201.01048	0.49749	0.48047
107	210.81801	0.47434	0.48042
108 109	218.81363 225.83766	0.45701 0.44280	0.48020 0.47986
110	232.21057	0.43064	0.47941
111	201.01048	0.49749	0.47957
112	210.81801	0.47434	0.47952
113	218.81363	0.45701	0.47932
The same of the state of the same of the s		will a straightful with the straightful war	

114	225. 33700	0.44280	0.47900
	2, 2, 1, 0,0		
115		0. +3064	0.47858
115	201.010.48	0.49749	0.47875
117	210.81801	0.47434	0.47871
118	218.81363	0.45701	0.47853
119	225.33766	0.44280	0.47822
120	232.21057	0.43064	0.47783
121	201.01048	0.49749	C.47799
122	210.81801	0.47474	0.47796
123	218.81463	0.45701	0.47779
124	225.33766	0.44280	0.47751
125	232.21057	0.43064	0.47713
126	201.01048	0.49749	C.47729
127	210.81801	0.47434	0.47727
128	218.81363	0.45701	0.47711
129	225.33766	0.44280	0.47685
130	232.21057	0.43064	0.47649
	·		
131	201.01048	0 : 49749	0.47665
132	210.31801	0.47434	0.47663
133	218.81353	0.45701	0.47649
134	225.83766	0.44280	0.47623
135	232.21057	0.43064	0.47590
	201.01043		
136		0.49749	0.47606
137	210.81801	0.47434	0.47604
138	218.81363	0.45701	0.47591
139	225.33766	0.44280	0.47567
140	232.21057	0.43064	0.47535
141	201.01048	0.49749	0.47550
142	210.81801	0.47434	0.47549
143	218.51363	0.45701	0.47536
144	225 . 83700	0.44280	0.47514
145	232.21057	0.43064	0.47483
146	201.01048	0.49749	0.47499
147	210.81801	0.47434	0.47498
148			
	218.31363	0.45701	0.47486
149	225.83766	0.44280	0.47465
150	232.21057	0.43064	0.47435
151	201.01048	0.49749	0.47451
152	210.81801	0.47434	0.47450
153	218.81363	0.45701	0.47439
154	225.83766	0.44280	0.47418
155	232.21057	0.43064	0.47390
156	201.01048	0.49749	0.47406
157	210.81801	0.47434	0.47406
158	218.81363	0.45701	0.47395
159	225.83766	0.44280	0.47375
160	232.21057	0.43064	0.47348
161	201.01048	0.49749	0.47363
162	210.81801	0.47434	C. 47364
163	218.81363	0.45701	0.47353
164	225.83766	0.44280	0.47335
165	232.21057	0.43064	0.47309
166	201.01048	0.49749	0.47324
167	210.81301	0.47434	0.47324
166	218.81363	0.45701	0.47315
160	225.83766	0.44287	0.47297
170	232.21057	0.43064	0.47272
171	201.01048	0.49749	0.47286
172	210.81801	0.47434	0.47287
173	218.31363	0.45701	0.47278
174		0.44280	
114	225.83766	V. 44200	0.47261

175	232.21057	0.43064	0 / 700 5
176	201.	0.49749	C. 47237
177	210.41501		C. 4725!
178	218.31363	0.47434	0.47252
179	225.33766	0.45701	0.47243
180		0.44280	0.47227
181	232.21057	0.43064	0.47204
	201.01049	0.49749	0.47218
192	210.51801	0.47434	0.47219
133	218.81363	0.45701	0.47210
134	225.83766	0.44280	0.47195
195	232.21057	C. 43064	0.47172
186	201.01048	0.49749	0.47196
187	210.81801	0.47434	0.47187
188	218.81363	0.45701	
189	225.83766	0.44280	0.47179
190	232.21057	0.43764	9.47164
191	201.01048		0.47143
192	210.81801	0.49749	0.47156
193	218.31363	C. 47434	0.47158
194		5.45701	0.47150
195	225.83766	0.44280	0.47135
	232.21057	0.43064	0.47114
196	201.01048	0.49749	0.47128
197	210.31801	0.47434	0.47129
198	218.31363	0.45701	0.47122
199	225.83766	0.44280	0.47108
200	232.21057	0.43064	0.47088
			C - 7 / U O B

MM 100	м 20	NSYS		FATER 00E-03	TIMP 10.0000	CREWS 10	Q 0.80000
	Ti		ETR	IETR			
	1.00000		5.00000	5			
IX		(T X)	TOTN(IX)	AVGTN(IX)	ATTPN		ATDAN(J)
1 2		0000 0000	1.00000	1.00000	0.74 0.51		1.00000 1.06397
3		0210	1.00000	0.83403	0.43		1.12356
4		4000	1.00000	0.78553	C. 39		1.13910
5		9554	1.00000	0.74755	0.36		1.26245
6		5158 3449	1.09609 1.07110	0.71657 0.69056	0.34	220	1.34534
8		1200	1.05725	0.66924			
9		9295	1.04817	0.64876			
10 11		7651 6211	1.04167	0.63154 0.61613			
12		4935	1.13575	0.60224			
13	0.4	3792	1.11631	0.58960			
14		2759	1.10241	0.57802			
15 16		1820 0960	1.09177 1.24217	0.56737			
17		0168	1.20553	C.54834			
18		9436	1.18135	0.53979			
19		8756	1.16330	0.53178			
20 21		3121 7527	1.14902 1.32569	0.52425 0.51715			
22		5969	1.28309	0.51045			
23		5444	1.25402	0.50410			
24 25		5948 5478	1.23178 1.21382	0.49808			
20		5033	1.42004	0.48688			
27	0.34	4010	1.37053	0.48167			
26		4207	1.33600	0.47668			
29 30		3823 3456	1.30915 1.28720	0.47191 0.46733			
31		105	1.50277	0.46293			
3?		753	1.44758	0.45871			
33		2445 2135	1.40857 1.37794	0.45464			
34 35	0.37		1.35268	0.44694			
36	0.31		1.57688	0.44328			
37	2.31		1.51684	0.43976		•	
38 39	0.31 0.30		1.47402 1.44C16	0.43634			
40	0.31		1.41210	0.42984			
4:	0.30		1.64430	0.42673			
42	0.30		1.58002	0.42372			
43 44	0.29 0.29		1.53386 1.49719	0.42079 0.41795			
45	0.29		1.46667	0.41519			
46	0.29		1.70636	0.41250			
47	0.25		1.63828	C.4C998 O.4C734			
48 49	0.28 C.28		1.58915 1.54998	0.40485			
50	0.28		1.51727	0.40243			
51	0.25		1.76399	0.40007			
52	0.28	1027	1.69247	0.39777			

e 2	0.27855	1.64066	0.39552
53	0.276	1.59922	0.39332
54	0.27525	1.56455	C.39117
55	0.27356	1.81791	0.38907
56	0.27300	1.74324	0.38702
57	0.27210	1.68897	0.38501
58	0.27058	1.64547	0.38305
59	0.26910	1.60899	0.38113
60	C.26765	1.86865	0.37924
61	0.26623	1.79107	0.37740
62	0.26484	1.73454	0.37559
63	0.26348		0.37382
64	0.26214	1.68913	0.37208
65	0.26094	1.65099	0.37037
56	0.25956	1.91665	0.36870
67	0.25831	1.83636	0.36706
68	0.25708	1.77771	0.36545
69	0.25587	1.73054	0.36386
70	0.25469	1.69086	0.36231
71	0.25353	1.96224	0.36078
72	0.25239	1.87940	
73	0.25127	1.81878	0.35928 0.35781
74	0.25017	1.76995	0.35636
75	0.24910	1.72883	
76	0.24804	2.00571	0.35493
77	0.24699	1.92046	0.35353
78	0.24597	1.85799	0.35215
79	0.24496	1.80760	0.35080
80	0.24397	1.76513	0.34946
81	0.24300	2.04727	0.34815
82	0.24204	1.95976	0.34685
83	0.24110	1.89553	0.34558
84	0.24017	1.84367	0.34432
85	0.23926	1.79991	0.34309
36	0.23836	2.08713	0.34187
87	0.23747	1.99746	0.34067
38	0.23660	1.93156	0.33949
89	0.23574	1.87831	0.33832
90	0.23490	1.83334	0.33717
91	0.23406	2.12545	0.33604
92	0.23324	2.03372	0.33492
93	0.23243	1.96623	0.33382
94	0.23163	1.91165	0.33273
95	C.23084	1.86553	0.33166
96	0.23007	2.16237	0.33060
97	0.22930	2.06866	0.32956
98	0.22854	1.99966	0.32853
oc.	0.22730	1.94381	0.32751
100	C. 22706	1.89659	0.32650
101	0.22034	2.19800	0.32551
102	0.22562	2.10241	0.32453
103	0.22491	2.03196	0.32356
104	0.22421	1.57499	0.32261
105	0.22352	1.92662	0.32167
136	0.22284	2.23246	0.32073
107	0.22217	2.13505	0.31981
108	0.22151	2.06320	0.31890
109	0.22085	2.00497	0.31800
110	0.22020	1.95569	0.31711
111	0.21956	2.26583	0.31623
112	0.21893	2.16667	0.31537
113	0.21830	2.09348	0.31451

114 115	0.2173	2.03413 1.98388	0.31366 0.31282
116	0.2164/	2.29820	0.31199
117	0.21587	2.19735	C.31116
118	0.21528	2.12287	0.31035
119	0.21470	2.06243	0.30955
120	0.21412	2.01124	0.30875
121	0.21355 0.21294	2.32964	0.30797
122 123	0.21242	2.22715 2.15142	0.30719 0.30642
124	0.21187	2.08994	0.30565
125	0.21132	2.03785	0.30490
126	0.21078	2.36020	0.30415
127	0.21025	2.25614	0.30341
128	0.20972	2.17919	0.30268
129 130	0.20919	2.11671 2.06374	0.30196
131	0.20816	2.38996	0.30053
132	0.20765	2.28436	0.29982
133	0.20714	2.20624	0.29913
134	0.20665	2.14278	0.29944
135	0.20615	2.08897	0.29775
136 137	0.20566 0.20518	2.41895 2.31186	0.29708
138	0.20470	2.23261	0.29574
139	0.20422	2.16820	0.29508
140	0.20375	2.11357	0.29443
141	0.20329	2.44723	0.29378
142 143	0.20282 0.20237	2.33870 2.25834	0.29314 0.29251
144	0.20191	2.19301	0.29188
145	0.20146	2.13758	0.29126
146	0.20102	2.47484	0.29064
147 148	0.20058 0.20014	2.36490 2.28346	0.29002 0.28942
149	0.19971	2.21724	0.28881
150	0.19929	2.16104	0.28822
151	C.19835	2.50181	0.28763
152	0.19843	2.39050	0.28704
153	0.19801 0.19759	2.30802	0.28646
154 155	C.19718	2.24093 2.18397	0.28588 0.28531
156	0.19678	2.52819	0.28474
157	0.19637	2.41554	0.28418
158	0.19597	2.33203	0.28362
159	0.19557	2.26410	0.28307
160 161	0.19513 0.19479	2.20641 2.55400	0.28252 0.28197
162	0.19440	2.44004	0.28143
163	0.19401	2.35554	0.28089
164	0.19363	2.28678	0.28036
165	0.19325	2.72837	0.27983
166 167	0.19288 0.19251	2.57927 2.46404	0.27931 0.27879
168	0.19214	2.37856	0.27827
169	0.19177	2.30899	0.27776
170	0.19141	2.24989	0.27725
171	0.19105 0.19069	2.60403 2.48755	0.27675
172 173	0.19033	2.40113	0.27625 0.27575
174	0.18998	2.33077	0.27526

175	0.189-3	2.27099	0.27477
170	C • 10 ·	2.62830	0.27428
177	0.18994	2.51060	0.27380
178	0.18859	2.42325	0.27332
179	0.18825	2.35212	0.27285
180	0.18792	2.29168	0.27233
191	0.18758	2.65211	0.27191
132	0.18725	2.53322	0.27144
183	0.18692	2.44496	0.27098
134	0.18659	2.37308	0.27052
185	0.18627	2.31198	0.27007
186	0.18594	2.67547	0.26961
137	0.18562	2.55542	0.26917
188	C.18530	2.46627	0.26872
189	0.18499	2.39365	0.26828
190	0.18467	2.33191	0.26784
191	0.18436	2.69842	0.26740
192	0.18405	2.57722	0.26696
193	0.18374	2.48720	0.26653
194	0.18344	2.41385	0.26611
195	0.18314	2.35149	0.26568
196	0.18283	2.72096	0.26526
197	0.18254	2.59863	0.26484
198	0.18224	2.50776	0.26442
199	0.18194	2.43371	0.26401
200	0.18165	2.37074	0.26359

MM 100	M NSYS 50 10000	FA1 0.50000E-	_	MP CREWS	
	TI 1.00000	ETR 1	ETR 5		
IX				J	ATTTP(J)
1				1	0.74755
2				2	0.60774
3 4		_		3	0.60774
5					
6					
7					
ŝ	168.87079	0.59217			
٥	179.55525				
10	188.97326				
11	139.01822				
12 13	156.04721 168.87079				
14					
15	188.37326		·		
16	139.01822				
17	156.04721				
18	168.87079				
19	179.55525				
20 21	188.87326 139.01822				
22	156.04721				
23	168.87079				
24	179.55525				
25	188.37326				
26	139.01822				
27	155.04721				
28 29	168.87079 179.55525				
30	188.87326				
31	139.01922				
32	156.04721				
33	168.37079				
34	179.55525				
35	188.87326				
36 37	139.01822 156.04721				
38	168.97079				
39	179.55525				
40	188.87326				
41	139.01822				
42	156.04721				
43	168.97079				
44 45	179.55525 168.87326				
46	139.01822		0.62328 0.62536		
47	156.04721	0.64083	0.62569		
48	168.87079				
49	179.55525	0.55693	0.62360		
50	188.87326		0.62172		
51	139.01822	0.71933	0.62364		
52	156.04721	0.64083	0.62397		

53	168.87079	0.59217	0.62337
54	175 25	0.55693	0.62214
55	188.87326	0.52946	C. 62045
56	139.01822		
		0.71933	0.62222
57	156.04721	0.64083	0.62254
58	168.87079	0.59217	0.62202
59	179.55525	0.55693	0.62092
େ	188.37320	0.52946	0.61939
61	139.01822	0.71933	0.62103
62	156.04721	0.64083	0.62135
63	168.87079	0.59217	0.62089
64	179.55525	0.55693	0.61989
65	188.37326	0.52946	0.61849
66	139.01922	0.71933	0.62002
67	156.04721	0.64083	0.62033
68	168.87079	0.59217	0.61992
69	179.55525	0.55693	0.61901
70	188.87326	0.52946	0.61773
71	139.01822	0.71933	0.61916
72	156.04721	0.64083	0.61946
73	168.87079	0.59217	0.61908
74	179.55525	0.55693	0.61824
75	188.87326	0.52946	0.61706
76	139.01822	0.71933	0.61841
77	156.04721	0.64083	0.61870
78	168.87079	0.59217	0.61836
79	179.55525	0.55693	0.61758
30	188.87326	0.52946	0.61648
81	139.01822	0.71933	0.61775
82	156.04721	0.64083	0.61803
83	168.87079	0.59217	
			0.61772
84	179.55525	0.55693	0.61699
85	188.87326	0.52946	0.61596
86	139.01922	0.71933	0.61717
87	156.04721	0.64083	0.61744
88	168.87079	0.59217	0.61715
89	179.55525	0.55693	0.61647
90	188.87326	0.52946	0.61551
91	139.01822	0.71933	C.61665
92	156.04721	0.64083	0.61691
93	168.27079	0.59217	0.61664
94	179.55525	0.55693	0.61601
95	188.87326	0.52946	0.61510
96	139.01822	0.71933	0.61618
97	156.04721	0.64083	0.61644
98	168.87079	0.59217	0.61619
99	179.55525	0.55693	0.61559
100	188.87326	0.52946	0.61473
101	139.01822	0.71933	0.61577
102	156.04721	0.64083	0.61601
103	168.87079	0.59217	0.61578
104	179.55525	0.55693	0.61521
105	188.87326	0.52946	0.61440
196	139.01822	0.71933	0.61539
107	156.04721	0.64083	0.61563
109	168.87079	0.59217	0.61541
109	179.55525	0.55693	0.61487
110	188.37326	0.52946	0.61409
111	139.01822	0.71933	0.61504
112	156.04721	0.64083	0.61527
	168.87079		0.61507
113	100.01014	0.59217	0.01301

114	179.55525	0.55693	0.61456	
115	1.55	0. 2946	0.6138?	
116	139.01322	0.71933	0.61473	
117	156.04721	0.64083	0.61495	
118	168.37079	0.59217	0.61476	
119	179.55525	0.55693	0.61427	
120	188.87326	0.52946	0.61357	
121	139.01522	0.71933		
122	155.04721	0.64083	0.61444 0.61466	
123	168.87079	0.59217	0.61447	
124	179.55525	0.55693	0.61401	
125	188.87326	0.52946	0.61333	
125	139.01622	0.71933	0.61417	
127	156.04721	0.64083	0.61417	
128	168.87079	0.59217		
120	179.55525	0.55693	0.61421	
130	189.87326	0.52946	0.61377	
131	139.01822	0.71933	0.61312	
132	156.04721		0.61393	
		0.64083	0.61413	
133	168.57079	0.59217	0.61397	
134	179.55525	0.55693	0.61354	
135	189.87326	0.52946	0.61292	
136	139.01822	0.71933	0.61370	
137	155.04721	0.64083	0.61390	
138	168.87079	0.59217	0.61374	
139	179.55525	0.55693	0.61333	
140	188.37326	0.52946	0.61273	
141	139.01822	0.71933	0.61349	
142	156.04721	0.64083	0.61368	
143	168.87079	0.59217	0.61353	
144	179.55525	0.55693	0.61314	
145	188.87325	0.52946	0.61256	
146	139.01822	0.71933	0.61329	
147	156.04721	0.64083	0.61348	
146	168.87079	0.59217	0.61334	
149	179.55525	0.55693	0.61296	
150	188.87326	0.52946	0.61240	
151	139.01822	0.71933	0.61311	
152	156.04721	0.64083	0.61329	
153	168.87079	0.59217	0.61315	
154	179.55525	0.55693	0.61279	
155	188.87326	0.52946	0.61225	
156 157	139.71822 156.04721	0.71933	0.61294	
158		0.64083	0.61311	
159	168.87079 179.55525	0.59217 0.55693	0.61298 0.61263	
	183.87326			
160 161		0.52946	0.61211	
152	139.01822 156.04721	0.71933 0.64083	0.61277	
163	168.87079		0.61295	
164	179.55525	0.59217	0.61248	
165	188.87326	0.55693 0.52946	0.61198	
166				
167	139.01822 156.04721	0.71933 0.64083	0.61262	
			0.61279	
168	168.87079	0.59217	0.61267	
169	179.55525	0.55693	0.61234	
170	188.37326	0.52946	0.61185	
171	139.01822	0.71933	0.51248	
172	156.04721	0.64083	0.61264	
173	168.87079	0.59217	0.61253	
174	179.55525	0.55693	0.61221	

175	188,37326	0.52946	0.61173
176	139.01 22	C.71933	0.61235
177	150.09721	0.64083	0.61251
178	158.87079	0.59217	0.61239
179	179.55525	0.55693	0.61208
180	188.87326	0.52946	0.61162
181	139.01822	0.71933	0.61222
182	156.04721	0.64083	0.61238
193	168.87079	0.59217	0.61226
184	179.55525	0.55693	0.61196
185	188.87326	0.52946	0.61152
136	139.01822	0.71933	0.61210
187	156.04721	0.64083	0.61225
188	168.87079	0.59217	0.61214
189	179.55525	0.55693	0.61185
190	188.87326	0.52946	0.61142
191	139.01822	0.71933	0.61198
192	156.04721	0.64093	0.61213
193	168.87079	0.59217	0.61203
194	179.55525	0.55693	0.61175
195	188.87326	0.52946	0.61132
196	139.01822	0.71933	0.61188
197	155.04721	0.64083	0.61202
198	168.87079	0.59217	0.61192
199	179.55525	0.55693	0.61165
200	188.87326	0.52946	0.61123

MM 100		SYS D 00 0.500	FAILR POCE-03	TIMP C	REWS Q 10 0.80000
	TI 1.00000	E TR 5 • 00000			
X123456789012345678901234567890123456789012345678901	TN(1X) 1.0000 0.80300 0.70210 0.64000 0.59566 0.59566 0.53449 0.51200 0.47651 0.44935 0.44235 0.44235 0.44235 0.44235 0.4521 0.44235 0.4521 0.44235 0.38127 0.384207 0.38548 0.38568	TOTN(IX) 1.00000 1.00000 1.00000 1.00000 1.00000 1.28067 1.19896 1.15658 1.1297 1.1111 1.55662 1.42614 1.35224 1.36248 1.59536 1.50159 1.43704 1.38889 1.51685 1.73343 1.62489 1.54928 1.49233 2.05328 1.85157 1.73111 1.64660 1.58254 2.17290 1.95566 1.82515 1.73312 1.66306 2.28006 2.04924 1.90995 1.8138 1.73611 2.37754 2.13458 1.98749 1.88311 1.80320 2.46727 2.21329 2.05913 1.94950 2.55060	AVGTN(1X) 1.00000 0.90000 0.83403 0.78553 0.74755 0.67856 0.66824 0.66826 0.6683154 0.6683154 0.6683154 0.58960 0.5834 0.58377 0.55428 0.55428 0.55428 0.55428 0.47668	ATTPN(J) 0.74755 0.51553 0.43903	1.00000 1.17888
			_		

02 0.26484 2.41972 0.3774 03 0.26348 2.24752 0.3755 64 0.26214 2.12452 0.3738 55 0.26084 2.62982 0.3720 60 0.25956 2.77134 0.3703 67 0.25831 2.48090 0.3687 68 0.25708 2.30346 0.3670 69 0.25587 2.17660 0.3654 70 0.25469 2.67882 0.3638 71 0.25353 2.83727 0.3623 72 0.25239 2.53905 0.3607 73 0.25127 2.35668 0.3592 74 0.25017 2.22618 0.3578 75 0.24910 2.12551 0.3563 76 0.24804 2.90011 0.3549 77 0.24699 2.59453 0.3535 78 0.24597 2.40748 0.3521 79 0.24496 2.27353 0.3508 80 0.24397 2.17014 0.3493 81 0.	53 54 55 56 57 58 59 60	0.27855 0.27603 0.27525 0.27366 0.27210 0.27058 0.26910 0.26765	2.12588 2.01144 1.92354 2.62857 2.35510 2.18848 2.06961 1.97818	0.39552 0.39332 0.39117 0.38907 0.38702 0.38501 0.38305 0.38113
69	62 63 64 65 60 67	0.26484 0.26348 0.26214 0.26084 0.25956 0.25831	2.41972 2.24752 2.12452 2.02982 2.77134 2.48090	0.37740 0.37559 0.37382 0.37208 0.37037 0.36870
76	69 70 71 72 73 74	0.25587 0.25469 0.25353 0.25239 0.25127 0.25017	2.17660 2.07882 2.83727 2.53905 2.35668 2.22618	0.36545 0.36386 0.36231 0.36078 0.35928 0.35781
32 C.24204 2.64761 0.34558 83 0.24110 2.45612 0.34558 84 C.24017 2.31890 0.34432 85 0.23926 2.21291 0.34306 86 0.23836 3.01785 C.34187 87 0.23747 2.69854 0.33949 89 0.23574 2.36246 0.33832 90 0.23490 2.25400 0.33717 91 0.23406 3.07325 0.33604 92 0.23324 2.74753 0.33382 93 0.23243 2.54774 0.33382 94 0.23163 2.40440 0.33273 95 0.23084 2.29358 0.33166 96 0.23007 3.12663 0.32956 96 0.22936 2.79474 0.32956 99 0.22780 2.44485 0.32751 100 0.22706 2.33177 0.32650 101 0.22634 3.17815 0.32551 102 0.22562 2.84033 0.32453 <t< th=""><th>76 77 78 79 80 81</th><th>0.24804 0.24699 0.24597 0.24496 0.24397</th><th>2.90011 2.59453 2.40748 2.27353 2.17014</th><th>0.35636 0.35493 0.35353 0.35215 0.35080 0.34946 0.34815</th></t<>	76 77 78 79 80 81	0.24804 0.24699 0.24597 0.24496 0.24397	2.90011 2.59453 2.40748 2.27353 2.17014	0.35636 0.35493 0.35353 0.35215 0.35080 0.34946 0.34815
89 0.23574 2.36246 0.33832 90 0.23490 2.25400 0.33717 91 0.23406 3.07325 0.33604 92 0.23324 2.74753 0.33492 93 0.23243 2.54774 0.33382 94 0.23163 2.40440 0.33273 95 0.23084 2.29358 0.33166 96 0.23007 3.12663 0.32956 97 0.22930 2.79474 0.32956 96 0.22854 2.59106 0.32953 99 0.22706 2.33177 0.32650 101 0.22634 3.17815 0.32551 102 0.22562 2.84033 0.32453 103 0.22421 2.63290 0.32356 104 0.22421 2.48394 0.32261 105 0.22352 2.36868 0.32167 106 0.22284 3.22798 0.32073 107 0.22217 2.88443 0.31890 109 0.22035 2.52177 0.31800	83 84 85 86 87	0.24110 0.24017 0.23926 0.23836 0.23747	2.64761 2.45612 2.31890 2.21291 3.01785 2.69854	0.34685 0.34558 0.34432 0.34309 0.34187 0.34067
96 0.23007 3.12663 0.33060 97 0.22930 2.79474 0.32956 96 0.22854 2.59106 0.32953 99 0.22706 2.33177 0.32650 101 0.22634 3.17815 0.32551 102 0.22562 2.84033 0.32453 103 0.22491 2.63290 0.32356 104 0.22421 2.48394 0.32261 105 0.22352 2.36868 0.32167 106 0.22284 3.22798 0.32073 107 0.22217 2.88443 0.31961 108 0.22151 2.67338 0.31890 109 0.22035 2.52177 0.31800 109 0.22035 2.52177 0.31800 110 0.22020 2.40442 0.31711 111 0.21956 3.27623 0.31623 112 0.21893 2.92715 0.31537	89 90 91 92 93 94	0.23574 0.23490 0.23406 0.23324 0.23243 0.23163	2.36246 2.25400 3.07325 2.74753 2.54774 2.40440	0.33949 0.33832 0.33717 0.33604 0.33492 0.33382 0.33273
102 0.22562 2.84033 0.32453 103 0.22491 2.63290 0.32356 104 0.22421 2.48394 0.32261 105 0.22352 2.36868 0.32167 106 0.22284 3.22798 0.32073 107 0.22217 2.88443 0.31961 103 0.22151 2.67338 0.31890 109 0.22035 2.52177 0.31800 110 0.22020 2.40442 0.31711 111 0.21956 3.27623 0.31623 112 0.21893 2.92715 0.31537	96 97 95 99 100	0.23007 0.22930 0.22854 0.22780 0.22706 0.22634	3.12643 2.79474 2.59106 2.44485 2.33177	0.32956 0.32953 0.32751 0.32650
109 0.22035 2.52177 0.31800 110 0.22020 2.40442 0.31711 111 0.21956 3.27623 0.31623 112 0.21893 2.92715 0.31537	103 104 105 106 107	C.22491 O.22421 O.22352 O.22284 O.22217	2.84033 2.63290 2.48394 2.36868 3.22798 2.88443	0.32453 0.32356 0.32261 0.32167 0.32073 0.31961
	109 110 111 112	0.22035 0.22020 0.21956 0.21893	2.52177 2.40442 3.27623 2.92715	0.31800 0.31711 0.31623 0.31537

114	0.2176	2.55845	0.31366
115	0.217	2.43908	0.31262
116	0.21647	3.52304	0.31199
117	0.21567	2.96859	0.31116
118	0.21523	2.75069	0.31035
119	0.21470	2.59405	0.30955
120	0.21412	2•47273	0.30875
121	0.21355	3•36849	0.30797
122	0.21298	3•00886	0.30719
123	0.21242	2.78769	0.30642
124	0.21187	2.62865	
125	0.21132	2.50544	0.30490
12e	0.21078	3.41268	0.30415
127 129 129	0.21025 0.20972 0.20919	3.04802 2.82368	0.30341
130 131	0.20919 0.20867 0.20816	2.66232 2.53727 3.45571	0.30196 0.30124 0.30053
132	0.20765	3.08614	0.29982
133	0.20714	2.85873	
134	0.20565	2.69511	0.29844 · 0.29775
135	0.20615	2.56829	
136	0.20565	3.49763	0.29708
137	0.20518	3.12330	0.29641
138 139 140	0.20470 0.20422	2.89289 2.72708	0.29574
141 142	0.20375 0.20329 0.20282	2.59853 3.53852 3.15955	0.29443 0.29378 0.29314
143	0.20237	2.92523 2.75829	0.29251 0.29183
145	0.20146	2.62805	0.29126
146	0.20102	3.57844	0.29064
147	0.20058	3.19495	0.29002
	0.20014	2.95879	0.28942
149	0.19971	2.78876	0.28881
150	0.19923	2.65689	0.28822
151	0.19835	3.61744	0.28763
152	0.19843	3.22954	0.28704
153	0.19801	2.99060	0.28646
154	0.19759	2.81855	0.23588
155	0.19718	2.68509	0.23531
156	C.19678	3.65558	0.28474
157	C.19637	3.26336	0.28418
158	0.19597	3.02172	0.28362
159	0.19557	2.84769	0.28307
160	0.19518	2.71267	0.28252
151	0.19479	3.69290	C.28197
152		3.29647	C.29143
163	0.19401	3.05218	0.28089
164	0.19363	2.87622	0.28036
165 166	0.19325	2.73968 3.72743	0.27983
167	0.1925l	3.32889	0.27879
168	0.19214	3.08202	0.27827
169	0.19177	2.90416	0.27776
170 171	0.19141	2.76614 3.76524	0.27725
172	0.19069	3.36065	0.27625
173	0.19033	3.11125	0.27575
174	0.18998	2.93155	0.27526

175	0.18963	2.79207	0.27477
176	0.108.5	3.80033	0.27428
177	0.18994	3.39179	0.27380
178	0.18859	3.13992	0.27332
179	0.18825	2.95841	0.27285
180	0.18792	2.81751	0.27238
181	0.18758	3.83476	0.27191
132	0.18725	3.42235	0.27144
183	0.18692	3.16805	0.27098
184	C.19659	2.98476	0.27052
185	0.18627	2.84247	0.27007
186	0.18594	3.86855	0.26961
187	0.18562	3.45234	0.26917
188	0.18530	3.19566	0.26872
189	0.18499	3.01064	0.26828
190	0.18467	2.86698	0.26784
191	0.18436	3.90173	0.26740
192	0.13405	3.48179	0.26696
193	0.19374	3.22278	0.26653
194	0.18344	3.03605	0.26611
195	0.18314	2.89105	0.26568
196	0.18283	3.93432	0.26526
197	0.18254	3.51073	0.26484
198	0.18224	3.24942	0.26442
199	0.18194	3.06102	0.26401
200	0.18165	2.91471	0.26359

MM 100	M 10	NSYS 20000	0.500	FAILR OCE-03		TIMP 0000	CREWS 10	0.80000
	1.000	T1 00	FTR 10.00000	IFT				
1 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 1 1 1 1 1 1 1 2 2 2 2 2 2 2 2 2 3 3 3 3	1.000	700 R (IX 100 00 00 00 00 00 00 00 00 00 00 00 00	10.00000 10.00000 10.00000 10.00000 10.0000	100000 1000000	0 AVG 0000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00	00335764642424740968461328229110056255158754471903	J 1 2 3 4 5 6 7 8 9 10 11	ATTTP(J) 0.63154 0.43082 0.37497 0.34566 0.32768 0.30812 0.30306 0.30006 0.29870 0.29870
51 52		298.8369 304.0332			0.4204			

53	308-40137	0.32425	0.41688
5.	312. 1 175	0.32016	0.41503
55	315.00781	0.31645	0.41329
56	319.46777	0.31302	0.41150
57	322.7666C	0.30982	0.40972
5.9	325.93335	0.30681	0.40794
59	328.93779	0.30396	0.40618
60	331.94409	0.30126	0.40443
61	307.25244	0.32547	0.40314
62	312.34790	0.32016	0.40180
63	316.61616	0.31584	0.40043
64	320.46533	0.31205	0.39905
65	324.03711	0.30861	0.39766
66	327.40723	0.30543	0.39626
67	330.61865	0.30246	0.39486
63	333.70044	0.29967	0.39346
69	336.67187	0.29703	0.39206
70	339.54785	0.29451	
71	312.09548	0.31959	0.39067
72	317.93433		C. 38967
73	322.14844	0.31453	0.38863
74	325.94116	0.31042	0.38755
75	329.45947	0.30680	0.38646
76	332.77759	0.30353	0.38536
77		0.30050	0.38424
	335.93823	0.29767	0.38312
78	338.97021	0.29501	0.38199
79	341.89331	0.29249	C.38085
80	344.72192	0.29009	C. 37972
81	316.31470	C.31614	0.37893
32	321.32251	0.31121	0.37911
83	325.50708	0.30721	0.37725
84	329.27075	0.30370	0.37638
85	332.76074	0.30052	0.37549
35	336.05103	0.29757	0.37458
87	339.18457	0.29482	0.37366
88	342.18970	0.29224	0.37274
69	345.08667	0.28978	0.37180
90	347.88965	C.28745	C.37087
91	317.83599	0.31458	C.37025
92	322.88135	0.30971	0.36959
93	327.05396	0.30576	0.36890
94	330.30591	0.30229	0.36820
95	334.28418	0.29915	0.36747
96	337.56299	0.29624	0.36673
97	340.68579	0.29353	0.36597
98	343.68018	0.29097	0.36521
99	346.56592	0.28855	0.36443
00	349.35815	0.28624	0.36365
101	317.88599	0.31458	0.36316
102	322.88135	0.30971	0.36264
.73	327.05396	0.30576	0.36209
.94	330.80591	0.30229	0.36151
.05	334.28418	0.29915	n. 36092
.06	337.56299	0.29624	0.36031
07	340.68579	0.29353	0.35968
96	343.68018	0.29097	0.35905
03	346.56592	0.28855	0.35840
10	349.35815	0.28624	0.35774
.11	317.88599	0.31458	0.35736
12	322.88135	0.30971	0.35693
13	327.05396	0.3057	35648

F F &	220, 174 <u>1</u>	0.30229	0.35600
115	* 7. 4	0.29915	0.35551
116	337.002.19	0.29524	0.35500
117			
	340.68579	0.29353	0.35447
118	343.65019	0.29097	0.35393
119	346.56592	0.28855	0.35338
120	349.35815	0.28624	0.35282
121			
	317.38599	0.31458	0.35251
122	322.88135	0.30471	0.35216
123	327.05396	0.30576	0.35178
124	330.80591	0.30229	0.35138
125	334.28418	0.29915	0.35096
126	337.56299	0.29624	0.35053
127	340.68579	0.29353	0.35008
123	343.68018	0.29097	0.34962
129	346.56592	0.28855	0.34914
130	349.35815	0.28524	
			0.34866
131	317.38599	0.31458	0.34840
132	322.35135	0.30971	0.34811
133	327.05396	0.30576	0.34779
134	330.80591	0.30229	0.34745
135	334.28418	0.29915	0.34709
136	337.56299	0.29624	0.34672
137	340.08579	0.29353	0.34633
139	343.60018	0.29097	0.34593
_			
139	346.56592	0.28855	0.34551
140	349.35815	0.28524	0.34509
141	317.88599	0.31458	0.34487
142	322.88135	0.30971	0.34463
143	327.05396	2.30576	0.34436
144	330.80591	0.30229	0.34406
145	334.28418	0.29915	0.34375
146	337.56299	0.29624	0.34343
147	340.56579	0.29353	0.34309
148	343.68018	0.29097	r.34274
149	346.56592	0.28855	0.34237
150	349.35815	C.28624	0.34200
151	317.38599	0.31458	0.34182
152	322.88135	0.30971	0.34161
153	327.05396	0.30576	0.34137
154	330.80591	0.30229	0.34112
155	334.28418	0.29915	0.34085
156	337.56299	0.29624	0.34056
	340.68579	0.29353	0.34026
157			
156	343.58018	0.29097	0.33995
159	346.56592	0.28855	0.33963
160	349.35315	0.28624	0.33929
161	317.88599	0.31458	C. 33914
			0.33896
152	322.88135	0.30971	
163	327.05396	0.30576	C.33875
164	330.80591	0.30229	0.33853
165	334.28418	0.29915	0.33829
166	337.55299	0.29624	0.33804
167	340.68579	0.29353	0.33777
168	343.68018	0.29097	0.33749
169	346.56592	0.28855	0.33720
170	349.35815	0.28624	0.33690
			0.33677
171	317.88599	0.31458	
172	322.88135	0.30971	0.33662
173	327.05396	0.30576	0.33644
174	330.80591	0.30229	0.33624

175	334.28413	0.29915	0.33603
176	33 1. 16 99	0.29624	0.33580
177	340.08579	0.29353	0.33556
178	343.68018	0.29097	0.33531
179	346.56592	0.28855	0.33505
180	349.35815	0.28624	0.33478
191	317.88599	0.31458	0.33467
182	322.88135	0.30971	0.33453
193	327.05396	0.30576	0.33437
194	330.80591	0.30229	0.33420
185	334.28418	0.29915	0.33401
136	337.56299	0.29624	0.33381
187	340.68579	0.29353	0.33359
188	343.68018	0.29097	0.33337
189	346.56592	0.28855	0.33313
190	349.35815	0.28624	0.33288
191	317.88599	0.31458	0.33279
192	322.58135	0.30971	0.33267
193	327.05396	0.30576	0.33253
194	330.30591	0.30229	0.33237
195	334.28418	0.29915	0.33220
196	337.56299	0.29624	0.33202
197	340.68579	0.29353	0.33182
198	343.68018	0.29097	0.33161
199	346.56592	0.28855	0.33140
200	349.35815	0.28624	0.33117

MM 100		NSYS 20000	0.500	FAILR OOE-03	TIMP 10.0000	CREWS 10	0.80000
1	TI 000000	1	FTR 0.00000	IETR 10			
1123456789012345678901234567890123456789012345678901234567890123456789012	1.000 1.0000 1.00000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.0000 1.	11 1000 1000 1000 1000 1000 1000 1000	.00000 .000000	AVGTN(IX) 1.00000 0.90000 0.93403 0.78553 0.74755 0.71657 0.66824 0.64876 0.63154 0.63154 0.58802 0.57837 0.557731 0.55837 0.553178 0.53178 0.53178 0.5244 0.4988 0.4988 0.48688	ATTPN C.63 O.41 C.35 O.27 O.26 O.24 O.23 O.23 O.22	154 696 350 736 283 461 030 864 886	ATDAN(J) 1.00000 1.03326 1.06075 1.08919 1.11902 1.15047 1.18370 1.21889 1.25622 1.29590 1.33816

53	0.27855	1.16406	0.39552
54	0.276.	1.15631	0.39332
55	0.27525	1.14967	0.39117
56	0.27366	1.14384	0.38907
57	0.27210	1.13861	0.38702
58	0.27058	1.13388	0.38501
59	0.26910	1.12955	0.38305
	0.26765		
60		1.12557	0.38113
51	0.26623	1.22251	0.37924
62	0.26484	1.20888	0.37740
63	0.26343	1.19873	0.37559
64	0.26214	1.19036	0.37382
65	0.26084	1.18313	0.37208
66	0.25956	1.17672	0.37037
67	0.25831	1.17095	0.36870
68	0.25708	1.16568	0.36706
69	0.25587	1.16093	0.36545
70	0.25409	1.15634	0.36386
71	0.25353	1.26058	0.36231
72	0.25239	1.24621	0.36078
73	0.25127	1.23538	0.35928
74	0.25017	1.22636	0.35781
75	0.24910	1.21852	0.35636
76	0.24834	1.21152	0.35493
77	0.24699	1.20519	0.35353
78	0.24597	1.19938	0.35215
79	0.24495	1.19401	0.35080
80	0.24397	1.18902	0.34946
81	0.24300	1.30099	0.34815
82	0.24204	1.28579	0.34685
	0.24110	1.27422	
83			0.34558
84	0.24017	1.26452	0.34432
85	0.23926	1.25603	0.34309
86	0.23836	1.24843	0.34187
87	0.23747	1.24151	0.34067
88	0.23660	1.23514	0.33949
89	0.23574	1.22923	0.33832
90	0.23490	1.22372	0.33717
91	0.23406	1.34400	0.33604
92	0.23324	1.32787	0.33492
93	0.23243	1.31550	0.33382
94	0.23163	1.30506	0.33273
95	0.23084	1.29589	0.33166
96	0.23007	1.28764	0.33060
97	0.22930	1.28010	0.32956
95	0.22854	1.27314	0.32853
99	0.22780	1.26667	C.32751
100	0.22706	1.26062	0.32650
101	0.22634	1.38987	0.32551
102	0.22562	1.37272	0.32453
103	0.22491	1.35947	0.32356
104	C.22421	1.34824	0.32261
105	0.22352	1.33832	0.32167
106	0.22284	1.32938	0.32073
107	0.22217	1.32118	0.31981
108	0.22151	1.31359	0.31890
109	0.22085	1.30653	0.31800
		1.29990	0.31711
110	0.22020		0.31623
111	0.21956	1.43277 1.41468	0.31523
112	0.21893	1.40063	
113	0.21830	1.40003	0.31451

114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130	0.21/5m 0.21/64/ 0.21567 0.21528 0.21470 0.21412 0.21355 0.21298 0.21242 0.21187 0.21132 0.21078 0.21025 0.20972 0.20979 0.20867	1.38868 1.37810 1.36852 1.35973 1.35158 1.34397 1.33683 1.47311 1.45417 1.43939 1.42678 1.41559 1.40544 1.39611 1.38744 1.37934 1.37172	0.31366 0.31282 0.31199 0.31116 0.31035 0.30955 0.30875 0.30797 0.30719 0.30642 0.30565 0.30415 0.30268 0.30196 0.30124
131 132	0.20816 0.20765	1.51125 1.49152	0.30053 0.29982
133	0.20714	1.47607	0.29913
134	0.20665	1.46285	0.29844
135 136	0.20615 0.20566	1.45110	0.29775 0.29708
137	0.20518	1.43059	0.29641
138	0.20470	1.42145	0.29574
139	0.20422	1.41290	0.29508
140 141	0.20375 0.20329	1,40484 1,54747	0.29443 0.29378
142	0.20232	1.52700	0.29314
143	0.20237	1.51093	0.29251
144 145	0.20191 0.20146	1.49715	0.29188
145	0.20148	1.48487 1.47371	0.29126 0.29064
147	0.20058	1.46341	0.29002
148	0.20014	1.45383	C.28942
149 150	0.19971 0.19928	1.44485 1.43639	0.28831 0.28822
151	0.19885	1.58198	0.28763
152	0.19843	1.56082	0.28704
153	0.19801	1.54417	0.28646
154 155	0.19759 0.19718	1.52986 1.51710	0.28588 0.28531
156	0.19678	1.50548	0.28474
157	0.19637	1.49475	0.28418
158 159	0.19597 0.19557	1.48475 1.47538	0.28362 0.28307
160	0.19518	1.46655	0.28252
161	0.19479	1.61498	0.28197
162	0.19440	1.59317	0.28143
163 164	0.19401 0.19363	1.57596 1.56116	0.28089 0.28036
165	0.19325	1.54794	0.27983
166	0.19288	1.53589	0.27931
167 168	0.19251 0.19214	1.52476 1.51438	0.27879 0.27827
169	0.19214	1.50464	0.27776
170	0.19141	1.49545	0.27725
171	0.19105	1.64662	0.27675
172 173	0.19069 0.19033	1.62419 1.60646	0.27625 0.27575
174	0.18998	1.59119	0.27526

175	0.18953	1.57754	0.27477
176	3.189.	1.56509	0.27428
177	0.19454	1.55357	0.27380
178	0.18859	1.54283	0.27332
179	0.18825	1.53275	0.27285
180	0.18792	1.52323	0.27238
191	0.18758	1.67702	0.27191
182	0.18725	1.65401	0.27144
133	0.18692	1.63579	0.27098
134	0.18659	1.62007	0.27052
185	0.19627	1.60602	0.27007
136	0.18594	1.59318	0.26961
187	0.18562	1.58130	0.26917
188	0.18530	1.57022	0.26872
189	0.18499	1.55981	0.26828
190	0.18457	1.54997	0.26784
191	0.18436	1.70631	0.26740
192	0.18405	1.68273	0.26696
193	0.18374	1.66405	0.26653
194	0.18344	1.64791	0.26611
195	0.18314	1.63347	0.26568
196	C.18283	1.62027	0.26526
197	0.18254	1.60805	0.26484
198	0.18224	1.59664	0.26442
199	0.18194	1.58591	0.26401
200	0.18165	1.57578	0.26359

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MM 1 00	M 20	NSYS 20000	0.5000	FAIL OGE-C			TII 10.000	MP CR	EWS 10	0	• 1	80	000
	T1 1.00000	10	ETR •00000	1 8	TR 10								
1x 1 2 3 4 5 6 7 8 9 10 11 12 13 14	10 12 14 15 16 17 18 19 20 20 19 21 21	R (TX) 0.0000 5.00000 2.42908 6.24998 7.88737 8.03636 7.09436 5.31244 2.86049 9.85918 3.11952 3.03636 1.16942 8.34438	T(1.00 0.80 0.70 0.64 0.59 0.56 0.51 0.49 0.47 0.47	0000 0210 0000 0564 0168 0295 0295 0782 0252 0799		AVG 1000000000000	T(IX) 0C000 90000 83403 78553 74755 71657 69056 66824 64876 63154 62120 61048 59994 58980	J 1 2 3 4 5 6		0.6 0.4 0.3 0.3 0.3	3:4:9:7:7:7:	15 57 93 97 22	4 6 9 2 1
15 16 17 18 19 20 21 22 23 24 25	23 24 24 25 22 23 23 24 25	4.87386 0.91975 5.58063 1.92294 6.99440 1.83105 3.16583 1.80775 8.79453 4.93269 0.51860 5.70117	0.44 0.43 0.42 0.41 0.40 0.39 0.41 0.40 0.39	3305 2269 335 3487 3709 810 3139 877 8828		0. : 0. : 0. : 0. : 0. :	58013 57094 56222 55395 54610 53865 53434 52966 52484 51998 51515						
27 28 29 30 31 32 33 34 35 36	26 26 27 23 24 25 25 26	0.56860 5.17822 9.57104 3.77686 7.40404 5.67889 2.32158 8.13599 3.41675 8.31152 2.90674	0.38 0.37 0.37 0.36 0.42 0.40 0.39 0.38 0.37	378 7710 7096 526 2122 7704 9632 7739 7963 270		0.5	50569 50110 49661 49223 48994 48735 48459 48459 47881 47587						
38 39 41 42 44 45 44 45 51 51	27 28 24 25 25 26 27 27 28 28 29 24	7.2583C 1.40601 5.37866 3.09402 1.26303 7.8C4444 3.52222 8.71C69 3.51665 8.02686 2.29688 5.36597 0.26294 3.09402 1.26303	0.36 0.35 0.35 0.41 0.39 0.38 0.37 0.36 0.35 0.34 0.34	067 0536 041 136 0799 789 789 789 789 789 789 789 789 789		0.4	46995 46702 46410 46281 46127 45956 45774 45588 45187 44984 44779 44572 44505						

53	257, 30444	0.38789	0.44308
54	26 2	0.37947	0.44190
55	268.71069	0.37215	0.44063
56	273.51685	0.36561	0.43929
57	278.02686	0.35968	0.43790
58	232.29638	0.35424	0.43646
59	286.36597	0.34920	-
			0.43498
60	290.26294	0.34452	0.43347
61	243.09402	0.41136	0.43311
62	251.26303	0.39799	0.43254
63	257.80444	0.38789	0.43183
64	263.52222	0.37947	0.43101
65	268.71069	0.37215	0.43011
66	273.51685	0.36561	0.42913
67	278.02686	0.35968	0.42809
68	282.29688	0.35424	
			0.42701
69	286.36597	0.34920	0.42588
70	290.26294	0.34452	0.42472
71			
	243.09402	0.41136	0.42453
72	251.26303	0.39799	0.42416
73	257.80444	0.38789	0.42366
74	263.52222	0.37947	0.42307
75	268.71069	0.37215	0.42239
76	273.51685	0.36561	0.42164
77	278.02666	0.35968	0.42083
78	282.29688	0.35424	0.41998
79	286.36597	0.34920	0.41908
80	290.26294	0.34452	0.41815
81	243.09402	0.41136	0.41807
32	251.26303	0.39799	0.41782
83	257.80444	0.3878 9	0.41746
84	263.52222	0.37947	0.41701
85	268.71069	0.37215	0.41648
86	273.51685	0.36561	0.41589
87	278.02686	0.35968	0.41524
88	282.29688	0.35424	0.41455
89	286.36597	0.34920	0.41382
90	290.26294	0.34452	0.41305
91	243.09402	0.41136	0.41303
92	251.26303	C.39799	0.41286
93	257.30444	0.38789	0.41260
94	263.52222	0.37947	0.41224
95	268.71069	0.37215	0.41182
96	273.51685	0.36561	0.41134
97	278.02686	0.35968	0.41091
98	282.29688	0.35424	0.41023
99	286.36597	0.34920	0.40961
105	290.26294	0.34452	0.40896
101	243.09402	0.41136	0.40899
102	251.26303	0.39799	0.40888
103	257.80444	0.38789	0.40867
104	263.52222	0.37947	0.40839
105	268.71069	C.37215	0.40805
106	273.51685	0.36561	0.40765
07	278.02686	0.35968	0.40720
108	282.29688	0.35424	0.40671
.09	286.36597	0.34920	0.40618
110	290.26294	0.34452	0.40562
111	243.09402	0.41136	0.40567
112	251.26303	0.39799	0.40560
13	257.80444	0.38789	0.40545
	271800444	V = 30107	0870772

114	263.52222	0.3/947	0.40522
115	24 7	0.77215	0.40493
110	273.51685	0.30561	0.40459
117	278.02686	0.55968	0.40421
118	282.29686	0.35424	0.40379
110	286.36597	0.34920	0.40333
120	290.26294	0.34452	0.40284
121	243.09402	0.41136	0.40291
122	251.26303	0.39799	0.40291
123	257.80444		
124	263.52222	0.38789	0.40274 0.40256
125		0.37947	
	268.71069	0.37215	0.40231
126	273.51685	0.36561	0.40202
127	278.02686	0.35968	0.40169
128	282.29688	0.35424	0.40132
129	286.36597	0.34920	0.40091
130	290.26294	0.34452	0.40048
131	243.09402	0.41136	0.40056
132	251.26303	0.39799	0.40054
133	257.80444	0.38789	0.40045
134	263.52222	0.37947	0.40029
135	268.71069	0.37215	0.40008
136	273.51685	0.36561	0.39983
137	278.02686	0.35968	0.39954
138	282.29688	0,35424	0.39921
139	286.36597	0.34920	0.39885
140	290.26294	0.34452	0.39846
141	243.09402	0.41136	0.39855
142	251.26303	0.39799	0.39855
143	257.80444	0.38789	0.39847
144	263.52222	0.37947	0.39834
145	268.71069	0.37215	0.39816
146	273.51695	0.36561	0.39794
147	278.02686	0.35968	0.39768
148	282.29688	0.35424	0.39738
149	286.36597	0.34920	0.39706
150	290.26294	0.34452	0.39671
151	243.09402	0.41136	0.39681
152	251.26303	0.39799	0.39681
153	257.80444	0.38789	0.39676
154	263.52222	0.37947	0.39664
155	268.71069	0.37215	0.39649
156	273.51685	0.36561	0.39629
157	278.02666	0.35968	0.39605
158	282.29688	0.35424	0.39579
159	286.36597	0.34920	0.39550
160	290.26294	0.34452	0.39518
161	243.09402	0.41136	0.39528
152	251.26303	0.39799	0.39530
	257.80444		
163		0.38789	0.39525
164	263.52222	0.37947	0.39515
165	268.71069	0.37215	0.39501
166	273.51685	0.36561	0.39484
167	278.02686	0.35968	0.39463
108	282.29688	0.35424	0.39439
169	286.36597	0.34920	0.39412
170	290.26294	0.34452	0.39383
171	243.09402	0.41136	0.39393
172	251.26303	0.39799	0.39395
173	257.80444	0.33789	0.39392
174	263.52222	0.37947	0.39384

175	268.71069	0.37215	0.39371
176	273. 10.5	0.36561	0.39355
177	278.02686	0.35968	0.39336
178	282.29688	0.35424	0.39314
179	286.30597	0.34920	0.39289
180	290.26294	0.34452	0.39263
181	243.09402	0.41136	0.39273
182	251.26303	0.39799	
183	257.80444	C.38789	0.39276
184	263.52222	0.37947	0.39273
185	269.71069	0.37215	0.39266
186	273.51685	0.36561	0.39255
187	278.02686	0.35968	0.39240
188	282.29688	0.35424	0.39223
139	286.36597	0.34920	0.39203
190	290.26294	0.34452	0.39180
191	243.09402	0.41136	0.39155
192	251.26303	0.39799	0.39165
193	257.80444	0.38789	0.39169
194	263.52222	0.37947	0.39167
195	268.71069		0.39161
196	273.51685	0.37215	0.39151
197	278.02686	0.36561	0.39137
198	282.29688	0.35968	0.39121
199	286.36597	0.35424	0.39103
200	290.26294	0.34920	0.39082
	270020294	0.34452	0.39059

М 20	NSYS 20000	0.5000	FAILR DOE-03	TIMP 10.0000	CREWS 10	0.80000
TI 1.000C0	ì	ETR 0.00000	IETR 10			
1.000C0 TNC0 1.00C0 TNC0 0.80 0.656 0.657 0.659 0.657 0.659 0.657 0.659 0.657 0.659	IX) TO 10000 1 100000 1 10000 1 10000 1 10000 1 100000 1 100000 1 10000 1 10000 1 100000 1 10000 1 10000 1 100	0.00000 IN(IX) .000000 .000000 .000000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .00000 .0	10 AVGTN(IX) 1.00000 0.83403 0.78553 0.74755 0.71657 0.66924 0.66924 0.66924 0.63154 0.63154 0.63154 0.63154 0.657802 0.55751 0.55751 0.55751 0.531715 0.531715 0.51045 0.49808 0.49808 0.49808 0.49808 0.49808 0.49808 0.49808 0.45871 0.46733 0.45871 0.46733 0.45871 0.46733 0.45871 0.45871 0.46733 0.45871 0.46733 0.42673 0.42673 0.41795 0.4	0.631 0.416 0.353 0.317 0.292	54 96 350 736 183	TDAN(J) 1.00000 1.06909 1.12983 1.19650 1.27110 1.35543
			0.40007 0.39777			
	TION (1.00 CO. 1.00 CO. 649 CO	TI 1.000C0 TN(IX) TD 1.000C0 TN(IX) TD 1.00C00 0.80C00 0.70C210 0.64C00 0.59564 1.0.56168 0.53449 0.51200 0.49295 0.47651 0.46211 0.364644 0.364644 0.364644 0.364644 0.364644 0.364644 0.364644 0.364644 0.364644 0.364644 0.364646 0.364666 0.36466	TI	TI	TI	TI

	0.070-5	1 20252	A 20552
53	0.27955	1.39252	0.39552
54	0.2750 0.27525	1.35203	0.39117
55 56	0.27366	1.33600	0.38907
57	0.27210	1.32184	0.38702
58	0.27058	1.30915	0.38501
59	0.26910	1.29767	0.38305
50	0.26765	1.28720	0.38113
61	0.26623	1.54516	0.37924
62	0.26484	1.50277	0.37740
63	0.26348	1.47220	0.37559
64	0.26214	1.44758	0.37382
65	0.26084	1.42673	0.37208
66	0.25956	1.40857	0.37037
67	0.25831	1.39244	0.36870° 0.36706
68	0.25708	1.37794	0.36545
59	0.25587	1.36476	0.36386
7C	0.25469 0.25353	1.62255	0.36231
71 72	0.25239	1.57688	0.36078
73	0.25127	1.54371	0.35928
74	0.25017	1.51684	0.35781
75	0.24910	1.49400	0.35636
76	0.24804	1.47402	0.35493
77	0.24699	1.45622	0.35353
78	0.24597	1.44016	0.35215
79	0.24495	1.42553	0.35080
50	0.24397	1.41210	0.34946
31	0.24300	1.69286	0.34815
82	0.24204	1.64430	0.34685
83	0.24110	1.60885	0.34558 0.34432
84	0.24017	1.58002 1.55542	0.34309
85	0.23926	1.53386	0.34187
86	C.23836 O.23747	1.51460	0.34067
37 88	0.23660	1.49719	0.33949
39	0.23574	1.48130	0.33832
90	0.23490	1.46667	0.33717
91	0.23406	1.75750	0.33604
92	0.23324	1.70636	0.33492
93	0.23243	1.66886	0.33382
94	0.23163	1.63828	0.33273
95	0.23084	1.61213	0.33166
96	0.23007	1.58915	0.33060
97	0.22930	1.56859	0.32956 0.32853
98	0.22854	1.54998 1.53295	0.32751
99	0.22790	1.51727	0.32650
100	0.22634	1.81749	0.32551
102	0.22562	1.76399	0.32453
103	0.26491	1.72464	0.32356
104	0.22421	1.69247	0.32261
105	0.22352	1.65492	0.32167
100	0.22284	1.64066	0.32073
107	0.22217	1.61893	0.31981
301	0.22151	1.59923	0.31890
109	0.22085	1.58119	0.31800
110	0.22020	1.56455	0.31711 0.31623
111	0.21956	1.87358 1.81791	0.31537
112	0.21993	1.77686	0.31451
113	0.21830	7.11000	0001701

114	C.2175	1.74324	0.31366
115	0.2./	1.71440	0.31282
116 117	0.21647	1.68897	0.31199
118	0.21587 0.21528	1.66617 1.64547	0.31116
119	0.21470	1.62650	0.31035
120	0.21412	1.60900	0.30955 0.30875
121	0.21355	1.92634	0.30797
122	0.21295	1.86865	0.30719
123	0.21242	1.82603	0.30642
124	0.21187	1.79107	0.30565
125 126	0.21132	1.76104	0.30490
127	0.21078 0.21025	1.73454 1.71075	0.30415
128	0.20972	1.68913	0.30341 0.30268
129	0.20919	1.66931	0.30196
130	0.20867	1.65100	0.30124
131	0.20816	1.97522	0.30053
132	0.20705	1.91665	0.29982
133 134	0.20714	1.87255	0.29913
135	0.20665 0.20615	1.83536 1.8052 2	0.29844
136	0.20566	1.77771	0.29775 0.29708
137	0.20513	1.75301	0.29641
138	0.20470	1.73054	0.29574
139	0.20422	1.70992	0.29508
140	0.20375	1.69096	0.29443
141 142	0.20329 0.20282	2.02358	0.29378
143	0.20237	1.96224	0.20314
144	0.20191	1.87940	0.29188
145	0.20145	1.84723	0.29126
146	0.20102	1.81879	0.29064
147 148	0.20053 0.20014	1.79322	0.29007
149	0.19571	1.74859	0.28942
150	0.19928	1.72893	0.23822
151	0.19885	2.06871	0.28763
152	C.19843	2.00571	0.28704
153 154	0.19801	1.95895	0.28646
155	0.19759 0.19718	1.92047 1.88731	0.28588 0.28531
156	0.19678	1.85799	0.28474
157	0.19637	1.83162	0.28418
158	0.19597	1.80760	0.28362
159	0.19557	1.78554	0.29307
160 151	0.19518 0.19479	1.76513 2.11186	0.28252
.62	0.19440	2.04728	0.28197 0.28143
.63	0.19401	1.99929	0.28089
.54	0.19363	1.95976	0.28036
65	0.19325	1.92568	0.27983
.56 .57	0.19288 0.19251	1.89553	0.27931
58	0.19214	1.86839 1.84367	0.27879 0.27827
69	0.19177	1.82095	0.27776
70	0.19141	1.79992	0.27725
71	0.19105	2.15323	0.27675
72 73	0.19069 0.19033	2.08713	0.27625
1.5 74	0.18998	2.03798 1.99746	0.27575 0.27526
	///	44 ///140	C + Z 12Z0

175	0.18963	1.96251	0.27477
175	0.1892	1.93157	0.27428
177	0.18994	1.90370	0.27380
178	0.18859	1.87931	0.27332
179	0.18925	1.85496	0.27285
180	0.18792	1.83334	0.27238
181	0.18758	2.19298	0.27191
182	0.18725	2.12545	0.27144
183	0.18692	2.07518	0.27098
134	0.18659	2.03372	0.27052
185	0.19627	1.99793	9.27007
186	0.18594	1.96624	0.26961
187	0.18562	1.93768	0.26917
138	0.18530	1.91165	0.26872
199	0.19499	1.88771	0.26828
190	C.18467	1.86553	0.26784
191	0.18436	2.23128	0.26740
192	0.18405	2.16237	0.26696
193	0.18374	2.11103	0.26653
194	0.18344	2.06867	0.26611
195	0.18314	2. C3208	0.26568
196	0.18283	1.99966	0.26526
197	0.18254	1.97045	0.26484
198	0.18224	1.94381	0.26442
199	0.18194	1.91930	0.26401
200	0.18165	1.89659	0.26359

MM 100	м 50	NSY5 20000	FAILR 0.50000E-03	TIMP 10.0000	CREWS 10	0.8C000
	Т		ETR LETR			
100	50	20000	ETR 1ETR 10 10 10 10 10 10 10 10 10 10 10 10 10		10	0.8C000 ATTTP(J) 0.63154 0.49865 0.49865
	50 51 52	236.0916 158.1991 173.7727	3 0.63211	0.52732		

62	195.39132	0.53940	0.52845
53 54	195.058.7	0.51267	0.52816
55	203.50394	0.49139	0.52749
56	211.08847	0.47373	0.52653
57	218.02330	0.45867	0.52534
58	224.44403	0.44555	0.52397
59	230.44417	0.43394	0.52244
60	236.09163	0.42356	0.52079
61	158.19913	0.63211	0.52262
62	173.77277	0.57546	0.52372
53	185.39182	0.53940	0.52355
54	195.05899	0.51267	0.52305
65	203.50394	0.47373	0.52231
66	211.08847	0.45867	0.52136
67	218.02330	0.44555	0.52024
68	224.44403 230.44417	0.43394	0.51899
69	236.09163	0.42356	0.51763
70	158.19913	0.63211	0.51924
71 72	173.772 7	0.57546	0.52002
73	185.39182	0.53940	0.52029
74	195.05899	0.51267	0.52018
75	203.50394	0.49139	0.51980
76	211.08847	0.47373	0.51919
77	218.02330	0.45867	0.51841
78	224.44403	0.44555	0.51747
79	230.44417	0.43394	0.51642
30	236.09163	0.42356	0.51525
81	158.19913	0.63211	0.51670 0.51741
82	173.77277	0.57546	0.51768
83	185.39182	0.53940	0.51762
84	195.05899	0.51267 0.49139	0.51731
35	203.50394	0.47373	0.51680
86	211.08847	0.45867	0.51613
37	218.02330	0.44555	0.51533
88	224.44403 230.44417	0.43394	0.51442
89	236.09163	0.42356	0.51341
90	158.19913	0.63211	0.51471
91	173.77277	0.57546	0.51537
92 93	185.39182	0.53940	0.51563
94	195.05899	0.51267	0.51560
95	203.50394	0.49139	0.51534
96	211.08847	0.47373	0.51491
97	218.02330	0.45867	0.51433
98	224.44403	0.44555	0.51363 0.51282
99	230.44417	0.43394	0.51193
100	236.09163	0.42356	0.51312
101	158.19913	0.63211	0.51373
102	173.77277	0.57546 0.53940	C.51398
103	185.39182	0.51267	0.51397
104	195.05899	0.49139	0.51375
105	203.50394	0.47373	0.51338
106	211.08847 218.02330	0.45867	0.51286
107	224.44403	0.44555	0.51224
108	230.44417	0.43394	0.51152
109	236.09163	0.42356	0.51072
110	158.19913	0.63211	0.51182
111 112	173.77277	0.57546	0.51239
112	185.39182	0.53940	0.51262
773			

114	195.15899	0.51267	0.51262
1.5	200 3 4	0.49139	0.51244
116	211.08947	0.47373	0.51211
117	218.02330	0.45867	0.51165
118	224.44403	0.44555	0.51109
119	230.44417	0.43394	0.51044
120	236.09163	0.42356	0.50972
121	158.19913	0.63211	0.51073
122	173.77277	0.57546	0.51126
123	185.39192	0.53940	0.51149
124	195.05899	0.51267	0.51150
125	203.50394	0.49139	0.51134
126	211.08847	0.47373	0.51104
127	218.02330	0.45867	0.51062
128	224.44403	0.44555	0 51012
129	230.44417	0.43394	0.50953
130	236.09163	0.42356	0.50886
131	158.19913	0.63211	0.50981
132	173.77277	0.57546	0.51030
133	185.39182	0.53940	0.51052
134	195.05899	0.51267	0.51054
135	203.50394	0.49139	0.51040
136	211.08847	0.47373	0.51013
137	218.02330	0.45867	0.50975
138	224.44403	0.44555	0.50928
139	230.44417	0.43394	0.50874
140	236. 49163	0.42356	0.50813
141	158.19913	0.63211	0.50901
142	173.77277	0.57546	0.50948
143	185.39182	0.53940	0.50969
144	195.05899	0.51267	0.50971
145	203.50394	0.49139	0.50958
146	211.08847	0.47373	0.50934
147	218.02330	0.45867	0.50899
148	224.44403	0.44555	0.50857
149	230.44417	0.43394	0.50806
150	236.09163	0.42356	0.50750
151	158.19913	0.63211	0.50833
152	173.77277	0.57546	0.50877
153	185.39182	0.53940	0.50897
154	195.05899	0.51267	0.50899
155	203.50394	0.49139	0.50888
156	211.08847	0.47373	0.50865
157	218.02330	0.45867	0.50833
158	224.44403	C • 44555	0.50794
159	230.44417.	0.43394	0.50747
160	236.09163	0.42356	0.50695
161	158.19913	0.63211	0.50772
162	173.77277	0.57546	0.50814
163	185.39182	0.53940	0.50833
164	195.05899	0.51267	0.50836
165	203.50394	0.49139	0.50826
166	211.08847	0.47373	0.50805
167	218.02330	0.45867	0.50775
168	224.44403	0.44555	0.50738
169	230.44417	0.43394	0.50695
170	236.09163	0.42356	0.50646
171	158.19913	0.63211	0.50719
172	173.77277	0.57546	0.50759
173	185.39182	0.53940	0.50777
174	195.05899	0.53540	C. 50780
¥ (**	1230000AA	7.071401	0.50100

175	203.50304	2 (0120	
116		0.49139	0.50771
	210	0.47373	0.50752
177	218.02330	0.45867	0.50724
178	224.44403	0.44555	0.50689
179	230.44417	0.43394	C.50649
180	236.09163	0.42356	0.50602
181	158.19913	0.63211	0.50672
182	173.77277	0.57546	0.50710
183	185.39182.	0.53940	0.50728
134	195.05899	0.51267	
135	203.50394	0.49139	0.50730
186	211.09847	0.47373	0.50722
187	218.02330		0.50704
188	224.44403	0.45867	0.50678
189		0.44555	0.50645
190	230.44417	0.43394	0.50607
	236.09163	0.42356	0.50564
191	158.19913	0.63211	0.50630
192	173.77277	0.57546	0.50666
193	185.39182	0.53940	0.50683
194	195.05899	0.51267	0.50686
195	203.50394	0.49139	0.50678
196	211.08847	0.47373	0.50661
197	218.02330	0.45867	
198	224.44403	0.44555	0.50637
199	230.44417		0.50606
200	230.09163	0.43394	0.50570
	530.03103	0.42356	0.50529

MM 100	м 5 0	\3YS 20000	0.5000	FAILR DOE-03	TIMP 10.0000	CREWS 10	0.8000
	TI 1.0000C		ETR 10.00000	IETR 10			
	TI 1.00000 X 1.0000 X 1.000 0.30	10000004890511529008661794883073658437526965666666666666666666666666666666666	ETR	IETR	ATTPN 0.63: 0.41: 0.35:	(J) 154 596	ATDAN(J) 1.00000 1.19592 1.41062
47 48 49 50	7 0.29 6 0.26 9 0.28 0 0.28	1954 1758 1568 1383	1.58414 1.54928 1.51899 1.49233 2.24135	0.40988 0.40734 0.40485 0.40243 0.40007			
52			2.05328	0.39777			

53	0.27855	1.93643	0.39552
54 55	0.270	35157	0.39332
56	0.27525 0.27366	1.78525 1.73112	0.39117
57	0.27210	1.68563	0.38907 0.38702
53	0.27058	1.64660	0.38501
59	0.26910	1.61258	0.38305
60	0.26765	1.58254	0.38113
61	0.26623 0.26484	2.37434	0.37924
63	0.26343	2.17290 2.04723	0.37740 0.37559
64	0.26214	1.95566	0.37382
65	0.21084	1.88389	0.37208
66	0.25956	1.82515	0.37037
57 58	0.25831 0.25708	1.77567	0.36870
69	0.25587	1.73312 1.69594	0.36706 0.36545
70	0.25469	1.66306	0.36386
71	C.25353	2.49326	0.36231
72	0.25239	2.28006	0.36078
73 74	0.25127	2.14667	0.35928
75	0.25017 0.24910	2.04924 1.97270	0.35781
76	0.24804	1.90995	0.35636 0.35493
77	0.24699	1.85700	0.35353
78	0.24597	1.81138	0.35215
79	0.24496	1.77147	0.35080
80 81	0.24397 0.24300	1.73611 2.60130	0.34946
82	0.24204	2.37754	0.34615 0.34685
83	0.24110	2.23725	0.34558
84	0.24017	2.13458	0.34432
85 86	0.23926	2.05381	0.34309
87	0.23836 0.23747	1.98749 1.93145	0.34187 0.34067
88	0.23660	1.88311	0.33949
89	0.23574	1.84076	0.33832
90	0.23490	1.80320	0.33717
91 92	0.23406	2.70064	0.33604
93	0.23324 0.23243	2.46727 2.32070	0.33492
94	C. 23163	2.21329	0.33382
95	0.23034	2.12869	0.33166
96	0.23007	2.05913	0.33060
97 98	0.22930 0.22854	2.00030	0.32956
99	0.22780	1.94950 1.90496	0.32853 0.32751
.00	0.22706	1.86541	0.32650
101	0.22634	2.79282	0.32551
102	0.22562	2.55060	0.32453
.03 .04	0.22491 0.22421	2.39827	0.32356
.05	0.22352	2.28651 2.19839	0.32261 0.32167
06	0.22284	2.12588	0.32107
. 27	0.22217	2.06449	0.31981
38	0.22151	2.01144	0.31890
09 10	0.22085 0.22020	1.96489	0.31800
11	0.21956	1.92354 2.87901	0.31711 0.31623
12	0.21893	2.62856	0.31537
13	0.21830	2.47089	0.31451

115	114	2.2.70	2.35510	0.31366
116 3.21647 2.18468 0.31199 117 0.21587 2.12473 0.31116 118 0.21528 2.06961 0.31035 119 0.21470 2.02121 0.30075 120 0.21412 1.97818 0.30875 121 0.21355 2.96008 0.30719 123 0.21242 2.53927 0.30642 124 0.21132 2.32531 0.30490 125 0.21132 2.32531 0.30490 126 0.21078 2.24752 0.30268 127 0.21025 2.18158 0.30341 128 0.20972 2.12452 0.30268 129 0.20912 2.07440 0.30196 130 0.20912 2.07440 0.30196 130 0.20913 3.03672 0.30053 132 0.20914 3.03672 0.30053 132 0.20915 2.77134 0.29982 133 0.20714 2.60397 <				
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173 0.19033 2.83399 0.27575				

175	0.18963	2.59134	0.27477
176	0.200	1.50252	0.27428
177	0.18894	2.42763	0.27380
178	0.18859	2.36246	0.27332
179	0.18825	2.30510	0.27285
180	0.18792	2.25401	0.27238
131	0.18758	3.36981	0.27191
182	0.18725	3.07326	0.27144
183	0.18692	2.88573	0.27098
184	0.18659	2.74753	0.27052
185	0.18627	2.63811	0.27007
186	0.18594	2.54774	0.26961
187	0.18562	2.47096	0.26917
188	0.18530	2.40440	0.26872
189	0.18499	2.34580	0.26828
190	0.18467	2.29358	0.26784
191	0.18436	3.42866	0.26740
192	0.18405	3.12663	0.26696
193	0.18374	2.93558	0.26653
194	0.18344	2.79474	0.26611
195	0.18314	2.68320	0.26568
196	0.18283	2.59106	0.26526
197	0.18254	2.51275	0.26484
198	0.18224	2.44485	0.26442
199	0.18194	2.38506	0.26401
200	0.18165	2.33177	0.26359

MM 100	M NSYS 10 10000	FAILR 0.50000E-03	TIMP 10.0000	CREWS 10	0.95000
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IX 123456789012345678901234567890123456789012345678901233456789012444444444444444444444444444444444444	R (IX) 100.0000 R (IX) 100.0000 105.26315 108.46938 110.80330 112.64816 112.76047 114.46570 115.81848 116.97081 117.98412 116.95087 118.22528 119.23178 120.69917 120.42192 121.29456 122.04410 122.71391 120.79845 121.84726 122.65477 123.34509 123.96083 121.79623	T(IX) 1.00000 5.00000 5.00000 6.0.95000 6.95000 6.92192 6.90250 6.86342 6.86349 6.82731 6.83822 6.83041 6.82444 6.81938 6.82731 6.82731 6.82731 6.83822 6.83041 6.82484 6.81938 6.82730 6.81530 6.81657 6.81530 6.81657 6.806671 6.81657 6.80699 6.80491 6.80699 6.80491 6.80699 6.80699 6.79737 6.81371 6.80729 6.80248 6.79845 6.79845 6.79845 6.79845		J 1 2 3 4 5 6 7 8 9 10 11	ATTTP(J) 0.93243 0.86527 0.83991 0.81625 0.81012 0.80602 0.80337 0.80182 0.80112 0.80112
50 51 52	126.13422 123.25824 124.22806	0.79281 0.81130 0.80497	0.83017 (.82980 0.82932		

5.1	124.06202	0.80024	A 92979
			0.82878
54	1.5%	C.79628	0.82817
55	125.13422	0.79281	0.82753
56	123.25824	0.81130	0.82724
57	124.22806	0.80497	0.82685
58	124.96182	0.80024	0.82639
59	125.58318	0.79628	
			0.82588
60	126.13422	0.79281	0.82533
01	123.25824	0.81130	0.82510
62	124.22806	0.80497	0.82477
63	124.96182	0.80024	0.82439
54	125.58318	0.79623	0.82395
05	126.13422		
		0.79281	0.82347
66	123.25824	0.81130	0.82328
67	124.22806	0.80497	0.82301
68	124.96182	0.80024	0.82267
69	125.58318	0.79628	0.82229
70	126.13422	0.79281	0.82187
71	123.25824	0.81130	0.82172
72	124.22806	0.80497	0.82149
73	124.96182	0.80024	0.82120
74	125.58318	0.79628	0.82085
75	126.13422	0.79281	0.82049
76	123.25824		
		0.81130	0.82037
77	124.22806	0.80497	0.82017
78	124.96182	0.80024	0.81991
79	125.58318	0.79629	0.81961
30	126.13422	0.79281	0.81928
81	123.25324	0.81130	C.81918
32	124.22806	0.80497	C.81900
83	124.96182	0.80024	0.81878
84	125.56318	0.79628	0.81851
85	126.13422	0.79281	0.81821
86	123.25824	0.81130	0.81813
87	124.22806	0.80497	0.81798
8.8	124.96182	0.80024	0.81777
39	125.58318	0.79628	0.81753
90	126.13422	0.79281	0.81726
91	123.25824	0.81130	0.81719
92	124.22806	0.80497	0.81706
93			
	124.95132	0.80024	0.81688
94	125.58318	0.79628	0.81666
95	126.13422	0.79281	0.81641
96	123.25824	0.81130	0.81635
97	124.22806	0.80497	0.81624
98	124.96182.	0.80024	0.81607
99	125.58318	0.79628	0.81587
100	126.13422	0.79281	0.81564
101	123.25824	0.81130	0.81560
102	124.22806	0.80497	0.81550
103	124.96182	0.80024	0.81535
104	125.58318	C.79628	0.81516
105	126.13422	0.79281	0.81495
156	123.25824	0.81130	0.81492
107	124.22806	0.80497	0.81482
108	124.96152	0.80024	0.81469
109	125.58318	0.79628	0.81452
110	126.13422	0.79281	0.81432
111	123.25824	0.81130	0.81430
112	124.22806	0.80497	0.81421
113	124.95192	0.30024	0.81409

114 115 116 117 118 119 120 121 123 124 125 127 128 129 130 131 132 133 134 135 136 137 138 139 140 141 142 143 144	125.58318 126.13422 123.25824 124.96182 125.58318 126.13422 123.25824 124.96182 125.58318 126.13422 123.25824 124.96182 124.96182 125.58318 126.13422 123.25824 124.22806 124.96182 125.58318 126.13422 123.25824 124.22806 124.96182 125.58318 126.13422 123.25824 124.22806 124.96182 125.58318 126.13422 123.25824 124.22806 124.96182 125.58318	0.79628 0.79281 0.81130 0.80497 0.9024 0.79628 0.79281 0.80497 0.80497 0.80497 0.80624 0.79628 0.79628 0.79628 0.79628 0.79628 0.79628 0.79628 0.79628 0.79628 0.79628 0.79628 0.79628 0.79628 0.79628 0.79628 0.79628 0.79628 0.79628	0.81393 0.81375 0.81373 0.81354 0.81359 0.81321 0.81321 0.81314 0.81303 0.81274 0.81273 0.81274 0.81257 0.81244 0.81229 0.81228 0.81228 0.81228 0.81214 0.81223 0.81214 0.81202 0.81214 0.81187 0.81187 0.81163 0.81149 0.81149 0.81144 0.81137
147 149 150 151 152 153 154 155 156	124.22806 124.96182 125.58318 126.13422 123.25824 124.22806 124.96182 125.58318 126.13422 123.25824 124.22806	0.81130 0.8C497 0.80024 0.79628 0.79281 0.81130 0.8C497 0.80024 0.79628 0.79231 0.81130 C.80497	0.81114 0.81109 0.81102 0.31092 0.81080 0.81080 0.81076 0.81070 0.81049 0.81049 0.81049
158 159 160 161 162 163 164 165 166 167 168 169 170 171	124.96182 125.59318 126.13422 123.25824 124.22806 124.96182 125.58318 126.13422 123.25824 124.22806 124.96182 125.58318 126.13422 123.25824 124.22806 124.96182	0.80024 0.79628 0.79281 0.81130 0.80497 0.80024 0.79628 0.79281 0.81130 0.80497 0.80024 0.79628 0.79628 0.79628 0.79628 0.81130 0.80497 0.80497 0.80497	0.81039 0.81030 0.81019 0.81020 0.81017 0.81011 0.81002 0.80992 0.80993 C.80990 C.80984 0.80976 0.80966 0.80966
174	125.58318	0.79628	0.80959 C.80951

175	126.13422	0.79281	0.80942
170	1230. 1 4	0.81130	0.80943
177	124.22805	0.80497	0.80940
178	124.96182	0.80024	0.80935
179	125.58318	0.79628	0.80928
180	126.13422	0.79281	0.80919
181	123.25824	0.81130	C.80920
182	124.22805	0.80497	0.80917
183	124.96182	0.80024	0.80913
194	125.58318	0.79628	0.80906
135	126.13422	0.79281	0.80897
185	123.25824	0.81130	0.80898
137	124.22806	0.80497	0.80896
188	124.96182	0.80024	0.80891
139	125.58318	0.79628	0.80885
190	126.13422	0.79281	0.80876
191	123.25824	0.81130	0.80877
192	124.22806	0.30497	0.80875
193	124.96182	0.80024	0.80871
194	125.58318	0.79628	0.80865
195	126.13422	0.79281	0.80856
196	123.25824	0.81130	0.90858
197	124.22806	0.80497	0.80856
198	124.96182	0.80024	0.80852
199	125.58318	0.79628	0.80846
200	126.13422	0.79281	80808

		0.500	FAILR 00E-03	10.0000	CREWS 10	0.9500
1.00	T I 000	ETR 5.00000	IETR 5			
X1234567890123456789012345678901234567890123456789012345678901234567890123456	0.00 1.000 1.000 0.950190 0.950190 0.950190 0.950190 0.9851933 0.851933 0.814519 0.814	ETP	IETR	ATTPNI 0.933 C.856 0.821 0.801 0.791 0.781 0.776	(J) 243 847 751 764 304 154 208 405 708	ATDAN(J) 1.00000 1.00792 1.01499 1.02927 1.03656 1.04396 1.05147 1.05909 1.06683 1.07469
48 49 50 51	0.75091 0.74975 0.74864	1.07033 1.06570 1.06205 1.05899 1.08529	0.80578 0.80561 0.80561 0.80447 0.80336 0.80226			

5.3	7.745	1.07354	0.8C119
		1. Co //1	0.80014
55	0.7433	1.06648	0.79911
			0.79809
56	0.74239	1.09282	
57	0.74142	1.08571	0.79710
58	0.74047	1.08073	0.79612
50	0.73053	1.07674	0.79516
60	0.73861	1.07337	0.79422
61	0.73771	1.09976	0.79329
62	0.73682	1.09249	0.79238
63	0.73595	1.08736	0.79149
64	0.73509	1.08324	0.79061
65	0.73425	1.07975	0.78974
66	0.73342	1.10619	0.78388
67	0.73260	1.09878	0.78804
68	0.73180	1.09353	0.78722
69	0.73101	1.08929	0.78640
70	0.73023	1.08569	0.78560
71	0.72947	1.11219	0.78481
72	0.72871	1.10465	0.78403
73	0.72797	1.09928	0.78326
74	0.72724	1.09495	0.78251
75	0.72051	1.09125	0.78176
76	0.72580	1.11780	0.78102
77	0.72510	1.11015	0.78030
78	0.72441	1.10468	0.77958
79	0.72373	1.10026	0.77887
80	0.72305	1.09647	0.77817
91	0.72239	1.12309	0.77749
82	0.72173	1.11533	0.77681
83	0.72109	1.10978	0.77613
84	0.72045	1.10526	0.77547
85	0.71982	1.10140	0.77482
86	0.71919	1.12807	0.77417
87	0.71856	1.12023	0.77353
88	0.71797	1.11459	0.77290
89	0.71737	1.11000	0.77227
90	0.71678	1.10607	0.77166
91	2.71619	1.13280	0.77105
92	0.71561	1.12487	0.77045
93	0.71504	1.11916	0.76985
94	0.71443	1.11450	0.76926
95	0.71392	1.11050	0.76868
96	0.71336	1.13729	0.76910
97	0.71282	1.12928	0.76753
98	0.71228	1.12350	0.76697
99	0.71174	1.11878	0.76541
100	0.71121	1.11473	0.76586
101	0.71069	1.14158	0.76531
102	0.71017	1.13349	0.76477
103	0.70966	1.12765	0.76424
104	0.70915	1.12287	0.76371
105	0.70855	1.11276	0.76318
106	0.70815	1.14567	0.76266
107	0.70766	1.13751	0.76215
108	0.70717	1.13161	0.76164
109	0.70669	1.12678	0.76113
110	0.70621	1.12262	0.76064
111	0.70574	1.14958	0.76014
112	0.70527	1.14136	0.75965
113	0.70481	1.13541	0.75917
440	J. 10401		0012711

114	0.704	1.13053	0.75868
1 : 1	19 64	1,12531	0.75821
116	0.70344	1.15333	0.75774
117	C.70300	1.14506	0.75727
118	0.70255	1.13905	0.75680
119	0.70212	1.13412	0.75634
120	0.70163	1.12937	0.75589
121	0.70125	1.15694	0.75544
			0.75499
122	0.70092	1.14861	
123	0.70040	1.14255	0.75455
124	0.69999	1.13758	0.75411
125	0.69955	1.13329	0.75367
126	0.69915	1.16041	0.75324
127	0.69374	1.15203	0.75281
128	0.69834	1.14593	0.75238
129	0.69794	1.14091	0.75196
130	0.69754	1.13658	0.75154
131	0.69714	1.16376	0.75113
132	0.69675	1.15532	0.75071
133	0.69030	1.14918	0.75030
134	0.69597	1.14413	0.74990
135	0.69559	1.13976	0.74950
136	0.69521	1.16699	0.74910
137	0.69493	1.15851	0.74870
138	0.69445	1.15232	0.74831
139	0.59409	1.14724	0.74792
140	0.69372	1.14283	0.74753
141	0.69336	1.17011	0.74715
142	0.69299	1.16158	0.74677
143	0.69253	1.15536	0.74639
	0.69228	1.15024	0.74601
144			
145	0.69192	1.14580	0.74564
145	0.69157	1.17313	0.74527
147	0.69122	1.16456	0.74490
145	0.69037	1.15831	0.74453
149	0.69053	1.15315	0.74417
150	0.69019	1.14868	0.74381
			0.74345
151	0.68985	1.17606	
152	0.68951	1.16745	0.74310
153	0.65918	1.16116	0.74275
154	0.68385	1.15597	0.74240
155	C.68852	1.15147	0.74205
156	0.68819	1.17890	0.74170
157	0.68786	1.17025	0.74136
158	0.68754	1.16392	0.74102
150	0.68722	1.15870	0.74968
160	0.58690	1.15418	0.74035
161	0.68658	1.18165	0.74001
162	0.68627	1.17297	0.73968
163	0.58595	1.16661	0.73935
164		1.16136	0.73902
	0.68555		
165	0.68534	1.15681	0.73870
166	0.68503	1.18433	0.73837
167	0.69473	1.17561	0.73805
168	0.68443	1.15922	0.73773
100	0.68412	1.16395	0.73742
170	0.68383	1.15937	0.73710
171		1.18693	0.73679
	0.68353		
172	0.68323	1.17818	0.73648
173	0.63294	1.17176	0.73617
174	0.68265	1.16646	0.73586

175	0.68235	1.16186	0.73555
176	0.502.	1.18947	0.73525
177	0.68179	1.18068	0.73495
178	0.68150	1.17423	0.73465
179	0.68122	1.16891	
130	0.68094		0.73435
181	2.68066	1.16428	0.73405
182		1.19194	0.73376
	0.68038	1.18311	0.73346
183	0.68011	1.17664	0.73317
184	0.67983	1.17129	0.73288
185	0.67956	1.16665	0.73259
186	0.67929	1.19434	0.73231
187	3.67902	1.18549	0.73202
188	0.67875	1.17899	0.73174
189	0.67849	1.17362	0.73146
190	0.67822	1.16895	0.73118
191	0.67796	1.19669	0.73090
192	0.67710	1.18781	0.73062
193	0.67743	1.18129	0.73035
194	0.67718	1.17589	0.73007
195	0.67692	1.17120	0.72980
196	0.67666	1.19898	
197	0.67641	1.19007	0.72953
198	0.67615		0.72926
199		1.18352	0.72899
	0.67590	1.17811	0.72872
200	0.67565	1.17340	0.72846

						AIU.
MM 100	м 20	45.75 1.0000	FAIL 0.50000E0		CREWS	A/4./
100						007,5000
1	1.000	TI 00 !	ETR LE 5.00000	TR 5		
IX		R(IX)	T(1X)	AVGT(IX)	_	ATTTP(J)
1 2 3 4		100.30000	1.00000 G.95000	1.00000 0.97500	1 2	0.93243 0.87220
3		108.46938	0.92192	0.95731	3	0.85271
4		110.80330	0.90250	0.94360	4	0.84414
5 5		112.64816	0.88772 0.89813	0.93243 0.92671	5 6	0.84090 0.84090
7		113.44319	0.88150	0.92025		
8		115.00192	0.86955	0.91391		
10		116.28554	0.85995 0.85185	0.90792 0.90231		
11		114.48541	0.87347	0.89769		
12		116.26293	0.86012	0.89639		
13 14		117.56190 118.63181	0.85062 0.84294	0.89287 C.38930		
15		119.55829	0.83641	0.38578		
16		115.82841	0.86335	0.88438		
17		117.51811	0.85093	0.88241 0.88017		
19		118.74062	0.84217 0.83512	0.87780		
20		120.60992	0.82912	0.87537		
21		116.32755	0.85964	0.87462		
22 23		117.99321	0.84751 0.83897	C.87339 O.87189		
24		120.17685	0.83211	C.87023		
25		121.02557	0.82627	0.36847		
26 27		116.32755	0.85964 0.84751	0.86813 0.86737		
29		119.19402	0.83897	0.86635		
29		120.17685	0.83211	0.86517		
30 31		121.02557 116.32755	0.826 27 0.85964	0.86388 0.86374		
32		117.99321	0.84751	0.86323		
3 3		119.19402	0.83897	0.86250		
34		120.17685 121.02557	0.83211	0.86160 0.86059		
35 36		116.32755	0.82627 0.85964	0.36057		
37		117.99321	0.84751	0.86021		
36		119.19402	0.83897	0.85965		
39 40		120.17685	0.83211 0.82627	0.858 95 0.85813		
41		116.32755	0.85964	0.85817		
42		117.99321	0.84751	0.85791		
43 44		119.19402	0.83897 0.83211	0.85747 0.85639		
45		121.02557	0.82627	0.85621		
46		116.32755	0.85964	0.85629		
47 48		117.99321	0.84751 0.83897	0.8561C 0.85574		
49		120.17685	0.83211	0.85526		
50		121.02557	0.82627	0.85468		
51		116.32755	0.85964 0.84751	0.85478 0.85464		
52		117.99321	U • 84 / 91	U . 0 2 4 0 4		

ii 2	110 10/02	0 1200	0.5131
53 54	119.19472	0.83897 0.83211	0.85434 0.85393
55	121.02547	0.82627	0.85343
56	116.32755	0.85964	0.85354
57	117.99321	C.84751	0.85343
5 S	119.19402	0.83897	0.85318
59 60	120.17685 121.02557	0.83211 0.82627	0.85283 0.85238
61	116.32755	0.85964	0.85250
62	117.99321	0.84751	0.85242
63	119.19402	0.83897	0.85221
64 05	120.17685	0.83211	0.85189
66	121.02557 116.32 7 55	0.82527 0.85964	0.85150 0.85162
67	117.99321	0.84751	0.85156
68	119.19402	0.83897	0.85138
69	120.17685	9.83211	0.85110
70 71	121.02557	0.92627	0.85074
72	116.32755 117.99321	0.85964 0.84751	0.85087 0.85082
73	119.19402	0.83897	0.85066
74	120.17685	0.83211	0.95041
75	121.02557	0.82627	0.85008
76 7 7	116.32755	0.85954	0.85021
78	117.99321 119.19402	0.84751 0.83897	0.85017 0.85003
79	120.17685	0.33211	0.84980
80	121.02557	0.82627	0.84951
31	116.32755	0.85964	0.84963
82 83	117.99321	0.84751	0.84961
33	119.19402 120.17685	0.83897 0.83211	0.84948 0.84927
35	121.02557	0.82627	0.84900
86	116.32755	0.85964	0.84913
67	117.99321	0.84751	0.84911
88 8 9	119.19402 120.17685	0.83897	0.84899
90	121.02557	0.83211 0.82627	0.8489C 0.84855
91	116.32755	0.85964	0.84867
92	117.99321	0.84751	0.84866
93	119.19402	C.83897	0.84856
94 95	120.17685 121.02557	0.83211 0.82627	0.84838 0.84815
95	116.32755	0.85964	0.84827
97	117.99321	0.84751	0.84826
98	119.19402	0.83897	C.84817
99	120.17685	0.83211	0.84800
100 101	121.02557 116.32755	0.82627 0.85964	0.84779 0.84790
102	117.99321	0.84751	0.84790
103	119.19402	0.83897	0.84781
104	120.17685	0.83211	0.84766
105	121.02557	0.32627	0.84746
106 107	115.32755 117.99321	0.85964 0.84751	0.84757 0.84757
105	119.19402	0.83897	0.84749
109	120.17685	0.83211	0.84735
110	121.02557	0.82627	0.84716
111 112	116.32755 117.99321	0.85964 0.54751	0.84727 0.84727
113	119.19402	0.83897	0.84727
-			

1:4	120. 7635	0.83211 0.42627	0.84707 0.84689
115	1.6.52.05	0.55964	0.84700
117	111.99321	0.84751	0.84700
116	119.19402	0.83897 0.83211	0.8469 3 0.8468 1
119 120	120.17665 121.02557	0.82627	0.84664
121	116.32755	0.85964	0.84674
122	117.99321	0.84751	0.84675
123	119.19402	0.83897	0.8466 9 0.8465 7
124 125	120 .176 85 121 . 32557	0.82627	0.84641
125	110.32755	0.85954	0.84651
127	117.99321	0.84751	0.84652
128	119-19402	0.83897 0.83211	0.846 46 0.84635
129 130	120.17635	0.82627	0.84619
131	116.32755	0.85964	0.94530
132	117.99321	0.84751	0.84631
133	119.19402	0.83397 6.43211	0.84625 0.84615
134 135	120.17663 121.02557	0.82527	0.34500
136	116.32755	6,45964	0.86010
137	117.99321	0.84751	0.84611
138	119.10402	0.83897	1.84606 3.84596
139 140	120 • 1 7685 121 • 02557	0.82627	0.24582
141	116.32755	0.85964	0.84571
142	117.99321	0.84751	0.84552 0.84588
143 144	119.17402 120-17585	0.8389 7 0.83211	0.84578
144	121.02557	0.82527	0.84565
146	115,32755	0.85964	0.845/4
147	117.49321	0.84751	0.94575 0.84571
148 149	119.19402 120.17635	0.83211	0.84552
150	121.02557	0.82627	0.84549
151	116.32755	0.85964	0.84558 0.84559
152 153	117.99321 119.19402	0.84751 0.83897	0.84555
154	120.17685	0.83211	0.84546
155	121.02557	0.82627	0.84534
156	116.32755	0.85964 0.84751	0.84543
157 158	117.99321 119.19402	0.83667	0.84540
159	120.17685	0.83211	0.84532
160	121.02557	0.82627	0.84520 0.84529
161	116.32755 117.99321	0.85°64 0.84751	0.84530
162 163	119.1940?	0.83997	0.84526
164	120.17685	0.83211	0.84518
165	121.02557	0.82627 0.85964	0.84507 0.84516
166 167	116.32755 117.99321	0.84751	0.84517
168	119.19402	C.83897	0.84513
169	120.17085	0.83211	0.84505
170	121.02557	0.82827	0.84495
171 172	116.32755 117.99321	0.84751	0.84505
173	119.19402	0.83897	0.84501
174	120.17685	0.83211	0.84494

1/5	121,02857	0.82627	0.84483
(-		0.85964	0.84491
177	117.95 21	0.84751	0.84493
178	119.19402	0.83897	0.84490
179	120.17685	0.83211	0.84482
180	121.02557	0.82627	0.84472
131	116.32755	0.85964	0.84480
182	117.99321	0.84751	0.84482
183	119.19402	0.83897	0.84479
184	120.17685	0.83211	0.84472
185	121.02557	0.82627	0.84462
136	116.32755	0.85964	0.84470
187	117.99321	0.84751	0.84471
188	119.19402	0.83897	0.84468
139	120.17685	0.83211	0.84462
190	121.02557	0.82627	0.84452
191	116.32755	0.85964	0.84460
192	117.99321	0.84751	0.84461
193	119.19402	0.33897	0.84458
194	120.17685	0.83211	0.84452
195	121.02557	0.82627	0.84443
196	116.32755	0.85964	0.84450
197	117.99321	0.84751	0.84452
198	119.19402	0.83897	0.84449
199	120.17685	0.83211	0.84443
200	121.02557	0.82627	0.84434

		N=Y5 10000		FAILR OCE-03	TIMP 10.0000	CREWS 10	0.95000
1.0	T1 00000		6 TR 5.00000	IETR 5			
1.0 1.23456769C123456769C123456769C123456769C123456789C123456789C123456789C12322222333333344444444445555	1.0052088784888888888888888888888888888888888	00127557937272756417642355777777566666555555544690622777265666555555544449062277727566665555555444490622777275666655555555444490662277727566665555555555555555555555555	5.00000 TOTN(10000 1.00000 1.00000 1.00000 1.00000 1.00000 1.00000 1.002547 1.01420 1.01427 1.01427 1.01427 1.02474 1.02474 1.025494 1.025494 1.03843 1.03843 1.03843 1.03843 1.03843 1.03843 1.04853 1.05807 1.069527 1.069528 1.08672 1.08675 1.08675 1.08672 1.08675 1.08672	A VGTN (IX) 1.00000 0.97500 0.97500 0.97500 0.93243 0.93243 0.92299 0.91484 0.90765 0.90124 0.89545 0.89517 0.89533 0.82780 0.86573	7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	243 847 751 764 304	ATDAN(J) 1.00000 1.01599 1.03045 1.04519 1.06034 1.07594

ラ ラ	0.7454		0.80119
55 56	3.1433		0.800 4 0.79911
57 58	0.74142	1.14308	0.79809 0.79710
59 60	0.73953	1.12518	0.79612 0.79516
51	0.73771	1.16529	0.79422
53 54	0.73595	1.13998	0.79238 0.79149
55 56	0.73425 0.73342	1.12533	0.79051 0.78974 0.78888
57 58	0.73260	1.15684	0.78804 0.73722
69 70	0.73101	1.13830	0.78640 0.78560
71 72	0.72947 0.72871	1.17845	0.78481 0.78403
73 74 75	0.72797	1.14420	0.78326 0.78251
76 77	0.72551 0.72550 0.72510	1.13731	0.78176 0.78102
73 79	9.72441 9.72373	1.16861	0.78030 0.77958
30 81	0.72305 0.72239	1.14975 1.14275 1.19000	0.77887 0.77817
82 93	0.72173	1.17426 1.16348	0.77749 0.77681 0.77613
84 85	0.72045 0.71982	1.15499	0.77547 0.77482
85 87	0.71919 0.71858	1.19528	0.77417 0.77353
38 89 90	0.71797	1.16853 1.15994	0.77290
91 92	0.71676 0.71619	1.15276	0.77166 0.77105
93 94	0.71561 0.71504 0.71446	1.18431	0.77045 0.76985
95 96	0.71392	1.16464 1.15738 1.20505	0.76926 0.76988
97 98	0.71282 0.71225	1.18895 1.17787	0.76710 0.76753 0.76697
99 100	0.71174 0.71221	1.16911 1.16178	0.76641 0.76586
101 102 103	0.71009 0.71017	1.20959 1.19338	0.76531 0.76477
104 105	0.70965 0.70915 0.70865	1.18221	0.76424
196 197	0.70315 0.70766	1.16598 1.21392 1.19762	0.76318 0.76266
108 109	0.70717 0.70669	1.19762 1.18637 1.17747	0.76215 0.76164 0.76113
110 111	0.70521 0.70574	1.17000	0.76064
112	0.70527	1.19000	0.7.905

114	0.70.	1.10138	0.75868
1.5		1 1400	0.75821
110	C	1.22205	0.75774
117	0. 1000	1,20556	0.75727
118	0.70259		0.75680
119	3.70218		0.75634
120	0.70138		0.75589
121	0.70125		0.75544
122	0.70052	4 4 7 27 1,	0.75499
123	0.70040		0.75455
125	0.69998		0.75411
126	0.69956 0.69915		0.75367
127	0.59874	1.22955	0.75324
128	0.69834	1.21290	0.75281
129	0.67794	1.20138 1.19224	0.75238
130	0.69754	1.18456	0.75196
131	0.69714	1.23310	0.75154
132	0.69675	1.21637	0.75113 0.75071
133	0.69636	1.20479	0.75030
134	0.59597	1-19560	0.74990
135	0.59559	1.18787	0.74990
136	0.09521	1.23652	0.74910
137	0.69433	1.21972	0.74870
138	0.65446	1.20809	0.74831
139	0.69409	1.19885	0.74792
140	0.69372	1.19107	0.14753
141 142	0.69336	1.23983	0.74715
143	0.69299	1.22309	0.74677
144	0.59263	1.21127	0.74639
145	0.69228 0.69192	1.20198	0.74501
146	0.69197	1.19417	0.74564
147	0.69122	1.24303	0.74527
148	0.59087	1.22610 1.21436	0.74490
149	0.69053	1.20502	0.74453
150	0.69019	1.19717	0.74417 0.74361
151	0.68995	1.24613	0.74345
152	0.0895;	1.22914	0.74310
153	0.58918	1.21735	0.74275
154	0.58835	1.20797	0.74240
155	0.65852	1.20008	0.74205
156	0.68819	1.24914	0.74170
157	0.08786	1.23208	C.74136
158	0.69754	1.22025	0.74102
159 160	0.68722	1.21083	0.74068
161	0.68690	1.20290	0.74035
162	0.62636 0.68627	1.25206	0.74001
163	0.68595	1.23495	0.73968
164	0.68565	1.22306 1.21351	0.73935
165	0.68534	1.20564	0.73902
166	0.65503	1.25489	0.73870
167	0.68473	1.23773	0.73837 0.73805
168	0.68443	1.22580	0.73773
169	0.68412	1.21631	0.73742
170	0.68383	1.20831	0.73710
171	0.68353	1.25765	0.73679
172	9.68323	1.24043	0.73648
173	0.68294	1.22846	0.73617
174	0.68205	1.21894	0.73586

170			
175	0 6853	1.21090	0.73555
A (11 4 2 2 2	1.20034	0.73525
177	C. 65175	1.24367	0.73495
178	0-64100	1.23106	0.73465
179	0.68122	1.22149	
180	0.6809.	1.21343	0.73435
181	0.68055	1.26295	0.73405
132	0.58039	1.24563	0.73376
193	0.58011		0.73346
184	0.67983	1.23358	0.73317
185	0.67956	1.22399	0.73288
1 36	0.67929	1.21589	0.73259
187	0.67902	1.26550	0.73231
133	_	1.24813	0.73202
189	0.67875	1.23604	0.73174
190	0.67849	1.22642	0.73146
	0.67822	1.21829	0.73118
191	0.67796	1.26799	0.73090
192	0.67770	1.25057	0.73062
193	0.67743	1.23945	0.73035
194	C. 57713	1.22879	0.73007
195	0.67692	1.22064	0.72980
196	0.67666	1.27041	0.72953
197	0.67641	1.25295	0.72926
198	0.67615	1.24079	
199	0.67590	1.23111	0.72899
200	0.67565		0.72872
_	-40,707	1.22293	0.72846

MM 15 . . 1 1 TIMP CREWS FAILR 100 20 0.95000 10300 0. 500006-03 10.0000 10 TR 1515 1.00000 . 00000 ΙX P ([X] T(1x) AVGT(IX) ;; ATTTP(J) 1 100.00000 1.00000 0.93243 1.00000 1 2 105.26315 0.95000 0.97500 2 0.89373 3 0.95731 109.46938 0.92132 0.89373 4 110.3330 0.90250 0.94360 ÷, 112,54316 0.88772 0.93243 6 107.03914 0.93380 0.93266 7 110.37557 0.906.00 0.92885 8 112.55222 0.88848 0.92380 C 114.22971 C, 8754? 0.91843 10 115.61258 0.86490 0.41308 11 107.08914 0.93370 0.91496 12 110,37567 0.90500 0.91422 112.55222 1.3 0.38349 0.91224 14 114,722671 6.57-43 0.90961 15 115.01258 0,86495 0. 90663 16 107.08914 0.93380 0.90833 17 110.37557 0.90600 0.90819 15 112.55222 C. 28348 0.90710 19 114,22071 0.87543 0.90543 115.61253 20 0.86496 0.90340 21 107.05914 0.93380 0.90485 22 110.37507 0.90600 0.90490 23 112,55222 0.88848 0,90419 24 114.22971 0.87543 0.90299 25 115.61258 0.90147 0.86496 26 107.08914 0.93380 0.90271 27 110.37567 0.90600 0.90283 28 112.55222 C.88848 0.90232 20 114.22971 0.87543 0.90139 30 115,61258 0.85496 0.90018 31 107.09914 0.93380 0.90126 32 110.37567 0.90600 0.90141 33 0.90102 112.55222 0.88848 114.22971 34 0.87543 0.90027 35 115.01258 0,96496 0,80026 36 107.08914 0.93380 0.90022 37 110,37567 0.90600 0.90037 38 112.55222 C. 89948 0.90006 39 114,22971 0.87543 0.89943 40 115.01258 C.86496 0.89857 41 107.09914 0.93380 0.89942 42 110.37567 0.89958 0.90600 43 112.55222 0.88848 0.89932 44 114.22971 0.87543 0.89873 45 115.61253 0.85496 0.59803 45 107.05914 0.93380 0.89331 47 110.37567 0.90600 0.89896 48 112.55222 0.89874 C.88848 49 114.229471 0.87543 0.89825 50 115.61258 0.86496 0.89760 51 107.08914 0.93380 6.89831

52

110.37567

0.90600

0.89845

23	112.0002	0.88848	0.89827
5		7543	0.89784
55		0.80496	0.89725
55	107.38914	0.92380	0.39790
57	110.37567	0.90600	0.89804
58	112.55222	0.88348	0.89788
50	114.22971	0.87543	0.89749
00	115.61258	0.86496	0.89695
			0.89756
o i	107.09914	0.93380	
52	110.37567	0.90600	0.89769
63	112.55222	0.38848	0.89755
54	114.22971	0.87543	0.89720
05	115.61258	0.86496	0.89670
0.0	107.08914	0.93380	0.89727
57	110.37557	0.90000	C.89740
68	112.5522?	0.88348	0.89726
69	114.22971	0.87543	0.89695
7 C	115.612.8	0.86490	0.89649
71	107.08914	0.93390	0.89702
72	110.37567	0.99600	0.89714
73	112.55222	0,33849	0.89702
74	114.22971	0.87543	0.30573
75	115.51258		
		0.05496	0.89631
76	107.08914	0.93380	0.89680
77	110.37567	0.90600	0.89692
78	112.55222	0.88348	0.89681
79	114.22971	0.87543	0.89654
90	115.61258	0.86496	0.89615
81	107.08914	0.93380	0.89661
92	110.37567		0.89672
		0.90600	
53	112.55222	0.88849	0.39663
34	114,22971	0.87543	0.39537
35	115.61258	0.86496	0.89600
86	107.08914	0.93380	0.89644
97	110.37557	0.90500	0.89655
88	112.55222	0.88848	0.89646
89	114.22971	0.87543	0.89622
9Ü	115.61258	0.86496	0.99588
91	107.08914	0.93380	0.89629
92	110.37567	0.90600	0.89640
93	112.55222	0.32848	0.89631
94	114.22971	C.87543	0.89609
95	115.61258	0.26496	0.89576
96	107.08914	0.93380	0.89516
97			0.39626
	110.37567	0.90600	-
98	112.55222	0.88848	0.89618
99	114.22971	0.87543	0.89597
100	115.61258	0.86496	C.89566
101	107.38914	0.93380	0.99604
102	110.37567	0.90660	0.89614
103	112.55222	0.88848	0.89606
104	114.22971	0.87543	0.89586
105		0.86496	0.89557
	115.61258		
106	107.08914	0.93380	0.89593
107	110.37567	0.90600	0.89602
108	112.55222	0.88843	0.89595
109	114.22971	0.87543	0.89577
110	115.61258	0.86496	0.89549
111	107.08914	0.93380	0.89583
112	110.37567	0.90600	0.89592
113			0.89586
110	112.55222	0.88848	0.09200

114	11/2 11.72	0 026/2	6 00510
115		0.87543	0.89568
115		v 4 9 b	0.81
	107. 1. 1. 1.	3.93330	0.89574
117	110. 7500	9. CD (O O	0.89583
118	112455222	0. 19064	0.89577
119	1.4.229/1	C. 9/543	0.89559
120	115.61259	0.56496	0.89534
121	107.08914	0.93380	
122	110.37567		0.89566
123		0.90600	0.89574
	112.55?22	0.88848	0.89568
124	114.22971	0.87543	0.89552
125	115.61253	0.36496	0.89527
126	107.08514	9.93380	0.89558
127	110.37567	C- 90600	0.89566
128	112.55222	0.88848	0.89561
120	114.22971	0.87543	0.99545
130	115.41258		
131		0.86496	0.89521
132	107.08014	0.43380	0.89551
	110.37567	0.40600	0.89559
133	112.5522	0.88849	0.89554
134	114.22971	0.87543	0.89539
135	115.01258	C. 80495	0.89516
136	107.0391-	0.53380	0.89544
137	110.37567	0.90600	0.89552
138	112.55222		
139		0.88848	0.89547
	114.22971	C. 97543	0.39533
140	115.01254	0.85496	0.09511
1+1	107.09514	0.93380	0.89538
142	110.37567	0.90500	0.89546
143	112.55222	0.83848	0.89541
144	114.22971	0.97543	0.89527
145	115.61258	0.86496	0.39505
145	107.08914	0.93380	
1 - 7	110.37:67		0.89533
143		0.90600	0.89540
	112.55222	0.88848	0.89535
:40	114.22971	0.87543	0.89522
150	115.61258	0.55496	0.89502
151	107.08914	0.93380	0.89527
152	116,37567	0.90600	0.89534
153	112.55222	0.38848	0.89530
154	114.22971	C. 87543	0.89517
155	115.61258	0.86496	0.89477
156	107,05514		
157		0.93380	0.89522
	110.37567	0.30400	0.89529
158	112.55222	0.88348	0.39525
159	114.22971	C.87543	0.89512
150	115.61259	C. P6495	0.89494
151	107.00914	1. 423 BD	0.39518
152	110.37567	0.90600	0.89524
163	112.55222	0.88848	0.89520
1.64	114.22971	0.87543	
165	115.61258		0.89508
		0.86495	0.89490
165	107.08914	0,93380	0.89513
167	110.37567	0.57600	0.89520
168	112.55222	0.88848	0.89516
159	114.22971	0.87543	0.89504
170	115.51258	0.86495	0.89486
171	107.08914	0.93390	0.89509
172	110.57567	0.90600	0.89516
1/3	112.55222	C. Re848	
1/3 174	114.22971		0.89512
. / -	114066711	C.37543	0.89500

175	115,51258	0.86496	0.89483
		0. 93380	0.8950
177	1107507	0.90600	0.89511
178	112.55222	0.88848	0.89508
179	114.22971	7.47543	0.89497
130	115.61258	0.86496	0.89480
181	107.08914	0.93380	0.89502
182	110.37567	0.90600	0.89508
133	112.55222	0.88843	0.89504
154	114.22971	0.87543	0.89493
135	115.61258	0.86496	0.89477
186	107.08914	0.93380	0.89498
167	110.37567	0.90600	0.89504
188	112.55222	0.88848	0.89501
189	114.22971	0.87543	0.89490
190	115.51258	0.86496	0.39474
191	107.08914	0.93380	0.89495
192	110.37567	0.90600	0.89501
193	112.55222	C.88848	0.89497
194	114.22971	0.87543	0.89487
195	115.01258	0.86496	0.89472
196	107.08914	0.93380	0.89492
197	110.37567	0.90600	0.89497
198	112.55222	0.88848	0.89494
199	114.22971	0.87543	0.89484
200	115.61258	0.86496	0.89469

T:		M NS 1 0 0000	(5 00 0.5000	FAILR POE-03	TIMP CRE 10.0000		
1 1.00000 1.00000 1.00000 C.93243 1.00000 2 0.95000 1.00000 0.97500 C.85847 1.04107 3 C.92192 1.00000 0.95731 0.82751 1.08002 4 0.90250 1.00000 0.93243 5 0.88772 1.00000 0.93243 6 0.87582 1.06620 0.92299 7 0.86589 1.04652 0.91484 8 0.85738 1.03627 0.90765 9 C.84493 1.02999 0.90124 10 0.84333 1.02564 0.89545 11 0.83741 1.11511 0.89017 12 0.83203 1.08900 0.88533 13 0.82712 1.07418 0.89085 14 0.82259 1.06423 0.87669 15 0.91841 1.05688 0.87280 16 0.81451 1.1733 0.86573 16 0.80744 1.10036 0.86916 17 0.81086 1.11733 0.86573 18 0.80744 1.0036 0.86249 19 0.80421 1.08855 0.85942 20 0.80117 1.0752 0.85651 21 0.79828 1.16977 0.85374 22 0.79554 1.13885 0.85109 23 0.79292 1.12051 0.84856 24 0.79043 1.10753 0.84614 25 0.78357 1.15624 0.83943 28 0.78147 1.23694 0.83736	1.0						
30 0.77749 1.11251 0.83344 31 0.77560 1.20397 0.83157 32 0.77378 1.17087 0.82976 33 0.77202 1.15084 0.82801 34 0.77032 1.13645 0.82632 35 0.76867 1.12527 0.62467 36 0.76707 1.21737 0.82307 37 0.76851 1.18352 0.82151 38 0.76400 1.16292 0.82000 39 0.75254 1.14805 0.81853 40 0.76111 1.13644 0.81709 41 0.75972 1.22914 0.81569 42 0.75637 1.19467 0.81433 43 0.75705 1.17361 0.81299 44 0.75576 1.15834 0.81169 45 0.75450 1.14639 0.81042 46 0.75328 1.23965 0.80918 47 0.75203 1.20465 0.80918 47 0.75091 1.18320 0.80678 49 0.74976 1.16761 0.80561	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	COCC TN(100002 (100000 (100000 (100000 (100000 (100000 (10	5.00000 TDTN(1X) 1.00000 1.00000 1.00000 1.00000 1.00000 1.006620 1.02999 1.02564 1.1511 1.08898 1.07418 1.06423 1.07962 1.168855 1.07962 1.18895 1.12315 1.12315 1.12317 1.18894 1.12315 1.12317 1.18984	5 AVGTN(IX) 1.00000 0.97500 0.97500 0.95731 0.94360 0.93249 0.912484 0.91245 0.89517 0.89517 0.89533 0.87667 0.86573	C.93243 C.85847	1.00060 1.04107	

	2 7 7 7 7 7 7		0.00110
53	0.74547	1.19191	0.80119
5'		1.7003	0.80014
55	3.16355	1.16354	0.79911
56	0.74239	1.25793	0.79809
57	0.74142	1.22197	0.79710
58	0.74047		
		1.19989	0.79612
50	0.73953	1.18376	0.79516
6C	0.73361	1.17106	0.79422
01	0.73771	1.26581	0.79329
62	0.73682	1.22960	0.79238
63	0.73595	1.20725	0.79149
	0.73509		
64		1.19091	0.79061
65	0.73425	1.17802	0.78974
66	0.73342	1.27321	0.78888
67	0.73260	1.23568	0.78804
68	0.73180	1.21409	0.78722
69	0.73101	1.19756	0.78640
70	0.73025	1.18449	0.78560
7:	0.72947	1.28011	0.78481
72	0.72871	1.24328	0.75403
73	0.72747	1.22049	0.78326
74	0.72724	1.20377	0.78251
75	0.72631	1.19956	0.78176
		1.28058	0.78102
76	0.72530		
77	0.72510	1.24948	0.78030
75	0.72441	1.22648	0.77958
			0.77887
79	0.72373	1.20961	
80	0.72305	1.19026	0.77817
31	0.72239	1.29256	0.77749
32		1.25531	9.77681
	0.72173		
33	0.72109	1.23214	0.77613
84	0.72045	1.21512	C.77547
35	0.71982	1.20164	0.77482
30	0.71919	1.29340	0.77417
87	0.71853	1.26782	0.77353
38	0.71797	1.23748	0.77290
59	0.71737	1.22033	0.77227
90	0.71678	1.20673	0.77166
91	0.71619	1.30384	0.77105
92	0.71561	1.26604	0.77045
93	0.71504	1.24255	0.76985
94	0.71443	1.22527	0.76926
95	0.71392	1.21157	0.76869
96	0.71330	1.30901	0.76810
97	0.71232	1.27101	0.76753
98	0.71228	1.24738	0.76697
99	0.71174	1.22998	0.76641
190	0.71121	1.21617	0.76586
101	0.71069	1.31394	0.76531
102	0.71017	1.27575	0.76477
113	0.70965	1.25198	0.76424
104	0.70915	1.23448	0.76371
105	0.70855	1.22057	0.76318
106	0.70815	1.31865	0.76266
137	0.70755	1.28027	0.76215
108	0.70717	1.25538	0.76164
109	0.70669	1.23877	0.76113
	0.70621	1.22478	0.76064
110			
111	0.70574	1.32315	0.76014
112	0.70527	1.23461	0.75965
	0.70481	1.26059	0.75917
113	0.10981	1.20034	0.12911

	10.	1 2/200	0 750/0
11.	104	1.24289	0.75868
115	1.1000	. 22852	0.75821
116	0.70344	1.32747	0.75774
117	0.70300	1.28876	0.75727
118	C. 70255	1.25464	0.75680
119	0.70212	1.24684	0.75634
120	0.70108	1.23209	0.75589
121	0.70125	1.33162	0.75544
122	0.70082	1,29276	0.75499
123	0.70040	1.26853	0.75455
124	0.69998	1.25065	0.75411
125	0.69956	1.23642	0.75367
126	0.59915	1.33562	0.75324
127	0.69874	1.29661	0.75281
128	0.69834	1.27227	0.75238
129	0.69794	1.25431	0.75196
130	0.69754	1.24002	0.75154
131	0.69714	1. 23947	0.75113
132	0.09575	1.30032	0.75071
133	0.09636	1.27589	0.75030
134	0.69597	1.25785	0.74990
135	0.59559	1.24348	0.74950
156	0.69321	1.34319	0.74919
137	0.69453	1.30390	0.74870
138	0.69446	1.27938	0.74831
130	0.69409	1.24126	0.74792
140	0.69372	1.24584	0.74753
141	0.69330	1.34678	0.74715
142	0.69299	1.717.7	0.74677
143	0.69253	1.28275	0.74539
144	0.69328	1.25456	0.74601
145	2.69192	1.25008	0.74564
146	0.69157	1.35026	0.74527
147	0.69122	1.31072	0.74490
			-
1.48	0.69087	1.28602	0.74453
49	0.19055	1.26776	0.74417
150	0.69019	1.25322	0.74381
_			
151	0.58935	1.75363	0.74345
152	0.68951	1.31397	0.74310
153	0.68913	1.23918	0.74275
154	C.68385	1.27086	0.74240
155	0.68352	1.25626	0.74205
156	0.68819	1.35690	C.74170
157	0.68733	1.31712	0.74136
158	0.68754	1.29225	0.74102
159	0.68722	1.2738 7	0.74068
150	3.50090	1.25922	0.74035
151	0.50450	1.36007	0.74001
152	0.68627	1.32018	0.73968
153	0.48595	1.29524	0.73935
164	0.68565	1.27679	0.73902
165	1.68534	1.26209	0.73870
150	0.68503	1.36315	0.73837
167	0.65473	1.32315	0.73805
		1.29813	0.73773
155	0.68443		
169	0.68412	1.27963	0.73742
170	0.68333	1.26498	0.73710
171	0.68353	1.36615	0.73679
172	0.68323	1.32604	0.73648
173	0.68294	1.30096	0.73617
174	0.58265	1.28240	0.73586

175	0.60534	1.26760	0.73555
1 20	7 4 1 2 4	36905	0.73525
177	0.58111	1.32886	0.73495
178	C.68150	1.30370	0.73465
179	0.68122	1.28509	0.73435
180	0.68094	1.27024	0.73405
181	0.58065	1.37190	0.73376
182	0.68038	1.33160	0.73346
193	0.63011	1.30638	0.73317
184	0.67985	1.28771	C.73288
185	0.57956	1.27282	0.73259
135	0.67929	1.37467	0.73231
187	0.67902	1.33427	0.73202
138	0.07875	1.30898	0.73174
189	0.57849	1.29027	0.73146
190	0.67822	1.27533	0.73118
191	0.67795	1.37737	0.73090
192	0.67770	1.33688	0.73062
193	0.67743	1.31153	0.73035
194	0.67718	1.29276	0.73007
195	0.67692	1.27779	0.72980
195	0.67666	1.38001	0.72953
197	0.67541	1.33942	0.72926
198	0.67515	1.31401	0.72899
199	0.67590	1.29520	0.72872
200	0.67565	1.28018	0.72846

APPENDIX B

This appendix contains the computer program used to generate the values tabled in Appendix A in such a manner that they could be plotted by the Calcomp Plotter and the nineteen families of curves which were plotted.

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	CALL ERRSET (
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- 1	7 60 III:1,5
	EAD (5,8) MM(III),W
o	JAMAI (213,
	FINA(111).EQ.987) G
	F (IIII.NE.
	1=1
	2=2
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	2=400
	1=2
	0 10
(5)	11 3
] = 4
	2=00
	0.10
4	- J u.
	L 1=601
	01 0
'n	14

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1F SG, 60 TO 31.
                                                                                                                                                                                                                                                                                                                                           IF(((1X-1)-200*(111-1))/1ETR(111)-MM(111)/M(111)) 31,33,33
                                                                                                                                                                                                                                                                                    CHECK TO SEE IF STEADY STATE HAS BEEN REACHED. OTHERWISE, GO TO 33.
                                                                   PERCYT(111)=(100-M(111))/MM(111)
                                                                                                                                                                                                                                                                                                                                                          IT=[IX-1-200*(III-1))/IETR(III)
                                                                                                              ETH FAMS YS FRAILS & LIMP / XCRUS
                                                                                                                                                                                                                                                                                                                                                                                                                                              8=8+X%/((X-8#ETR)##F)
                                                                                                                                                                                                                                                                                                                                                                                                    IF(II-1) 22,321,321
DG 322 N=1,II
                                                                                                                                                                                                                                                                                                                                                                                        AH (XMM- AWAM) / (XMAH)
                                                                                                                                                         ZET × (111) = 1 = 1 ETR(111)
A ALOG( .) / AL CG(2.0)
                                                       AIN=NK(111)/N(111)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       J=IX-IETR(III)
                                                                                                                                          1518 (1111) = XE18
                                                                                                                                                                                                                 DO 40 IX=11, L2
                                                                                                                           Xtln=2144.5
                                                                                XNSY SHNSYS
XCHUSHNCRUS
            CITION SEX
                                                                                                                                                                      INDEX = 200
SUMM = 0.0
                                                                                                                                                                                                  し。いまれるとつい
                                                                                                                                                                                                                                                                                                                                                                                                                                                                           2(1X)=4+8
                           ( I I I ) W = W X
                                        AREXYN/XE
                                                                                                                                                                                                                                              X=1X-L1+1
                                                                                                                                                                                                                                                                                                                                                                                                                                                            CONTINUE
                                                                                                                                                                                                                              9=0.0
                                                                                                                                                                                                                                                                                                                                                                         11=4
                                                                                                                                                                                                                                                                                                                                                                                                                                  215
                                                                                                                                                                                                                                                                                                                                                                                                                                                              322
                                                                                                                                                                                                                                                                                                                                                                                                                    321
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        33
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L=(J-L1+1)*IETK(I11)-IETR(I11)+L1
                                                                                                                                                                 IF (ICK-LE-INDEX) GO TO 41
                                                                                                                                    1+(111)%/(111)%%=(111)1v%I
                                                                                                                                                                                                                                                                                                                                                                                 ATDAR(J)=ATTTP(J)/ATTPN(J)
                                                                                                                                                                               INAT(111)=INDEX/IETR(111)
                                                                                                                                                                                                                             K=(J-L1+1)*[ETK(III)+[1-1
                                                                                                                                                   ICK=18AT(111)#1ETR(111)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    IF (1.NE.2) GO TO 1092
                                                                                                                                                                                                                                                                                                                                                                                                                                                          IF (I.NE.1) 50 TO 1091
                                                                                                      (XI)NI/(XI)I=(XI)NIOI
                                                                                                                                                                                               KNX=L1+IRAI(III)-1
00 51 J=L1,KNA
                                                                         CX TORT + MEET SHARKEDS
                                                                                     AVSTALLAL = SUMMN/A
                                                                                                                                                                                                                                                                                                                                                                 AITENIO) = SUMN/EIR
                                                                                                                                                                                                                                                                                                                                                                                                                            CALL FACTOR (0.9)
                                                                                                                                                                                                                                                                                                                                                 ATITP(J)=SUM/ETR
                                                                                                                                                                                                                                                                                                                     (×I) NI+NEOS = NEOS
                                          AVCTITAL SUSHIX
              T(IX) XMM/A(IX)
                              (XI)1・MMOSHMEDS
                                                           TRIIX)-II*Xeel
                                                                                                                                                                                                                                                                                                      SUM = SUM + T (IX)
                                                                                                                                                                                                                                                                                                                                                                                                                                           20 114 (=1,5
                                                                                                                                                                                                                                                                                       33 53 IX=L,K
FIX) S(1)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      50 TC 11A
                                                                                                                                                                                                                                                                                                                                                                                              CONTINUE
CONTINUE
                                                                                                                                                                                                                                                                         SUMN=0.0
                                                                                                                                                                                                                                                                                                                                    BUNITED S
                                                                                                                     CONTINUE
                                                                                                                                                                                                                                                           いっじ=いつの
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      302=27
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   L1=201
                                                                                                                                                                                                                                                                                                                                                                                                                                                                         L 1 = 1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     1601
                                                                                                                                                                                                                                                                                                                                                                                                51
               3.5
                                                                                                                      C 5
                                                                                                                                                                                                                                                                                                                                     50
                                                                                                                                                                                                Ţ
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CALL AXISI (0..0.19H REPETITION NUMBER ,-19,10.,6.,6.,20.,19.)
CALL SYMBOL (0.0.-1.0,0.10,57HFIGURE PLOT OF CUMULATIVE AVER
CALE IASK TIME WITH Q=,0.0,57)
                                                                                                                                                                                                                                                                                                                                                         CALL LINEI 1266..0..1..0..20...2)
CALL AXISI (0.,C.,30H CUMULATIVE AVERAGE TASK TIME ,36,5.,50.,0.,
                                                                                                                                                                                                                                       ALIGNING ZERD OF Y-AXIS ING INCHES ABLUE SOTTON OF PAPER
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              CALL SYMDGL (1.114,-1.20,0.10,5HIETR=,0.,5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              CALL NUMBER (XZ.YZ.0.10, 3.0.,2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                           CALL WHERE (AZ.YZ.FACTOR)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               CALL MHEPE (XZ,YZ,FACTUR)
                                                                                                                                                                                                                                                                                                         PLOT(6.C,-12.0,-2)
                 IF (1.NE.3) GO 10 1093
                                                                                  H (1.NE.4) SO 10 1094
                                                                                                                                                                                                                                                                          PLCT (13.,11.,-3)
                                                                                                                                                    IF (I.NE.5) GU IJ 112
                                                                                                                                                                                                                                                                                         PLOT (0. r, 11.0,3)
                                                                                                                                                                                                                                                                                                                       CALL PLGI(2.5,2.0,-3)
                                                                  60 10 112
60 10 112
                                                                                                                                    S0 to 112
                                                                                                                                                                                                      60 10 112
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               Yi=Yi-, 25
                                                                                                                                                                                                                                                                                                                                                                                                                                                                               61.+2X=3X
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 72=X4+110
                                                                                                                                                                                                                                                                                                                                                                                          C.2,10.0)
                                                                                                                                                                                      L 2=1960
                                                                                                                   ういなっとう
                                  1.1-4-1
                                                   160.71
                                                                                                   199=17
                                                                                                                                                                       L 1=801
                                                                                                                                                                                                                                                                                       CALL
                                                                                                                                                                                                                                                                                                        CALL
                755
                                                                                  1693
                                                                                                                                                     7501
                                                                                                                                                                                                                                                                    111
                                                                                                                                                                                                                                                                                                                                         ں
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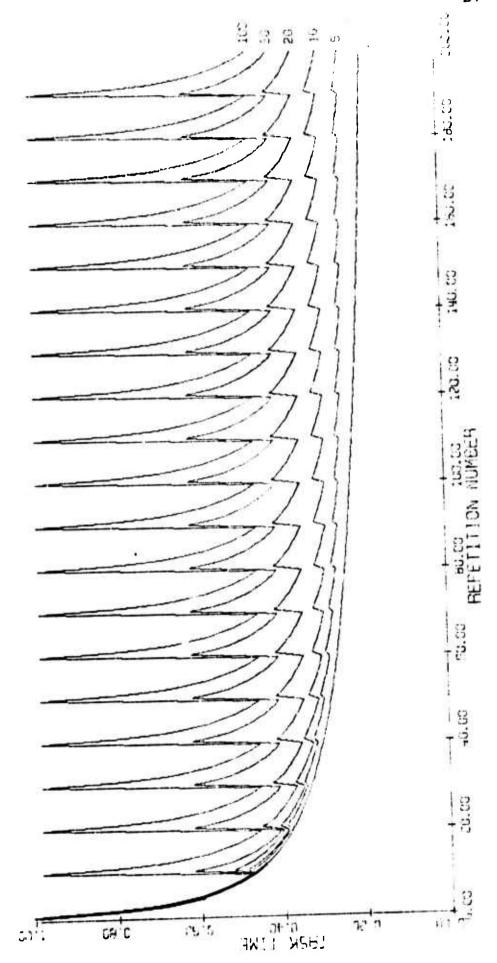
```
CALL NUMBER (XZ,YZ,0.10, PERCNT(I),0.,-1)
CALL NUMBER (AZ,YZ,0.10,ZETR(1),0.,-1)
                                             CALL LINE 2 (XX, AVGIN(IX), 1, 0, C, 0)
                                                                                                               CALL LINEZ (XX,AVGT(IX),1,0,0,0)
         CALL LINE 2 (1.,1.,1,0,1,0)
                                                                            CALL LINE2 (1.,1.,1.0,1.0)
DO 113 IX=L1,L2
                                                                                                                                      CALL WHERE (XZ,YZ,FACTOR)
                                                                                                                                                                                                          CALL PLOT (0.0,0.0,-99)
                                                                                                                                                                                                                                                                  GG TG 120
IF (I.NE.2) GG TG 225
                                                                                                                                                                                                                                 IF (I.NE.1) 50 TO 224
                                                                                                                                                                                                                                                                                                                           IF (I.NE.3) GO TO 226
                                                                                                                                                                                                                                                                                                                                                                         IF (1.NE.4) GO TO 227
                                                                                                                                                                                   CALL PLOT (0.,0.,3)
                                                                 CALL PLCT(0.,0.,3)
                      00 111 1X=L1,L2
                                                                                                                                                                                                                     DO 124 I=1,5
                                 XX= IX-L1+1
                                                                                                    XX=IX-L1+1
                                                                                                                                                             YZ=YZ-.75
                                                                                                                                                  ¥7=x2+10
                                                        CONTINUE
                                                                                                                           CONTINUE
                                                                                                                                                                                                                                                                                                                GO TO 122
                                                                                                                                                                                              CONTINUE
                                                                                                                                                                                                                                                                                                                                                             GD TO 122
                                                                                                                                                                                                                                                                                                                                                                                                           GO TO 122
                                                                                                                                                                                                                                                        L2=200
                                                                                                                                                                                                                                                                                                                                                  L2=60C
                                                                                                                                                                                                                                                                                                     12=400
                                                                                                                                                                                                                                                                                          L1=201
                                                                                                                                                                                                                                                                                                                                                                                     109=17
                                                                                                                                                                                                                                                                                                                                        105=17
                                                                                                                                                                                                                                             1=17
                                                      111
                                                                                                                          113
                                                                                                                                                                                                                                                                                                                           225
                                                                                                                                                                                                                                                                                                                                                                       226
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PLOT OF AVERAGE TASK TIM
                                                                                                                                                                                                                                                                                       CALL AXISI (0.,0.,35H AVERAGE TASK TIME PER TIME PERICO ,35,
                                                                                                                                                                                                                                                                                                                                    ,-15,10,,0,,0,,2,,10,,
                                                                                                            ALIGNING ZERD OF Y-AXIS IND INCHES ABOVE BOTTOM OF PAPER
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       SYMBOL (1.114,-1.20,0.10,5HIETR=,0.,5)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            CALL NUMBER (XZ,YZ,O.10,ZETR(I),O.,-1)
CALL LINEZ (1.,1.,1.,0,1,0)
                                                                                                                                                                                                                                                                                                                                CALL AXISI (0.,0.,15H PERIOD NUMBER
                                                                                                                                                                                                                                                                                                                                                      CALL SYMBOL (0.0,-1.0,0.1,52HFIGURE
                                                                                                                                                                                                                                                                                                                                                                          CE PER TIME PERIOD MITH Q=,0.0,62)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        CALL LINE 2 (XX, ATTPN(IX), 1,0,0,0)
                                                                                                                                                                                                                                                               CALL LINE1 (20.,C.,1.C.,0.,2.,.2)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                 CALL NUMBER (XZ,YZ,0.10,0,0.12)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       CALL LINE2 (1.,1.,1,0,1,0)
                                                                                                                                                                                                                                                                                                                                                                                                 CALL WHERE (XZ,YZ,FACTCR)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            CALL WHERE (XZ,YZ,FACTCR)
                                                                                                                                                                                               PLOT (5.0.-12.0.-2)
                                                                                                                                                     CALL PLOT (13.,11.,-3)
                                                                                                                                                                          PLOT(0.0,11.0,3:
IF (1.NE.5) GO TO 122
                                                                                                                                                                                                                     PLOT (2.5,2.0,-3)
                                                                                                                                                                                                                                                                                                          C5.,90.,0.,2,19.0)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 CALL PLOTIC., C., 3)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       KNR=LI+IRAT(I)-1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           DO 121 IX=L1, KNR
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             KNR=L 1+1 RAT(1)-1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    XX=1X-L1+1
                                                                                                                                                                                                                                                                                                                                                                                                                      47=Y4-.05
                                                                                                                                                                                                                                                                                                                                                                                                                                              01 *+ 2 X = 7 X
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 XZ=XZ+.1C
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       42=Y2-.05
                                                                 60 TO 122
                                         L 2=1000
                    108=17
                                                                                                                                                                                                                       CALL
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         CALL
                                                                                                                                                                            CALL
                                                                                                                                                                                                  CALL
                                                                                                                                                     120
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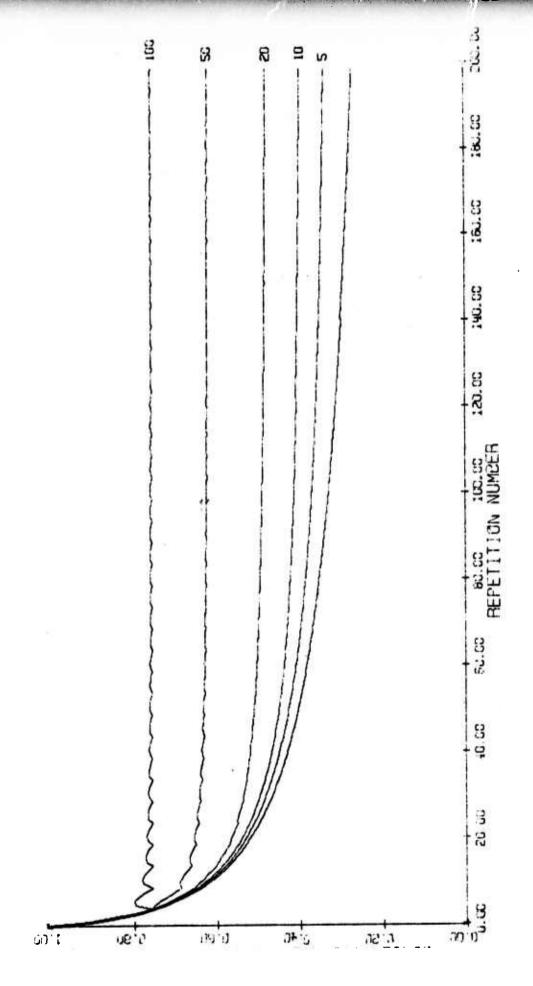
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ALIGNING ZERO OF Y-AXIS TWO INCHES ABOVE BOTTOM OF PAPER
                                                                                         CALL NUMBER (XZ,YZ,O,10,PERCNT([),G,,-1)
CALL PLOT (G,,0,,3)
                         CALL LINE? (XX,ATTTP(IX),1,0,C,0)
                                                   CALL WHERE (XZ,YZ,FACTCR)
                                                                                                                   CALL PLOT (0.0,0.0,-99)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                CALL PLGT (13.,11.,-3)
                                                                                                                                                         IF (I.NE.1) GO TO 234
                                                                                                                                                                                                              G0 T0 235
                                                                                                                                                                                                                                                               IF (1.NE.3) GO TO 236
                                                                                                                                                                                                                                                                                                                   IF (I.NE.4) GO TO 237
                                                                                                                                                                                                                                                                                                                                                                       IF (I.NE.5) GO TO 132
00 123 IX=L1,KNK
                                                                                                                                           00 134 1=1,5
                                                                                                                                                                                                GO TO 130
IF (1.NE.2)
              XX=[X-11+1
                                                                                                                                                                                                                                                                                         L2=600
60 TU 132
                                                              01 - + 7 X = 7 X
                                                                             ¥2=¥2-.05
                                                                                                                                                                                                                                                   60 TO 132
                                                                                                                                                                                                                                                                                                                                                        50 10 132
                                      CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                 12=1000
                                                                                                                                                                                                                         L1=201
L2=400
                                                                                                                                                                                  12=200
                                                                                                                                                                                                                                                                                                                                             L2=800
                                                                                                                                                                                                                                                                                                                                                                                   158=17
                                                                                                                                                                                                                                                                                                                               11=901
                                                                                                                                                                                                                                                                             11=401
                                                                                                                                                                       1=17
                                      123
                                                                                                                   124
                                                                                                                                                                                                             234
                                                                                                                                                                                                                                                                235
                                                                                                                                                                                                                                                                                                                   236
                                                                                                                                                                                                                                                                                                                                                                       237
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CALL AXISI (0.,0.,0.) PERIOD NUMBER ,-15,10.,0.,0.,2.,1C.)
CALL SYMBCL (0.0,-1.0,0.1,109HFIGURE
CE TASK TIME PER TIME PERICD FOR DIFFERENT TURNOVER RATES TO THE ,
                                                                                                                                                                                               TASK TIME PER TIME PERIOD
                                                                                                 AXISI (0.,0.,21H ATTTP(IX)/ATTPN(IX) ,21,5.,90.,1.,.2,10.0)
                                                                                                                                                                                                                .,0.0,77)
                                                                                                                                                                                                                                      CALL NUMBER (6.171,-1.20,0.10,0,0.2)
CALL NUMBER (7.028,-1.20,0.10,2ETR(!),0.,-1)
CALL LINE2 (1.,1.,1.0,1.0)
                                                                                                                                                                                              CALL SYMBOL (1.114,-1.20,0.10,77HAVERAGE WITH NO TURNOVER WITH LE AND IETR=
                                                                                                                                                                                                                                                                                                                                                                                                                                                         CALL NUMBER (XZ,YZ,0.10,PERCNT([),0.,-1)
                                                                                                                                                                                                                                                                                                                                                            (0.0.0.
                                                                             LINE1 (2C.,0.,2.,1.,2.,2)
                                                                                                                                                                                                                   C WITH NO TURNOVER WITH CH
                                                                                                                                                                                                                                                                                                                                                                                                CALL WHERE (XZ,YZ,FACTOR
                                                                                                                                                                                                                                                                                                                                                            CALL LINEZ (XX, ATDAN(IX
                  PLCT(0.0,-12.0,-2)
                                      PLUT (2.5,2.0,-3)
PLGT (0.0,11.0,3)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  CALL PLOT (0.,0.,-99)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                             CALL PLOT (0.,C.,3)
                                                                                                                                                                                                                                                                                                 KNR=11+1RAT(1)-1
                                                                                                                                                                                                                                                                                                                     00 131 IX=L1, KNR
                                                                                                                                                                                                                                                                                                                                        XX=! X-L1+1
                                                                                                                                                                                                                                                                                                                                                                                                                   XZ=XZ+-10
                                                                                                                                                                                                                                                                                                                                                                                                                                      YZ=YZ-.05
                                                                                                                                                                                                                                                                                                                                                                              CONTINUE
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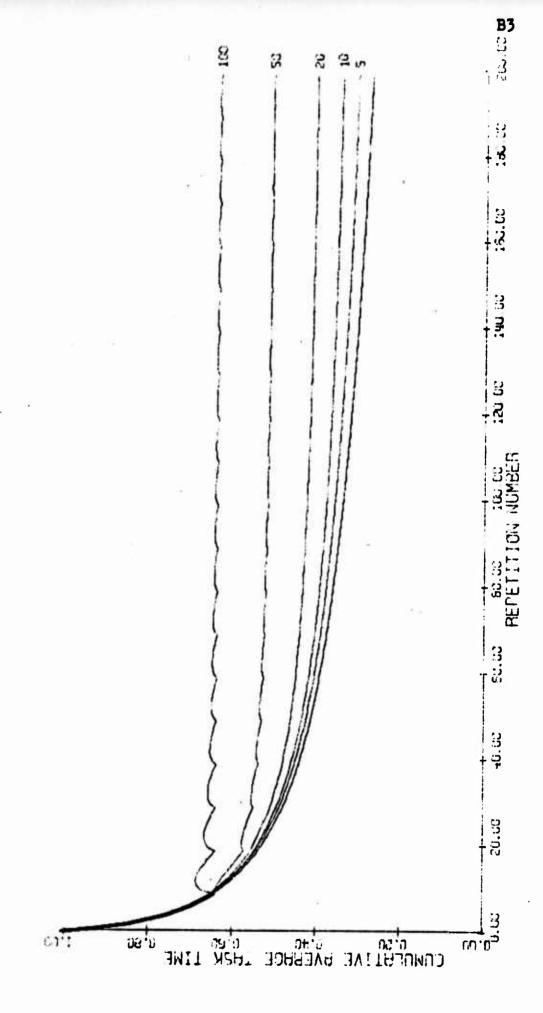




PLST OF TOTAL AND INCLAL FOR DIPPERENT TURNOLDS SATES WITH G-U.35. TETRATO FIGURE BL :



FIS RE BR : PLOT OF CUMULATIVE AVERAGE 195K TIME WITH G-0.50



EIGUPE B3 : PLOT OF COMULATIVE AVERSOE TASK/IIME WITH 0 C.30

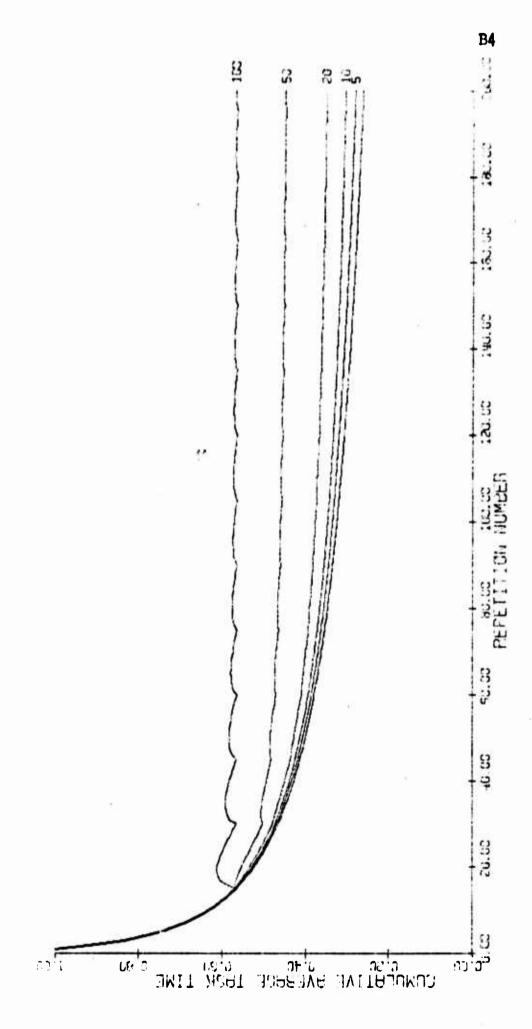
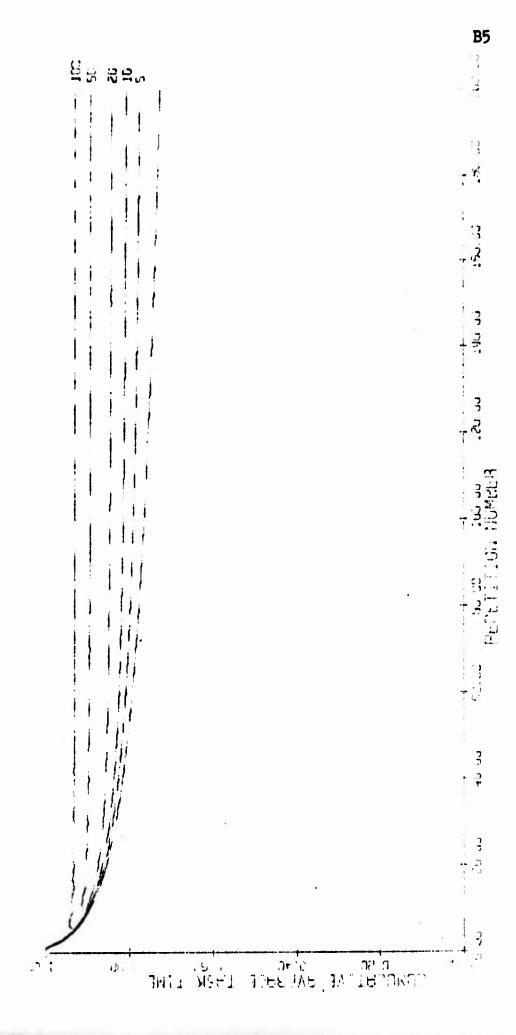
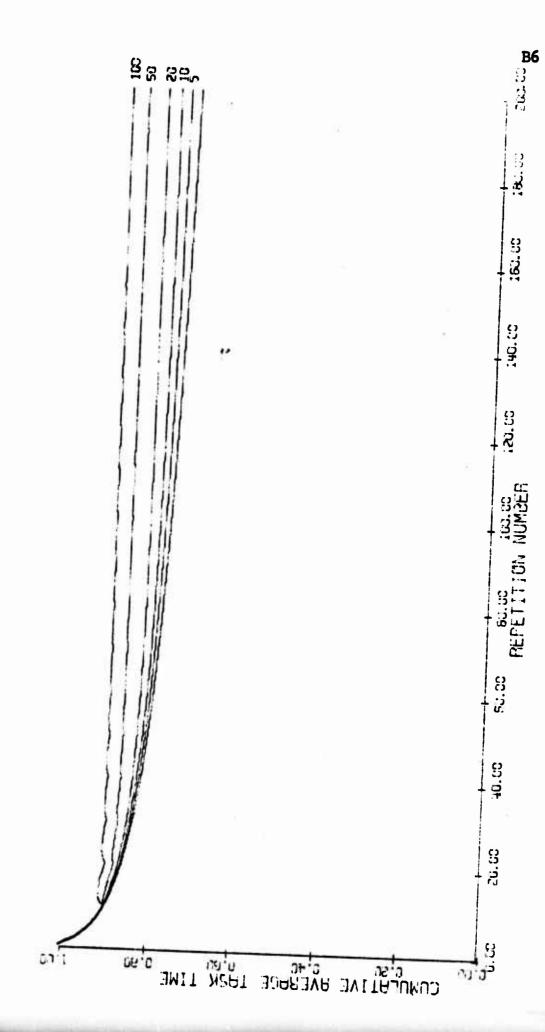


FIGURE B4 : PLGT GF UPMULRITYE AVERAGE TASK TIME MITH G-G-30 IETA-15



FILUPL BS - 7.87 6-18%.317c AVERAGE 1956 117c WITH U-0 95



FISURE B6: PLOT OF COMOLATIVE AVERAGE 195K TIME WITH G-0.95

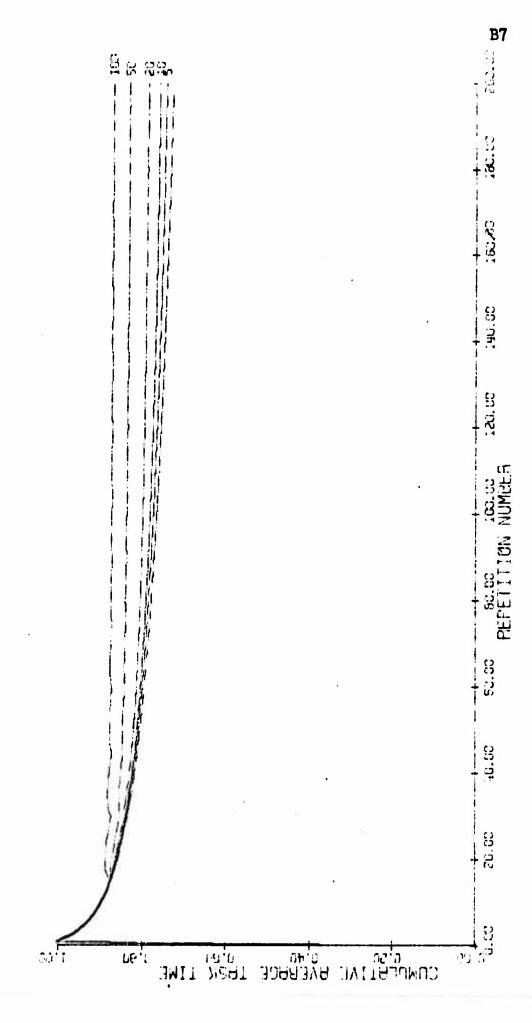
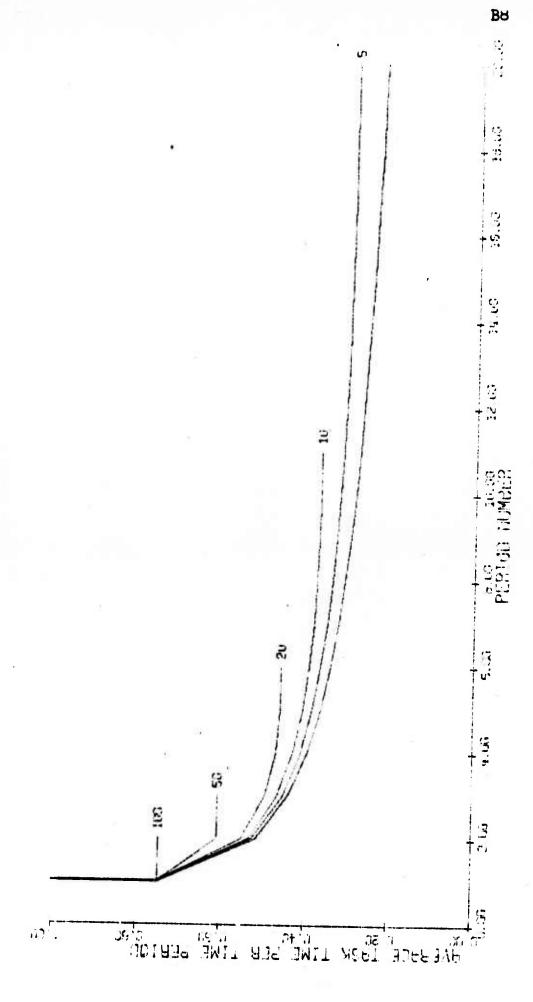


FIGURE BZ : PLGF OF COMOLETINE RYERBUSE FRSK TIME WITH G-G-95 TETR-15



FILAME BS : PLOT OF EVERAGE FASK TIME PER TIME PERIOD ATTH GROUPS

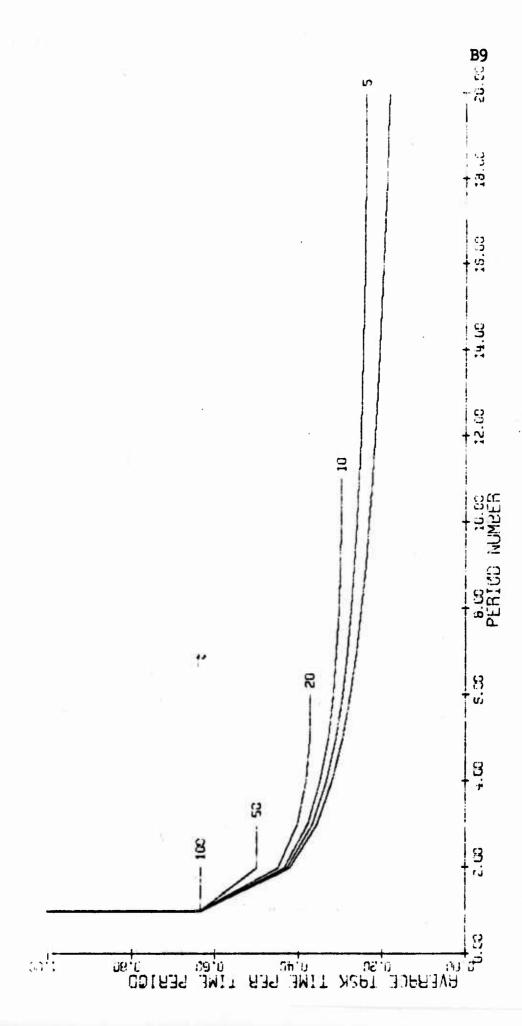
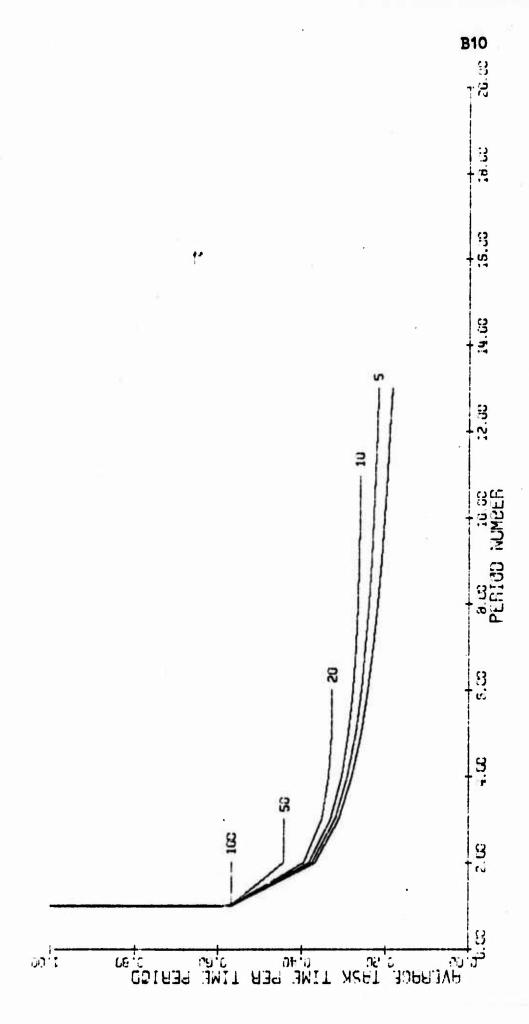
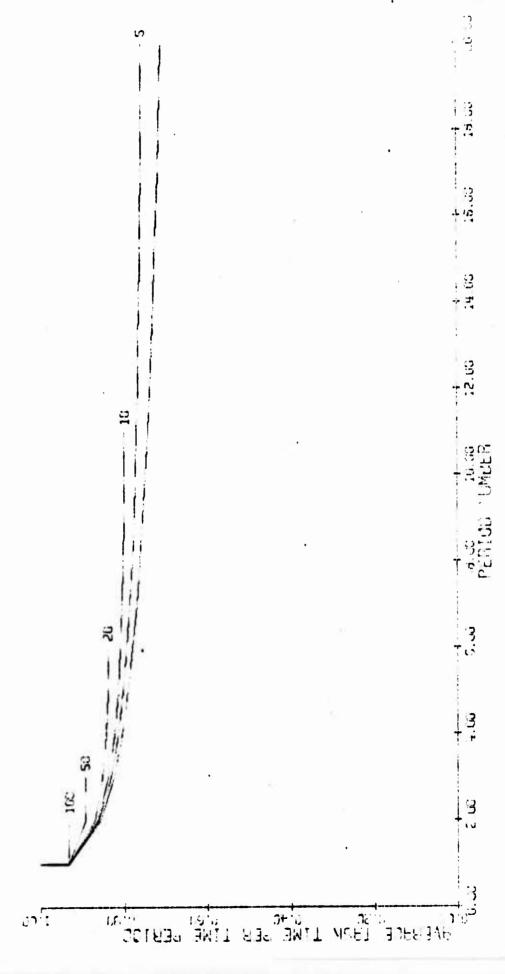


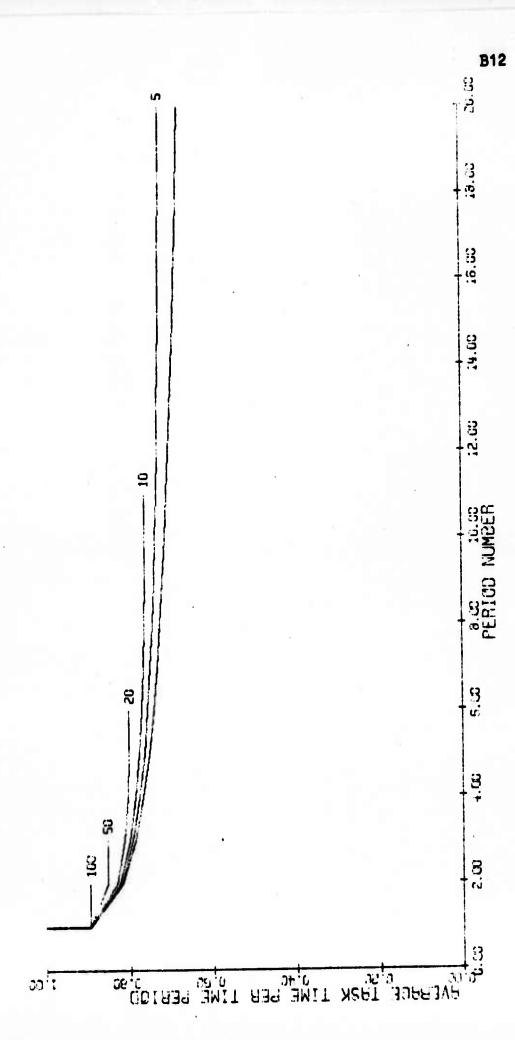
FIGURE 89 : PLGT OF SVERRUE TASK TIME PER TINE PERIOD WITH 0.6.30



FICURE BIO: PLOT OF EVERSUE TSSK TIME PER TIME PERIOD WITH G-U.50



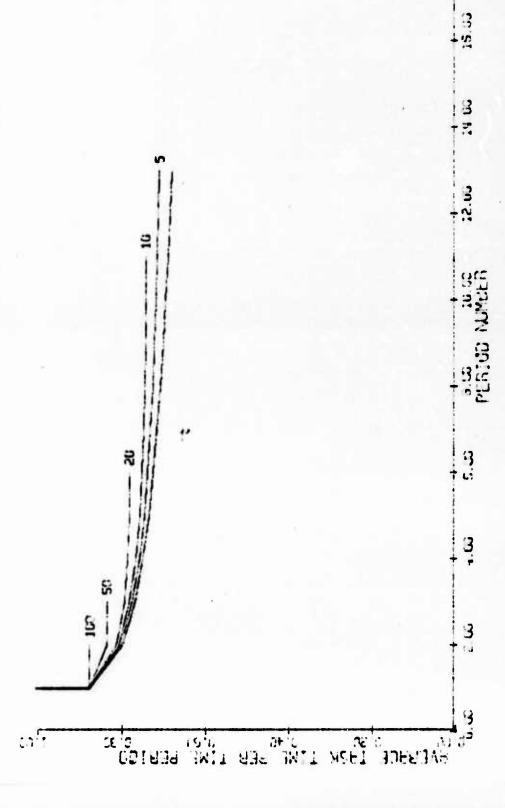
FILLER BN: PLGT G AVERAGE TASK TIME FLT TIME PLETGE WITH U-0.95



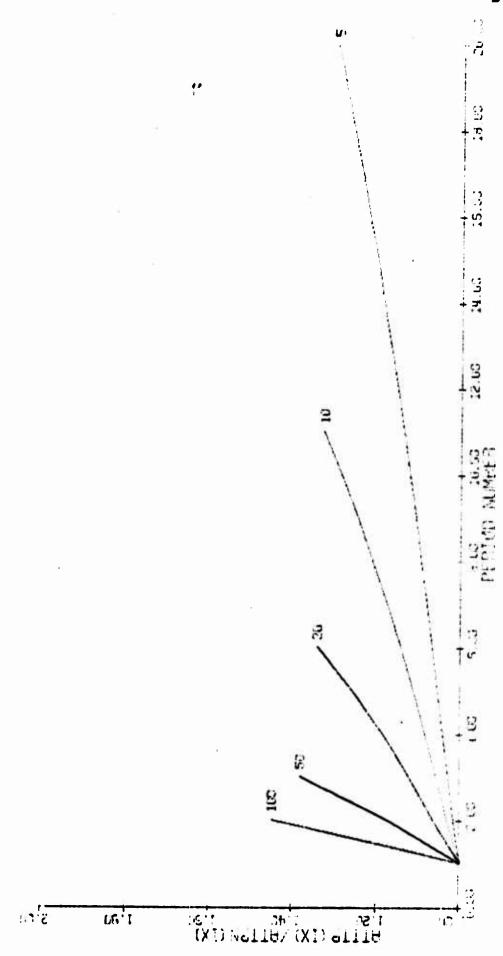
FICURE BIZ : PLGT OF SVENGOE TASK TIME PER TINE PERIOD WITH G-0.95 IETR-10



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FILUPE BUS : PLOT OF EVERRENE TOSK TIME TER TIME TERIOD ATTM GAG. 95



FLANDE **214**: PLUT OF BATES JR BYGROLE 1994 TIME PET TIME PECICOL FUR DEFENENT TUR IGVER 191ES TO FHE GAMES WITH UP OLSO RED 1519-5

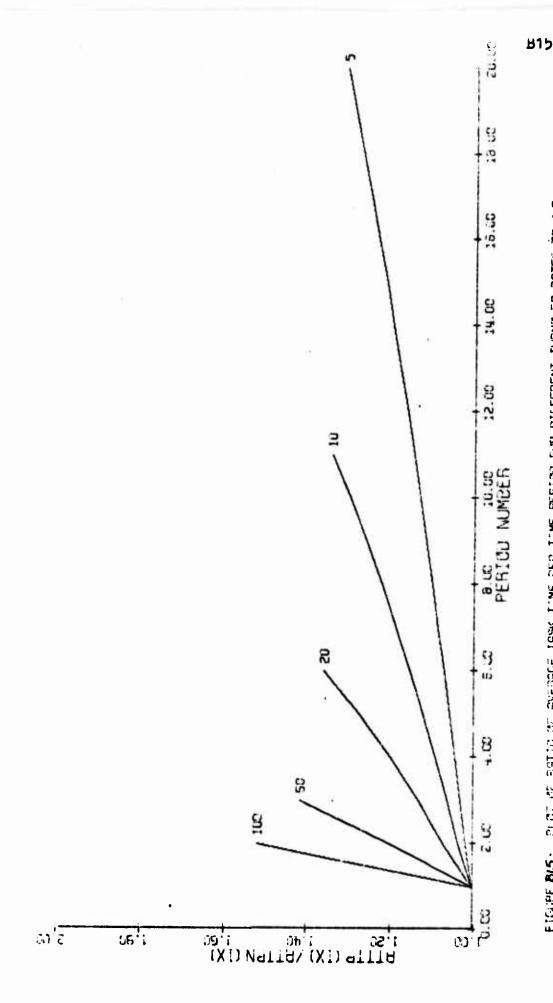
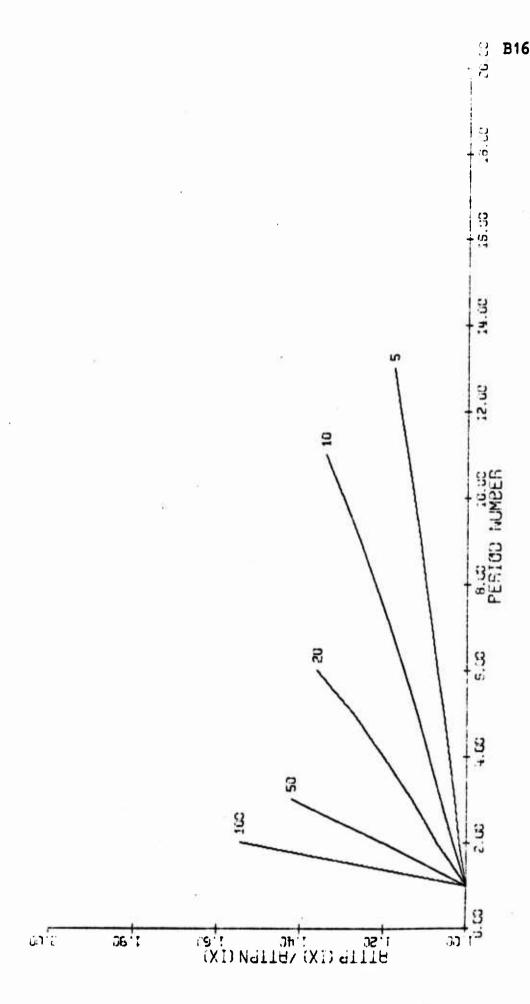


FIGURE **8/5:** PLOT OF SATIO OF SVENEGE 199K TIME PEN TIME PENTON FOR DIFFERENT TURNOVER SATES TO TAE AVERGOE 195K TIME PEN TIME PERTON WITH NO TURNOVER WITH QUI DISCOND TETAL 10

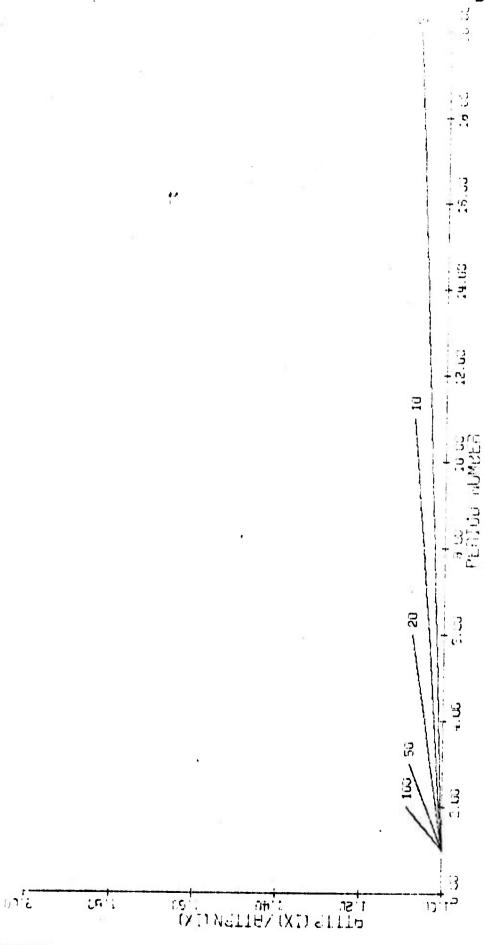


FICUPE BIG. PLOT OF SATIO OF SVERBGE 185K TIME PER TIME FERIOD FOR DIFFERENT TURNOVER SATES TO THE RECIPE STORY.





FIGURE **817**: PLOT OF 1971G OF AVENAGE ISSK TIME PER TIME PERIOG FOR OFFERENT TURNGWEN ASTES TO THE AVENAGE THAT FOR TIME PERIOD WITH BUILD BUTH G. O.95 9ND 1519±5



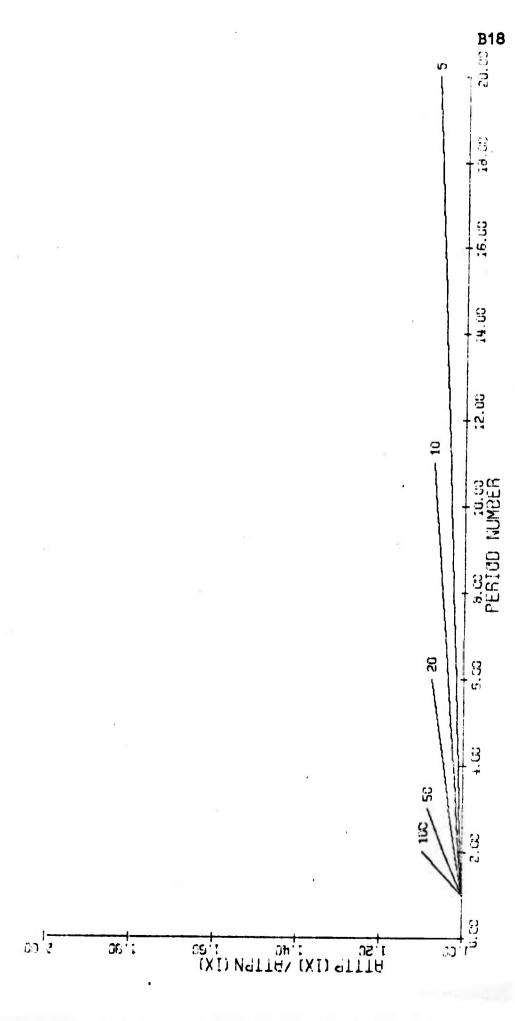
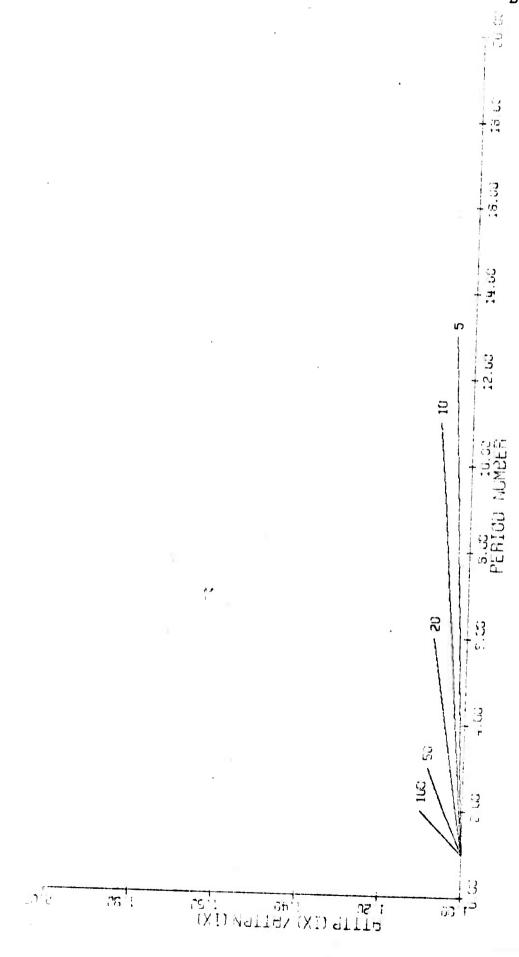


Figure BIS: "LOT OF SATIO OF AVERAGE 19SK TIME PER TIME PERIOD FOR DIFFERENT TURNOVER 99TES TO 19E GVERGGE 19SK TIME PER TIME PERIOD WITH NO TURNOVER WITH OF 0.95 AND TEGRE NO.



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FISCAL **819**: Pids of natio of evergoe 185K TIME PER TIME PERIOD FOR DIFFERENT TURNOVER RETES TO THE AVERGOE 185K TIME PERIOD WITH NO TURNOVER WITH G- 0.95 AND INTA-15.